

DRAFT:
DATE SUBMITTED: August 15, 2008

ROUTINE AND FRACTURE CRITICAL BRIDGE INSPECTION REPORT



Mn/DOT CONTRACT NO. 91600

**BRIDGE # 9090
THE JOHN F. KENNEDY MEMORIAL BRIDGE
US HIGHWAY 2 over the RED RIVER OF THE NORTH
EAST GRAND FORKS, POLK COUNTY
DISTRICT 2**

**Start Date of Inspection: 06/24/2008
Finish Date of Inspection: 06/28/2008**

**Prepared For
Minnesota Department of Transportation
Office of Bridges and Structures**



Prepared By:



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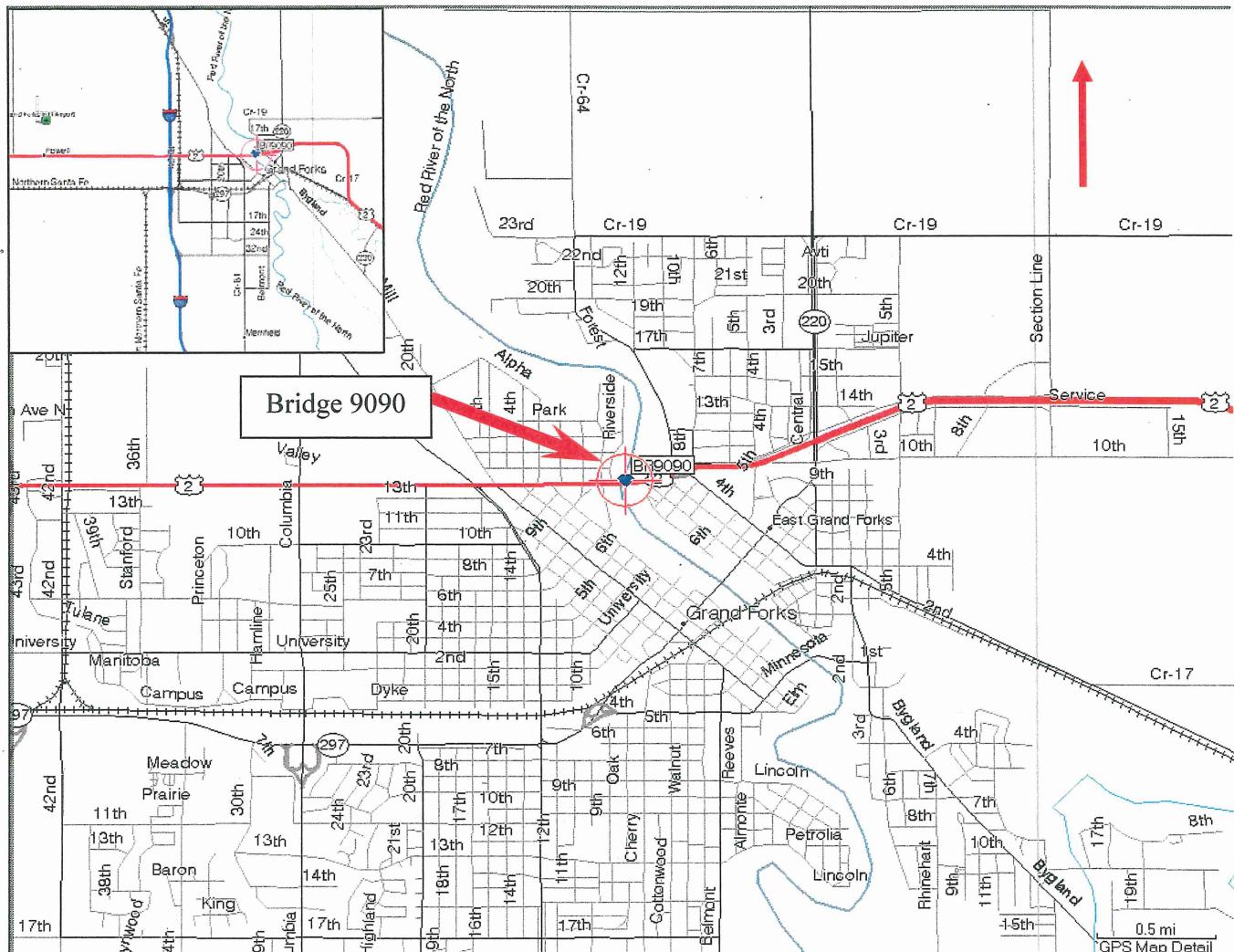
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LOCATION MAP
(Located in Grand Forks, SD)



EAST GRAND FORKS, POLK COUNTY

I. Executive Summary

This report documents the findings of the routine and fracture critical inspection of Mn/DOT Bridge No. 9090 – US TH 2 over the Red River of the North in East Grand Forks, Polk County, Township, Minnesota.

The inspection started on June 24, 2008 and was completed on June 28, 2008. No underwater inspection was performed.

A. SIGNIFICANT FINDINGS

1. A crack was found during the 2007 inspection at Panel Point L0 on the south truss of the west span, in the lower right corner of the gusset plate. The crack was approximately 2" long. The gusset plate at this location is welded to the bottom and the top chord member. The crack was totally removed by grinding and extended completely through the outer chord plate (Photo 18).

Recommendation: Monitor area of gusset plate where crack was removed for further cracking on a yearly basis.

2. At several panel points on each truss (Panel Points L1A, L1, L1'), the gusset plates are stiffened with angles along the unsupported portion of the plate. These angles are only tack weld to the gusset plate. At L1A' on the north truss of the east span, pack rust has caused random tack welds to crack (Photo 12). One of the angles on the east side of the inner plate was easily removed by hand during the inspection.

Recommendation: Analysis shall be performed to determine if stiffening angles are required at these locations. If required, existing cracked welds shall be removed and more permanent welds shall be used to re-attach stiffening angles to gusset plates.

3. At the end Panel Points for each truss, there is an area above the bottom chord that is completely enclosed by steel members that has trapped a significant amount of moisten laden dirt and debris (Photo 14).

Recommendation: These areas shall be flush clean of moisten laden dirt and debris, and holes shall be drilled in batten plates (top and bottom) just above the bottom chord to allow for drainage of water off the top surface of the bottom chord.

4. There are pins and hangers located in Spans 1 to 3 and 9 to 12 (Photo 20). The nuts have been tack welded to the channel hanger at two locations on each nut. The majority of these tack welds on the lower pin have cracked (Photo 16). There is no evidence that the crack has propagated into the base metal.

Recommendation: The movement of the hangers has caused these tack welds to crack. Thus, these tack welds should be removed to allow free rotation and movement of the pin and hanger system.

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5. The rocker bearings at Piers 6 are excessively expanded, approximately 8.4 degrees to the west, at a temperature of 81°F (Photo 21). The pintles are partially exposed.

Recommendation: The rocker bearings on Pier 6 should be continued to be monitored for movement and an interim inspection should be performed during the winter months when temperatures are significantly lower for signs of movement.

6. There are sliding plate bearing in Spans 5 and 8. The keeper plates for several of these bearings have cracked due to pack rust (Photo 22).

Recommendation: Where keeper plates have cracked, the keeper plate shall be removed, the pack rust removed and the keeper plate re-welded back into place.

7. Pier 6 has diagonal cracks on both faces of the pier (Photo 23). However, these cracks go in the opposite direction of each other and could indicate movement of the pier causing torsion or twisting of the pier wall.

Recommendation: Monitoring of Pier 6 for additional cracking and movement should be performed. A detail survey of Pier 6 setting up control point should be established to detect any future movement of the pier.

For additional recommendations, refer to Section V, Conclusions and Recommendations.

B. CONDITION SUMMARY

The results of the inspection indicate that the bridge is overall in satisfactory condition. There were no significant noticeable changes in any of the structural components since the last inspection. The paint system is in generally good condition. There is some random areas where the paint has peeled and several locations where pack rust is evident between the bottom horizontal connection plate and the floorbeams.

The deck is in satisfactory condition. There are random spalls along the concrete curb face and parapet.

The 2007 Inspection report indicated that the superstructure was in fair condition however the SI&A sheet indicate the superstructure to be in good condition. Based on the finding of this inspection, the superstructure is considered to be in satisfactory condition. The lower truss members within region of splash zones have isolated areas of minor corrosion on the splice connection, gusset plates and horizontal connecting plates. At several panel points pack rust has developed between the bottom horizontal connection plate and the bottom flange of the floorbeams. No significant section losses were noted. The floorbeams are in satisfactory condition with no significant

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deterioration or defects noted. The stringers are in good condition for both the truss spans and all 11 approach spans. There are isolated areas of peeling paint and minor surface rust. No pitting or section loss has occurred. There is an area of minor collision damage in Span 12 to Stringers 1 and 2. The bottom flange of Stringer 1 has been bent upward 1 ½".

There are pins and hangers in Spans 1 to 3 and Spans 9 to 12. The nuts have been tack welded to the channel hanger. The majority of these tack welds on the lower pin have cracked. There is no evidence that the crack has propagated into the base metal.

The rocker bearings at Pier 6 are excessively expanded at a temperature of 81 degrees. At Pier 6, the rockers have shifted approximately 8.4 degrees to the west and the pintles are exposed. At Pier 7, the rocker bearings on the south truss have shift in opposite directions. There are sliding plate bearing in Spans 5 and 8. The keeper plates for several of these bearings are cracked due to pack rust.

The substructure is in satisfactory condition. Pier 6 has diagonal cracks on both faces of the pier. However, these cracks go in the opposite direction of each other and could indicate torsion or twisting of the pier. At Bent 5, there is some erosion of the soil around the foundation. The steel pier columns at Bents 2 to 5 and 9 to 13, exhibit some surface rust but not significant loss of section.

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II. Introduction

The focus of this report is the presentation of the routine inspection findings and fracture critical evaluation for Mn/DOT Bridge No. 9090, US TH 2 over the Red River of the North in East Grand Forks located in Polk County, Minnesota.

The bridge was inspected on June 24, 2008 to June 28, 2008..

The inspection team was comprised of Jeff Moore, P.E. (TL), Dave Haxton, P.E. (TL), Kyle Stanley (ATL) and Kevin Clark (ATL).

In addition, as specified in the contract, red line markups of the previous Mn/DOT Structure Inventory Reports and Mn/DOT PONTIS Bridge Inspection Reports have been provided as separate attachments to this report.

Bridge Description

Bridge 9090 is a 13-span structure consisting of two Park style high truss main spans and eleven (11) steel multi-beam approach spans (Photo 1). The trusses are constructed of built-up members assembled with a combination of welding and high strength bolts. The structure was built in 1963 and has a total structure length of 1,261 feet.

The main truss spans are supported by concrete piers and span 279 feet each. The approach spans have concrete abutments and hinged steel bents. The bridge runs east to west on US TH 2 over the Red River of the North at the North Dakota state line. It carries 4 lanes of traffic, two in each direction.

Inspection Access

The hands-on and visual Fracture Critical and Routine inspection was performed using a UB-50 to inspect the underside of the deck, floorbeams and lower chord members. A 45 foot manlift was used to access the upper portion of the truss (above the deck), and all sway frames and top horizontal and diagonal bracing members. The abutments, wingwalls and lower portions of the piers were inspected from the ground .

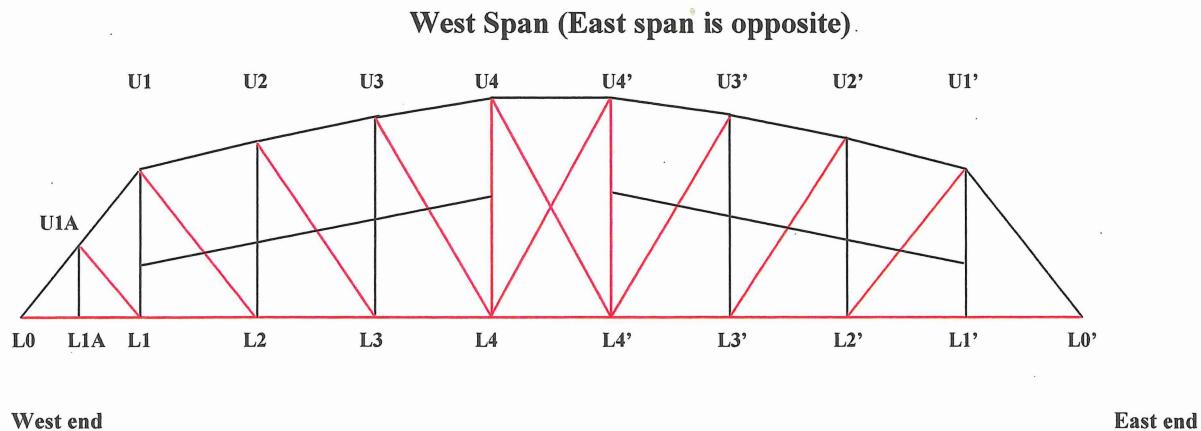
Fracture Critical Members on this bridge are the tension members of the non-redundant trusses and the floorbeams.

Additional bridge data can be found in the MNDOT Structure Inventory Report.

Prior to the inspection of the bridge, advance notification to the appropriate authorities was required prior to performing any lane closures. Minnesota DOT provided single lane closures during the inspection.

III. Fracture Critical Members and Fatigue-Prone Details

Fracture Critical Members on this bridge are the tension members of the non-redundant trusses and the floorbeams. The riveted, built up truss connections are classified as Fatigue Category D in accordance with AASHTO LRFD Bridge Design Specification, 4th Edition, Table 6.6.1.2.3-1.



Truss diagram showing Panel Point numbering system
Fracture Critical tension Members shown in **Bolded Red** (per previous cycle report)

V. Inspection Findings

Deck Elements

The deck element is in satisfactory condition.

Wearing Surface: The concrete deck is covered with a low slump overlay. The overlay is in generally good condition with only minor random transverse cracks (Photo 3). In Span 10, there is a concrete fracture (1'x2.5') in the overlay surface in the right lane of the EB roadway. The concrete edge along the deck joints exhibit minor chipping and spalls. There are also several locations in Spans 11 and 12 that have been repaired with a concrete patch.

Underside of deck: The underside of the deck is in satisfactory condition (Photo 6). There are random transverse cracks with light efflorescence in each span. In Span 10, bay1, there is a large area (5'x10') where deck exhibit moisture contamination with map cracking and efflorescence (Photo 8). In addition, the overhang areas along the approach spans exhibit random spalls, fractures and in some locations expose and rust reinforcing steel(Photo 7) . In the two main truss spans, the sides of the deck slab have spalled directly over the floorbeams. The deck is also pumping (moving up and down) over the floorbeams most evident at each end and under the longitudinal joint (Photo 24).

Bridge Railing: The approach spans have a concrete bridge railing along both safetywalks. The crack posts are randomly cracked and spalled in each span. At some locations there is exposed rebar (Photo 5). The metal railing on top of the concrete railing has been damage at two locations at the northeast end of the bridge.

Curbs: The concrete curbs are in fair condition. The curbs are randomly riddled with small spalls, fractures, cracks and exposed rebar (Photo 4). It appears in most cast these spalls have been caused by insufficient concrete cover over the reinforcing steel. In several of the spans the deterioration to the curb is substantial and can be found at the following locations:

Span 1	North curb	4'-0" long
Span 5	Median curb, south side mid span	14'-0" long
Span 7	Median curb both sides (Riddle with Spalls)	Full length
Span 9	North curb	5-0" long
Span 11	North curb	25'-0" long

Joints: All joints on the bridge are in generally good condition. The strip seal joints are all in tack and partially cover with dirt and debris but functioning. The strip seal joint over Pier 2 in the median area has a missing joint plate cover on the north face. The finger joints over Piers 6 and 8 exhibits no visible problems and has sufficient space to expand and contract. The rubber drainage trough under the finger joints is in tack and functioning. The hot poured joints in the deck slab are in good condition.

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Deck Drainage: The drain outlets are located on each side of deck along the gutterline and are positioned between floorbeams. Outlets are all clear of debris and functioning. The drain pipes in Spans 6 and 7 (truss spans) extends below the bottom chord and are supported by a steel strap that is welded directly to the bottom chord. At these locations there is significant corrosion and pack rust between the strap and the side of the bottom chord. In additional, there were several locations in the truss spans where the drainage pipe was missing allow water runoff to outlet onto the bottom chord (Photo 7).

Superstructure

The superstructure elements are in satisfactory condition.

Trusses: The **Upper Chords** members are in good condition (Photo 9). The paint system is in tack and there are no significant signs of rust (Photo 11). At some enclosed panel point locations, pigeons have nested and there is a significant amount of debris that has caused some rust stains on the surface of the paint (Photo 10).

The **Lower Chords** are in satisfactory condition. The paint system has minor areas of peeling paint and isolated locations of rusts in the splash zones. In general, there appears to be more rust exhibit at either ends of the each truss (L0 and L0') and at the splice connections (Photos 13 & 15). At all four corners of each truss (L0 and L0') there is an enclosed area on the top of the bottom chord that traps water and debris (Photo 14). This water and debris is causing corrosion to the top of the bottom chord and the inner surface of the vertical gusset plates.

At panel points L1A, L1A', L2' and L2, the vertical gusset plates are stiffened with angles long the unsupported length. These angles are only tack welded to the gusset plate and the space between welds has allowed moisture and rust to develop between the angle and the gusset plate. This rust has caused in many locations the tack welds to crack. At L1A' on the north truss, east span, the stiffening angles was removed by hand from the gusset plate (Photo 12).

It should also be noted that at random floorbeam locations, pack rust has developed between the horizontal connection plate and the bottom of the floorbeam. This pack rust is a maximum $\frac{1}{4}$ " at random locations and has slight distort the plates (Photo 25). At L3N west span, the bottom connection plate appear to have been bent upward during construction in order to connect to the bottom flange of the floorbeam which appears to be slight higher then the bottom of the lower chord.

Vertical and Diagonal Members have very minor random corrosion in the splash zone region. This area normally encompasses the bottom third of the members.

Floorbeams: The Floorbeams are in good condition. There are brown stains typically found on each floorbeam on the top flange and web surface at each end and under the longitudinal joint (Photo 24). This is due to the deck pumping directly above the

floorbeam. There is also some minor random rust at the floorbeam connection to the bottom chord.

Stringers (Truss Spans): The stringers are in good condition. The paint system is in good condition with only several minor areas where paint has peeled and there are not significant defects.

Secondary members: The Top and Bottom Lateral Bracings and Sway Frames are in good condition.

Approach Spans: The approach spans consist of 8 - 36" rolled stringers (4 lines of stringers in each direction). The stringers are in good condition with no significant corrosion or section loss. The paint system on the bottom flange in random spans has deteriorated and the surface rust has developed. There is some minor collision damage in Span 12 to stringers 1 and 2 (Photo 17).

There are pins and hangers in Spans 2, 3, 4, 9, 10, 11 and 12 (Photo 20). There are tack welds between the nut and the hanger at both top and bottom pins. It was observed that most tack welds on the bottom pins have cracked (Photo 16). Cracks have not propagated into the base metal of the hanger. There are also rotation pins at the centerline. At some locations, there is significant corrosion exhibited in and around these pins.

Bearings: There are fixed bearing on Pier 7 supporting the north trusses and rocker bearings on Piers 6, 7 and 8 supporting the end of both trusses. At Pier 6, the rockers have shifted approximately 8 degrees to the west and the pintles are exposed (Photo 21). At Pier 7, the rocker bearings on the south truss have shift in opposite directions.

There are sliding plate bearing in Spans 5 and 8. The keeper plates for several of these bearings have cracked due to pack rust (Photo 22).

Substructure

The substructure elements are in satisfactory condition.

East and West Abutments: The abutments have no significant defects. There is some minor cracking and spalls on the backwall.

Pier 6 has diagonal cracks on both faces of the pier (Photo 23). However, these cracks go in the opposite direction of each other and could indicate torsion or twisting of the pier. At Bent 5, there is some erosion of the soil around the foundation.

The steel pier columns at Bents 2 to 5 and 9 to 13, exhibit some surface rust but not significant loss of section. The embankment on the west side of the river appears to be unstable and erosion of the soil is evident. The fixed hinges that support the stringers on top of the steel pier bents are securely attached to the top of the bent. There are several missing cotter pins on Bent 4 (from west) (Photo 19).

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Miscellaneous

Approach Pavements: The approach pavements at both ends of bridge appear to be in good condition. There are a few minor cracks in the concrete surface. The westbound roadway in the west approach is overlaid with asphalt (Photo 2).

Approach Guardrails: There are no approach guiderails.

Load posting: None noted

V. Conclusions and Recommendations

The overall condition of the bridge is satisfactory due to the condition of the superstructure and substructure.

The deck is in satisfactory condition. The underside of the deck slab has numerous random fractures and spalls with exposed rebar in the overhang area of the deck. The deck is also pumping (moving) about the floorbeams, most evident at the end of each span.

The superstructure is in satisfactory condition. The paint system is in generally good condition throughout the bridge. However, there are random areas on the approach stringers where the paint has failed on the bottom flange of the fascia stringers. There is also some minor rust at bottom chord splice connections and at each panel point.

Pack rust is starting to develop and is randomly located between the bottom flange of the floorbeams and the lower chord connection plate, and was evident at the rotational pin in the approach spans.

The substructure is in satisfactory condition and has no significant defects or deterioration. Pier 6 exhibits diagonal cracks on either side of the concrete pier wall. These cracks go in opposite direction and need to be monitored.

Recommendations:

We recommend that the following safety improvements, repairs or rehabilitation and/or monitoring should be made, to retard further deterioration, preserve the structural integrity of the bridge and extend its useful life:

1. **Priority for Repair:** Analysis shall be performed to determine if stiffening angles are required at Panel Points L1A' U1A', L2' east span and L1A, U1A, L2 in the west span. If required, existing cracked tack welds shall be removed and more permanent welds shall be used to secure stiffening angles to gusset plates. At L1A' where the stiffener has fall off, stiffener needs to be welded back into place (Photo 12).
2. **Priority for Repair:** At the end Panel Points for each truss, these areas shall be flush clean of moisten laden dirt and debris, and holes shall be drilled in batten plates (top and bottom) just above the bottom chord to allow for drainage of water off the top surface of the bottom chord (Photo 14).
3. **Priority for Repair:** Where keeper plates have cracked on the sliding plate bearings in Span 5 (Str. 1, 2, 3, 5 and 7) and Span 8 (str. 5), the keeper plate shall be removed, the pack rust removed and the keeper plate re-welded back into place (Photo 22).

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4. Since there are no approach guardrails and the blunt end of the barrier curb is exposed on both approach roadways, it is recommended that MnDOT and North Dakota conduct a review of design criteria for guardrails to determine the need for them at this location.
5. The rocker bearings on Pier 6 should be continued to be monitored for movement and an interim inspection should be performed during the winter months when temperatures are significantly lower for signs of movement (Photo 21).
6. Monitoring of Pier 6 for additional cracking and movement should be performed. A detail survey of Pier 6 setting up control point should be established to detect any future movement of the pier (Photo 23).
7. The movement of the hangers has caused these tack welds to crack. Thus, these tack welds should be removed to allow free rotation and movement of the pin and hanger system (Photo 16).
8. Monitor area of gusset plate at Panel Point L0 on the south truss of the west span where crack was removed for further cracking on a yearly basis (Photo 18).

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Appendix A

Inspection Photographs

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Photo 1 – South Elevation looking north.



Photo 2 – West Approach looking west.

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Photo 3 – General view of top of deck, looking east.

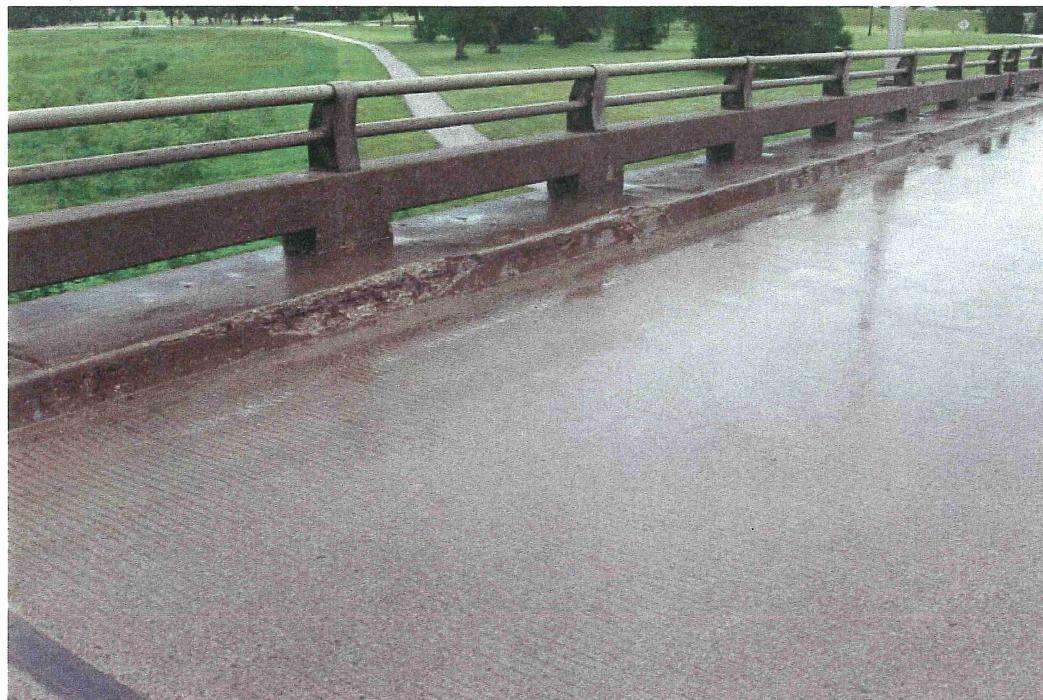


Photo 4 – Span 11, north curb line, approximately 25 feet of spalled curb with exposed rebar.

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Photo 5 – Span 7, concrete spall in parapet post with exposed rebar, looking south. Cracking of concrete and insufficient concrete cover has caused spalls to develop at random location along each parapet.



Photo 6 – Typical condition of longitudinal deck joint along center line of structure. Looking west.

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Photo 7 – East Truss Span (Span 7), random spall with exposed rebar in north soffit area. Note there is no downspout extension connected to deck outlet pipe. Looking up and west.



Photo 8 – Span 10, underside of deck slab between Stringers S1 and S2 exhibits an area of moisture contaminate deck, 5'x10'. Looking up and east.

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Photo 9 – General view of upper chord members, looking east.



Photo 10 – At random locations inside the upper chord members, birds have nested. This nest is located in the lateral bracing adjacent to panel point U4'N.

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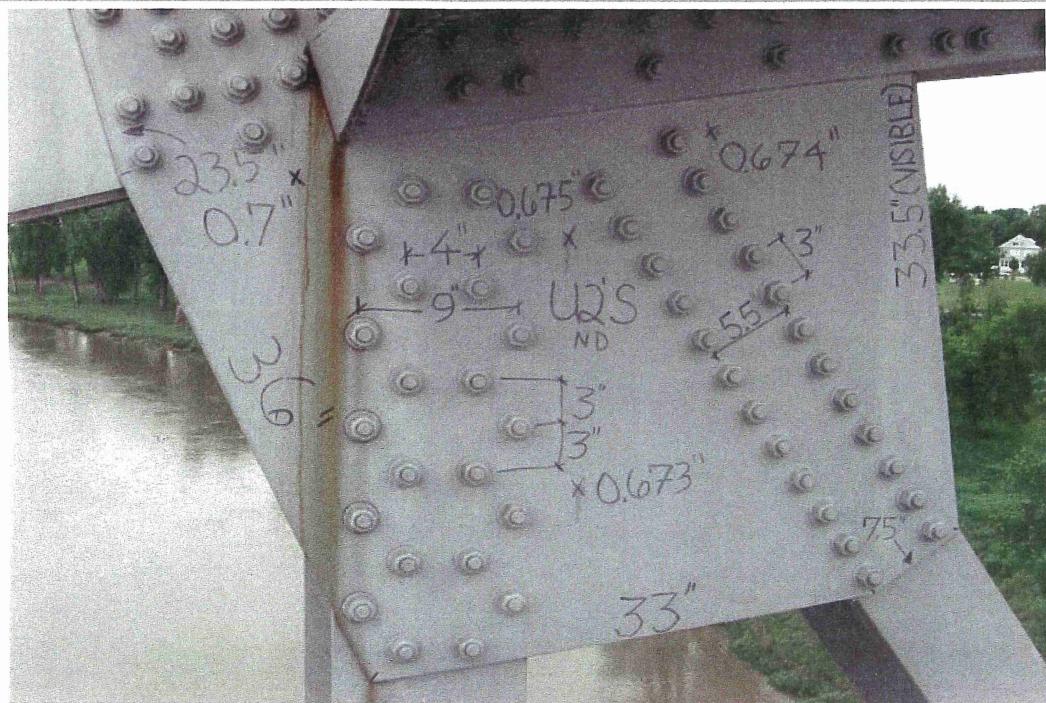


Photo 11 – Panel Point U2'S, inner gusset plate. Looking south.

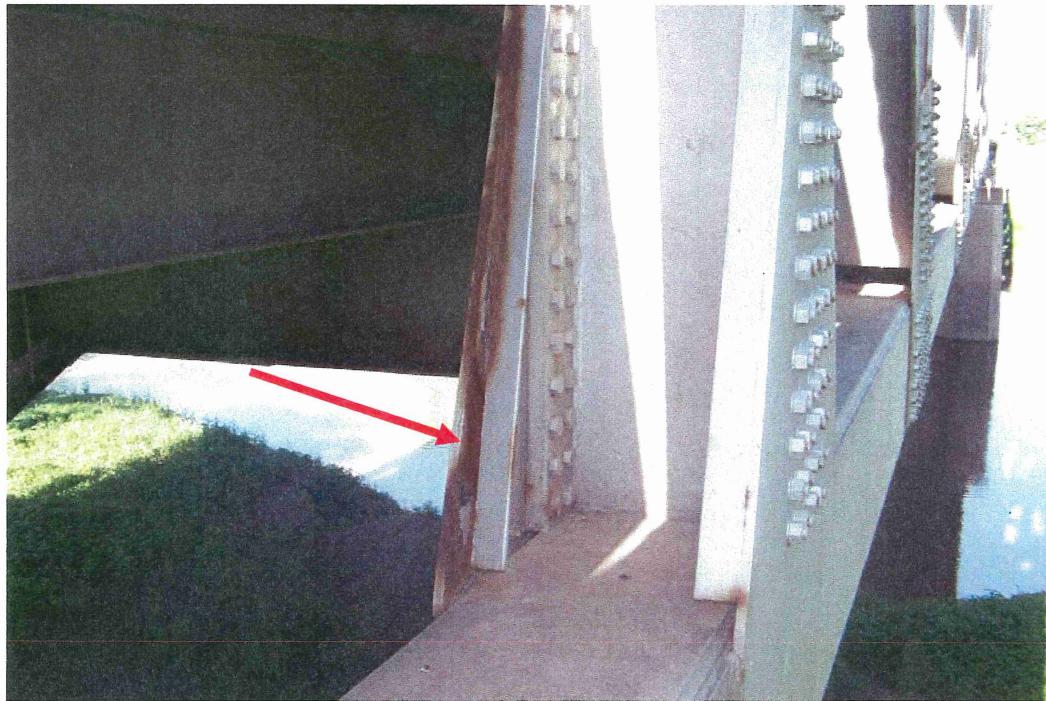


Photo 12 – North Truss, East Span (Span 7), east side of panel point L1A', looking west. Note stiffening angles is partial detached from inner gusset plate. This stiffener was removed by inspector by hand. Looking west.

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Photo 13 – North truss, west span, panel point L0'. Top batten plate has heavy pack rust between plates causing bending of the out portion of the plate. Looking southwest.



Photo 14 – East Truss Span (Span 7), panel point L0 on the south truss. Note that water and debris has accumulated inside of diagonal member. This is a typical condition at all end panels. Looking west.

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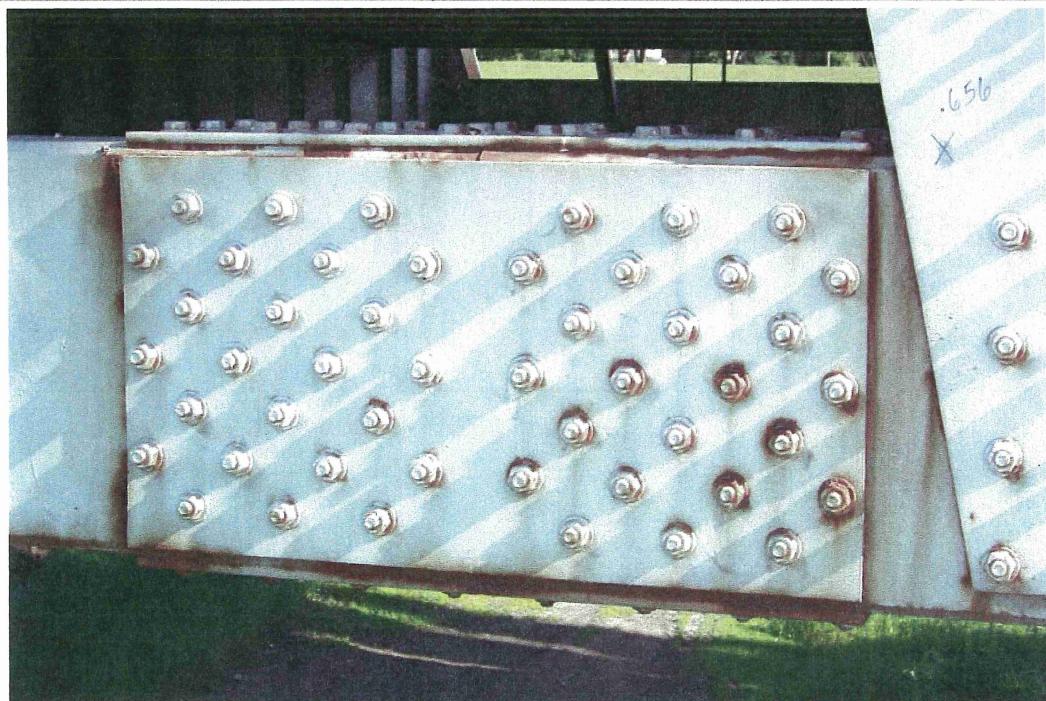


Photo 15 – West Truss Span (Span 6), south truss, typical lower chord splice connection. Rust is developing between splice plates and lower chord members. Looking north.

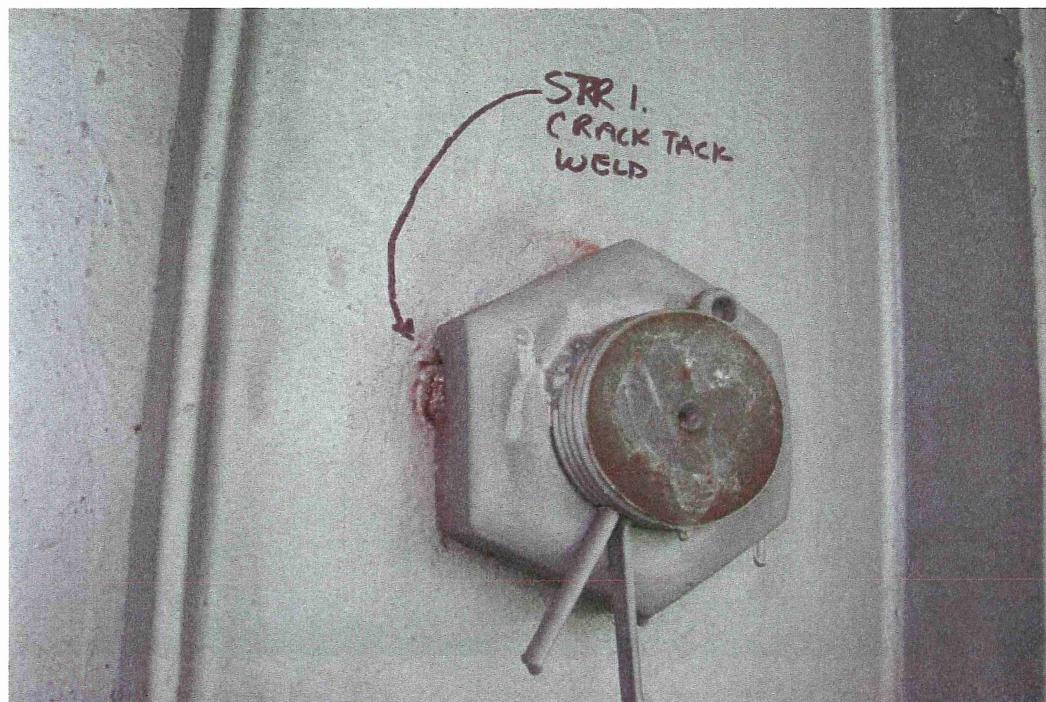


Photo 16 – Span 9, Stringer 1, crack tack weld between nut and hanger. Looking North.

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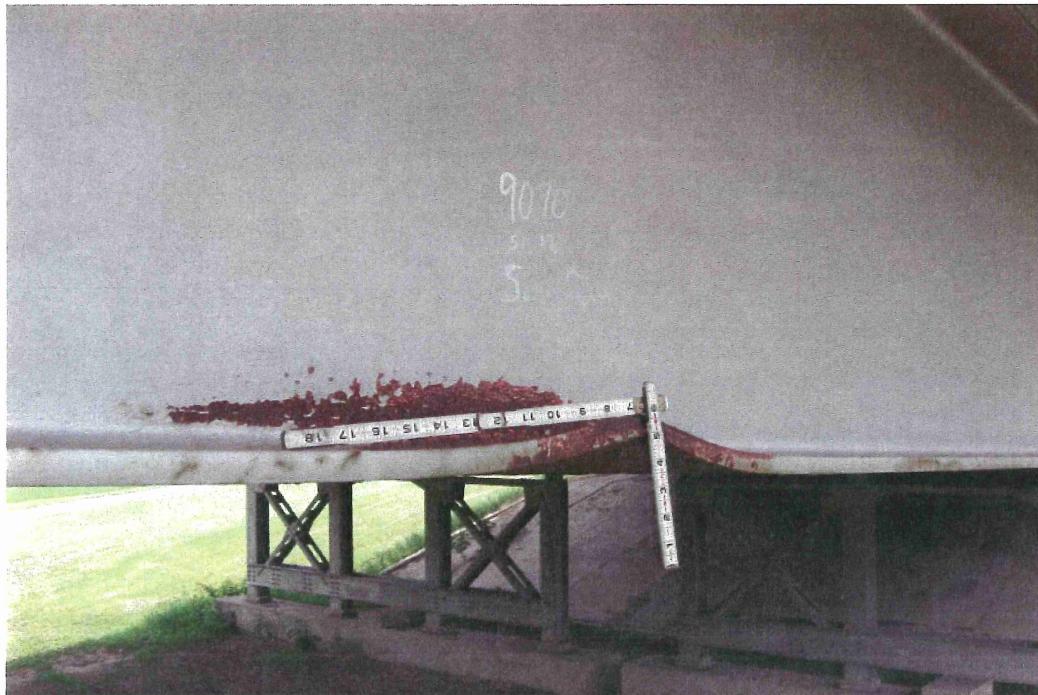


Photo 17 – Span 12, south fascia, impact damage to bottom flange. Bottom flange has been bent upward 2". Looking northeast.



Photo 18 – West span, south truss, panel point L0. Location where crack was previous removed by grinding and caulked. Note visible signs of new cracks. Looking north.

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Photo 19 – Typical fixed support over Bents 2 to 5, and 9 to 13. Photo taken at Bent 5, Stringer 6, missing cotter pin on south side.



Photo 20 – Typical condition of pin and hanger.

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Photo 21 – Pier 6, north rocker bearing. Rocker bearing has rotated 8.4° to the west with an air temperature of 81 degrees. Looking north. Pintles are exposed.



Photo 22 – Span 5, Stringer 1, cracked keeper plate weld.

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Photo 23 – Bent 6, east face, note 1/8" diagonal cracks in pier face. Similar cracks noted on west face however going in the opposite direction.

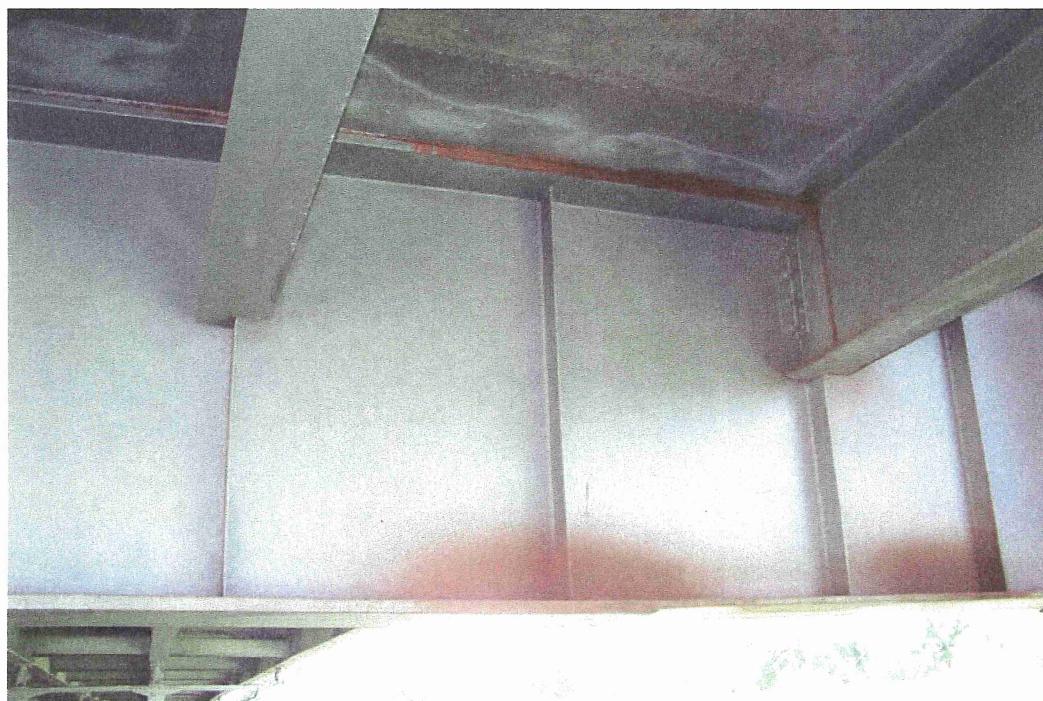


Photo 24 – Typical pumping of deck above floorbeams in truss spans. Pumping of deck is most evident at either end of floorbeam and at mid span.

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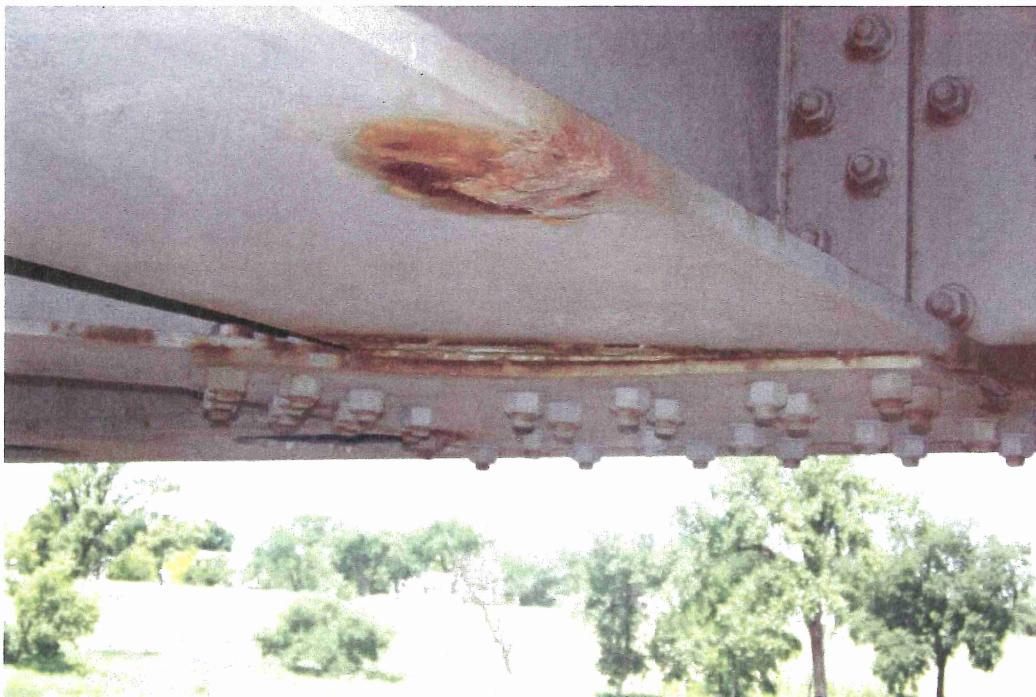


Photo 25 – East Truss Span (Span 7), north truss at panel point L3'. Note pack rust (3/8") between lower horizontal connection plate to bottom flange of floorbeam. This condition is randomly found throughout the truss spans.

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Appendix B

Field Inspection Notes

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Appendix C

Structure Inventory Report (SIR) and Pontis Redlines

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Mn/DOT Structure Inventory Report

Bridge ID: 9090 US 2 over RED RIVER & CITY ST

Settler A moore 7-15-08

JJ H Moore (TL) Date: 06/11/2008

+ G E N E R A L +		+ R O A D W A Y +		+ I N S P E C T I O N +	
Agency Br. No.		Bridge Match ID (TIS)	1	Deficient Status	ADEQ
District 2	Maint. Area 2B	Roadway O/U Key	1-ON	Sufficiency Rating	83.4 <i>6-28-2008</i>
County 60 - POLK		Route Sys/Nbr	USTH 2	Last Inspection Date	05-09-2007
City EAST GRAND FORKS		Roadway Name or Description		Inspection Frequency	12
Township		US 2		Inspector Name	<i>DISTRICT 2 PB</i>
Desc. Loc. AT N DAKOTA STATE LINE		Roadway Function	MAINLINE	Structure	A-OPEN
Sect., Twp., Range 02 - 151N - 50W		Roadway Type	2 WAY TRAF	+ C O N D I T I O N C O D E S +	
Latitude 47d 55m 59.78s		Control Section (TH Only)	6018	Deck	6 ✓
Longitude 97d 02m 13.84s		Ref. Point (TH Only)	000+00.000	Superstructure	7 6 ✓
Custodian STATE HWY		Date Opened to Traffic	01-01-1963	Substructure	6 ✓
Owner STATE HWY		Detour Length	2 mi.	Channel	7 ✓
Inspection By DISTRICT 2		Lanes	4 Lanes ON Bridge	Culvert	N
BMU Agreement No.		ADT (YEAR)	21,500 (2004)	+ A P P R A I S A L R A T I N G S +	
Year Built 1963		HCADT	1,935	Structure Evaluation	6
Year Fed Rehab		Functional Class.	URB/OTH PR ART	Deck Geometry	5 ✓
Year Remodeled		+ R D W Y D I M E N S I O N S +		Underclearances	4 ✓
Temp		If Divided	NB-EW SB-WB	Waterway Adequacy	6 ✓
Plan Avail. CENTRAL		Roadway Width	28.0 ft	Approach Alignment	7 ✓
+ S T R U C T U R E +		Vertical Clearance	19.9 ft	+ S A F E T Y F E A T U R E S +	
Service On HWY;PED		Max. Vert. Clear.	19.9 ft	Bridge Railing	1-MEETS STANDARDS ✓
Service Under HWY;STREAM		Horizontal Clear.	28.0 ft	Appr. Guardrail	1-MEETS STANDARDS ✓
Main Span Type STEEL HIGH TRUSS		Lateral Cir. - Lt/Rt		GR Transition	1-MEETS STANDARDS ✓
Main Span Detail PARKER		Appr. Surface Width	60.0 ft	GR Termini	1-MEETS STANDARDS ✓
Appr. Span Type STEEL BM SPAN		Roadway Width	56.0 ft	+ I N D E P T H I N S P . +	
Appr. Span Detail		Median Width	4.0 ft	Frac. Critical	Y 24 mo 09/2007 <i>04/2008</i>
Skew		+ M I S C . B R I D G E D A T A +		Underwater	Y 60 mo 07/2004
Culvert Type		Structure Flared	NO	Pinned Asby.	Y 48 mo 06/2007
Barrel Length		Parallel Structure	NONE	Spec. Feat.	
Number of Spans		Field Conn. ID	RIVETED	+ W A T E R W A Y +	
MAIN: 2 APPR: 11 TOTAL: 13		Cantilever ID	PIN & HANGER	Drainage Area	
Main Span Length 279.0 ft		Foundations		Waterway Opening	29000 sq ft
Structure Length 1,261.0 ft		Abut.	CONC - FTG PILE	Navigation Control	NO PRMT REQD
Deck Width 65.0 ft		Pier	STEEL - FTG PILE	Pier Protection	
Deck Material C-I-P CONCRETE		+ P A I N T +		Nav. Vert./Horz. Cir.	
Wear Surf Type LOW SLUMP CONC		Year Painted	1996	Nav. Vert. Lift Bridge Clear.	
Wear Surf Install Year 1984		Pct. Unsound	5 %	MN Scour Code	L-STBL;LOW RISK
Wear Course/Fill Depth 0.17 ft		Painted Area	183,102 sf	Scour Evaluation Year	1997
Deck Membrane NONE		Primer Type	OTHER	+ C A P A C I T Y R A T I N G S +	
Deck Rebars N/A		Finish Type	URETHANE	Design Load	HS20
Deck Rebars Install Year		+ B R I D G E S I G N S +		Operating Rating	HS 35.4
Structure Area 81,965 sq ft		Posted Load	NOT REQUIRED	Inventory Rating	HS 21.3
Roadway Area 70,611 sq ft		Traffic	NOT REQUIRED	Posting	
Sidewalk Width - L/R 2.5 ft 2.5 ft		Horizontal	OBJECT MARKERS	Rating Date	11-13-1995
Curb Height - L/R 0.75 ft 0.75 ft		Vertical	NOT REQUIRED	Mn/DOT Permit Codes	
Rail Codes - L/R 19 19				A: 1	B: 1
				C: 1	

STRUCTURE INVENTORY REPORT V2008

Mn/DOT Bridge No. 9090
Routine and Fracture Critical Bridge Inspection Report

06/11/2008

Page 1 of 4

Inspector: DISTRICT 2
BRIDGE 9090

PB

Mn/DOT BRIDGE INSPECTION REPORT

6-28-2008

INSP. DATE: 05-09-2007

County: POLK	Location: AT N DAKOTA STATE LINE	Length: 1,261.0 ft
City: EAST GRAND FORKS	Route: USTH 2 Ref. Pt.: 000+00.000	Deck Width: 65.0 ft
Township:	Control Section: 6018 Maint. Area: 2B	Rdwy. Area / Pct. Unsd: 70,611 sq ft
Section: 02 Township: 151N Range: 50W	Local Agency Bridge Nbr:	Paint Area/ Pct. Unsd: 183,102 sq ft 5 %
Span Type: STEEL HIGH TRUSS		Culvert N/A
NBI Deck: 6 Super: 7 Sub: 6 Chan: 7 Culv: N	Open, Posted, Closed: OPEN	
Appraisal Ratings - Approach: 7 Waterway: 6	MN Scour Code: L-STBL;LOW RISK	Def. Stat: ADEQ Suff. Rate: 83.4
Required Bridge Signs - Load Posting: NOT REQUIRED	Traffic: NOT REQUIRED	
Horizontal: OBJECT MARKERS	Vertical: NOT REQUIRED	

STRUCTURE UNIT: 0

ELEM NBR	ELEMENT NAME	ENV	INSP. DATE	QUANTITY	QTY CS 1	QTY CS 2	QTY CS 3	QTY CS 4	QTY CS 5
22	LS O/L (CONC DECK)	2	05-09-2007 05-08-2006	81,965 SF 81,965 SF	0 0	81,965 81,965	0 0	0 0	0 0
Notes: Cracks in overlay at west finger jt. Small spall in median concrete on bottom side @ E. abut. br/wall w/bar exposed. Some deterioration of overhangs w/rust staining on appr. spans. Concrete spalling at the ends of many floorbeams. There appears to be a dip at the joint above the second bent from the west. There is a large hole in the deck 3.5' X 5' patched with bituminous. on the EBL in the right driving lane, on the ND side. ** This spall was patched with concrete on 7/11/07. DSH									
06-28-2008 81,965 SF 0 81,965 0 0 0 0 0 0									
300	STRIP SEAL JOINT	2	05-09-2007 05-08-2006	700 LF 700 LF	700 700	0 0	0 0	N/A N/A	N/A N/A
Notes: 06-28-2008 700 LF 700 0 0 N/A N/A									
301	POURED DECK JOINT	2	05-09-2007 05-08-2006	1,400 LF 1,400 LF	1,400 1,400	0 0	0 0	N/A N/A	N/A N/A
Notes: **Re-did all poured jts. w/hot rubber in 06 . DSH 06-28-2008 1,400 LF 1,400 0 0 N/A N/A									
303	ASSEMBLY DECK JOINT	2	05-09-2007 05-08-2006	140 LF 140 LF	140 140	0 0	0 0	N/A N/A	N/A N/A
Notes: < none > 06-28-2008 140 LF 140 0 0 N/A N/A									
321	CONC APPROACH SLAB	2	05-09-2007 05-08-2006	2 EA 2 EA	2 2	0 0	0 0	0 0	N/A N/A
Notes: < none > 06-28-2008 4 EA 4 0 0 0 N/A N/A									
333	RAILING - OTHER	2	05-09-2007 05-08-2006	2,522 LF 8,274 LF	2,274 8,274	250 0	0 0	N/A N/A	N/A N/A
Notes: Minor spalls in rails. Minor spall in South rail @ West end w/bar exposed. Two rail anchor castings on NE end have been hit & are broken. Several spalls on the bottom of the railposts.									
107	PAINTED STEEL GIRDER	2	05-09-2007 05-08-2006	5,600 LF 5,600 LF	5,600 5,600	0 0	0 0	0 0	0 0
Notes: Rust Beginning to Form. Several of the centerline rotational pins appear to be frozen due to corrosion. There is a bend in the bottom flange of the south fascia beam, span 12, no cracks present.									
113	PAINT STEEL STRINGER	2	05-09-2007 05-08-2006	97 LF 97 LF	97 97	0 0	0 0	0 0	0 0
Notes: Rust Beginning to Form. 06-28-2008 4,464 4208 0 256 0 0									

Mn/DOT Bridge No. 9090
Routine and Fracture Critical Bridge Inspection Report

06/11/2008

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Mn/DOT BRIDGE INSPECTION REPORT

Inspector: DISTRICT2

BRIDGE 9090

US 2 OVER RED RIVER & CITY ST

INSP. DATE: 05-09-2007

STRUCTURE UNIT: 0

ELEM NBR	ELEMENT NAME	ENV	INSP. DATE	QUANTITY	QTY CS 1	QTY CS 2	QTY CS 3	QTY CS 4	QTY CS 5
985	SLOPES	2	05-09-2007 05-08-2006	1 EA 1 EA	0 0	1 1	0 0	N/A N/A	N/A N/A
	Notes: Major transverse cracking in slope paving @ West end w/some heaving. Erosion at the 3rd bent from the west. The Dike on the MN side has been removed.		06-28-2008	1 EA	0	1	0	N/A	N/A
986	CURB & SIDEWALK	2	05-09-2007 05-08-2006	1 EA 1 EA	0 0	1 1	0 0	N/A N/A	N/A N/A
	Notes: cracks are present		06-28-2008	1 EA	0	1	0	N/A	N/A
988	MISCELLANEOUS	2	05-09-2007 05-08-2006	1 EA 1 EA	1 1	0 0	0 0	N/A N/A	N/A N/A
	Notes: < none >		06-28-2008	1 EA	1	0	0	N/A	N/A
422	PAINTED BEAM ENDS	1	05-09-2007	2 EA	2	0	0	0	0
	Notes:		06-28-2008	2 EA	2	0	0	0	0

General Notes:	NORTH	SOUTH
BENT 13	2-1/2"	0"
BENT 12	2"	1-1/2"
BENT 11	0"	1-1/2"
BENT 10	3/4	2"
BENT 9	1"	1-1/2"
PIER 8	1-3/4	1-3/4"
PIER 7	1-1/2"	2-1/4"
PIER 6	2"	6-1/2"
BENT 5	4"	3-1/4"
BENT 4	0"	0"
BENT 3	2-3/4"	0"
BENT 2	1 1/2"	3"

JH/HM

Inspector's Signature

Reviewer's Signature / Date

Mn/DOT Bridge No. 9090
Routine and Fracture Critical Bridge Inspection Report

06/11/2008

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Mn/DOT BRIDGE INSPECTION REPORT

Inspector: DISTRICT2

BRIDGE 9090

US 2 OVER RED RIVER & CITY ST

INSP. DATE: 05-09-2007

STRUCTURE UNIT: 0

ELEM NBR	ELEMENT NAME	ENV	INSP. DATE	QUANTITY	QTY CS 1	QTY CS 2	QTY CS 3	QTY CS 4	QTY CS 5
234	CONCRETE CAP	2	05-09-2007 05-08-2006	210 LF 210 LF	210	0	0	0	N/A
	Notes: Cracks in the west pier are at 1/16 inch wide.				06-28-2008	210LF	210	0	N/A
387	CONCRETE WINGWALL	2	05-09-2007 05-08-2006	4 EA 4 EA	4	0	0	0	N/A
	Notes: < none >				06-28-2008	4EA	4	0	N/A
357	PACK RUST	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	0	N/A
	Notes: < none >				06-28-2008	1EA	1	0	N/A
358	CONC DECK CRACKING	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	0	N/A
	Notes: Deck is cracked with leaching, and have been epoxied.				06-28-2008	1EA	1	0	N/A
359	CONC DECK UNDERSIDE	2	05-09-2007 05-08-2006	1 EA 1 EA	0	0	0	1	0
	Notes: Spalling at numerous places in the approach spans @ CenterLine @ 2nd Floor Beam W. of E. pier. Concrete spalling out over Floor Beams @ the 3rd and 4th from W. pier with rebar exposed. Large spalls in deck soffit both sides east approach span.				06-28-2008	1EA	0	1	0
360	SETTLEMENT	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	N/A	N/A
	Notes: Appears south end of west main pier has moved toward the river. There appears to be a dip at the joint above the second bent from the west. Is this Bent Footing settling? This needs to be checked out.				06-28-2008	1EA	1	0	N/A
363	SECTION LOSS	2	05-09-2007 05-08-2006	1 EA 1 EA	0	1	0	0	N/A
	Notes: ***The through trusses were blasted & painted in 1996. The % rated down is to denote existing sect loss. This problem will be evaluated at the next snooper inspection.***				06-28-2008	1EA	0	1	N/A
964	CRITICAL FINDING	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	N/A	N/A	N/A
	Notes: DO NOT DELETE THIS CRITICAL FINDING SMART FLAG.				06-28-2008	1EA	1	0	N/A
966	FRACTURE CRITICAL	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	N/A	N/A
	Notes: Do Not Remove. See in-depth report for location of F/C members.				06-28-2008	1EA	1	0	N/A
981	SIGNING	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	0	0
	Notes:				06-28-2008	1EA	1	0	0
982	GUARDRAIL	2	05-09-2007 05-08-2006	1 EA 1 EA	1	0	0	N/A	N/A
	Notes: Minor damage to SE connection plate.				06-28-2008	1EA	0	1	N/A
984	DRAINAGE	2	05-09-2007 05-08-2006	1 EA 1 EA	0	1	0	N/A	N/A
	Notes: Downspouts missing on NE corner of the main span. Slope washouts @ E. River bank.				06-28-2008	1EA	0	1	N/A

Mn/DOT Bridge No. 9090
Routine and Fracture Critical Bridge Inspection Report

06/11/2008

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Mn/DOT BRIDGE INSPECTION REPORT

Inspector: DISTRICT2

BRIDGE 9090

US 2 OVER RED RIVER & CITY ST

INSP. DATE: 05-09-2007

STRUCTURE UNIT: 0

ELEM NBR	ELEMENT NAME	ENV	INSP. DATE	QUANTITY	QTY CS 1	QTY CS 2	QTY CS 3	QTY CS 4	QTY CS 5
121	P/STL THRU TRUSS/BOT	2	05-09-2007 05-08-2006	1,116 LF 1,116 LF	1,116 1,116	0 0	0 0	0 0	0 0
Notes: Rust is beginning to form. There is scattered areas of surface pitting on the bottom cords and minor section loss with moderate pitting at the bottom panel point connections on the gusset plates and truss members (see photo 2003 FC report). Pack rust is forming at the gusset plates and batten plates on the bottom of the chords. The bolting plate @ the bottom of the 4th vert chord in the NW cor of the trusses is twisted down approx 1in. where cross brace ties in. The cross brace coming into this plate is also twisted. 3 cross bracing hanger rods are bent. The X-bracing on the SW cor of truss is also bent. Bolt chord boxes are infested with pigeons. Several interior welds of the lower chord box members were inspected after blasting & cleaning-no defects were noted. There are some nuts missing on diag bracing hanger rods. Two broken hanger rods 1 at MN (east) Pier, 1 at ND (west) pier. ***The lower chord was blasted & painted in 1996. **A crack was detected by the FC inspectors on 9/12/07 @ SW corner of truss (gusset plate) @ lower cord. Consulted w/CO & was instructed to grind out crack and prime & apply Dow 888 to prevent rusting. Continue to monitor next 3 & 6 mos. Re-inspect in December 07 & again in March of 08. DSH.***Ground out crack was re-inspected on 11/19/07 by DSH and found to have no further propagation.									
126	P/STL THRU TRUSS/TOP	2	05-09-2007 05-08-2006	1,116 LF 1,116 LF	1,116 1,116	0 0	0 0	0 0	0 0
Notes: Rust Beginning to Form. Minimal sect loss on top chord verticals & diagonals. Pigeons nesting in upper chord box members. There are broken welds on the angle stiffeners on top of the inside gusset plates (deck height) @ the 1st panel points W of the NE & SE end posts. ***The through trusses were blasted & painted in 1996. ***									
152	PAINT STL FLOORBEAM	2	05-09-2007 05-08-2006	1,380 LF 1,380 LF	690 690	690 690	0 0	0 0	0 0
Notes: Rust Beginning to Form. Rust Beginning to Form. Rust stains on top flange of Flr Bm @ E pier. ***Floor beams were blasted & painted in 1996*** Top Flanges of the floor beam are rusting.									
161	PIN & HANGER-PAINTED	2	05-09-2007 05-08-2006	56 EA 56 EA	56 56	0 0	0 0	0 0	0 0
Notes: Rust Beginning to Form. Crack in Tack Weld on Nut to Hanger bottom pin 4th beam from north, 4th bent from the east. 2003 ultrasonic with no indications.									
311	EXPANSION BEARING	2	05-09-2007 05-08-2006	148 EA 148 EA	146 146	0 0	2 2	N/A N/A	N/A N/A
Notes: SW rocker is tipped all of the way toward the west. East rockers tipped slightly to the E. Base plates 3rd Beam from the N. @ E. expansion jt. & 3rd Beam from S. or N side @ W. expansion all are fractured. Bearings @ piers 6, 7, & 8 have been blasted & painted. Rockers need adjusting. W. Pier rockers tipped away from river @ 40 degrees Base plate on No. one beam @ W. finger jt. also fractured on inside face. Two west bents have dirt piled up around the lower rockers, should be cleaned and greased. Bearings and pins need cleaning and greasing. Bearing holder plate is broken loose, crack between beam and Bearing Holder east finger Jt.									
313	FIXED BEARING	2	05-09-2007 05-08-2006	18 EA 18 EA	18 18	0 0	0 0	N/A N/A	N/A N/A
Notes: Abutment Bearings have been blasted and painted.									
202	PAINT STL COLUMN	2	05-09-2007 05-08-2006	72 EA 72 EA	36 36	18 18	18 18	0 0	0 0
Notes: Four cotter keys missing 4th bent from the west, two cotter keys missing at the south facial beam 4th bent from the east. There appears to be a dip at the joint above the second bent from the west. Is this bent settled? Needs an evaluation.									
210	CONCRETE PIER WALL	2	05-09-2007 05-08-2006	210 LF 210 LF	210 210	0 0	0 0	0 0	N/A N/A
Notes: Cracks in Pier walls in the E & W piers. There is 6 feet of debris and soft silt at the bottom of the pier - 2004 underwater inspection.									
215	CONCRETE ABUTMENT	2	05-09-2007 05-08-2006	140 LF 140 LF	140 140	0 0	0 0	0 0	N/A N/A
Notes: Minor Hairline cracks @ W. abut. 1 sq. ft. of spall & deteriorated concrete @ S. end of W. Br/wall. 6 in X 6 in. X 2 in. deep spall in W. conc. flr. Bm @ S. end. Patch is coming out of conc. flr. Bm. @ N. end of SW. Bm. Water leaking through poured joint over parapets some cracking w/leaching of E. parapet. Horz. crack in S. half of W b/wall. Small spall in top of E. br./wall w/rebar exposed.									

Mn/DOT BRIDGE RATING AND LOAD POSTING REPORT
FOR TRUNK HIGHWAYSBridge Location and Description

Hwy. No. 2 over RED RIVER + CITY ST.
 Year Built 1963 Year Remodeled _____ Replaces Br. _____
 Type 303 County POLK Ref. Pt. _____
 Description 2 TRUSS SPANS, 11 APPROACH SPANS, NO SKEW, TWO 28'-0" ROADWAYS,
CONG. PARAPET BASE W/ 2 LINES OF METAL PIPE RAILING, NO SIDEWALKS, 4'-0" MEDIAN
 Location EAST GRAND FORKS

Bridge No. 9090Data for Basis of Report (Check all that apply.)

- Bridge Inventory File
 Previous Bridge Rating and Load Posting Report
 Bridge Plans
 - New Overlay (1/4" SCARIFY AND 2" OVERLAY IN 1984)
 - Repair/Reconstruction _____
 - Other Dead Load Modifications _____ Bridge Inspection Report, by _____, date _____
 - Damaged Component _____
 - Deteriorated Component _____

Type of Analysis:

- Manual Computer* BARS Virtis, V.5.6.0 Other*

* TRUSS ANALYZED USING TRAP SOFTWARE
VIRTIS USED FOR FLOOR SYSTEM

Method of Rating (Check appropriate box)

- Load Factor (LF)
 Allowable Stress (AS)
 Load & Resistance Factor (LRFR)
 Load Testing
 No Rating Computations performed

Design Load HS - 20Design Method ASDSummary of Rating and Load Posting Analysis

Load Posting	Required Not Required				Bridge Rating		
		TONS			Inventory	Operating	
R12-1A	<input type="checkbox"/>	/		/	15.2		25.4
R12-5	<input type="checkbox"/>	M3	M3S2	M3-3	Overweight Permit Code		
R12-X11	<input type="checkbox"/>	/	45	/	A 1	B 1	C 2

I hereby certify that this report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of Minnesota.

Signature: Jon W. SuterDate: 2/13/08Typed or Printed Name: Jon W. SUTERReg. No. 25128

1/10
 6/16
 8/22/08

Revised on March 08

BRIDGE RATING DETAILS

Bridge Type 303Bridge No. 9090Rating Method LFDDesign Load: HS-20Roadway Width 28'-0", 28'-0"Inventory Rating: 15.2 Curved, TaperedOperating Rating: 25.4Beam Spacing N/ARated RAM Checked JWS

Live Load Distribution Lane Width

Date 2/13/08Single LEVER RULE Multiple _____Sheet 2 of 5

**SEE SHEET 3 OF 5 FOR TRUSS
ELEVATION AND LABELING.**

MEMBER L6-US CONTROLS

BEAM ELEVATION ②

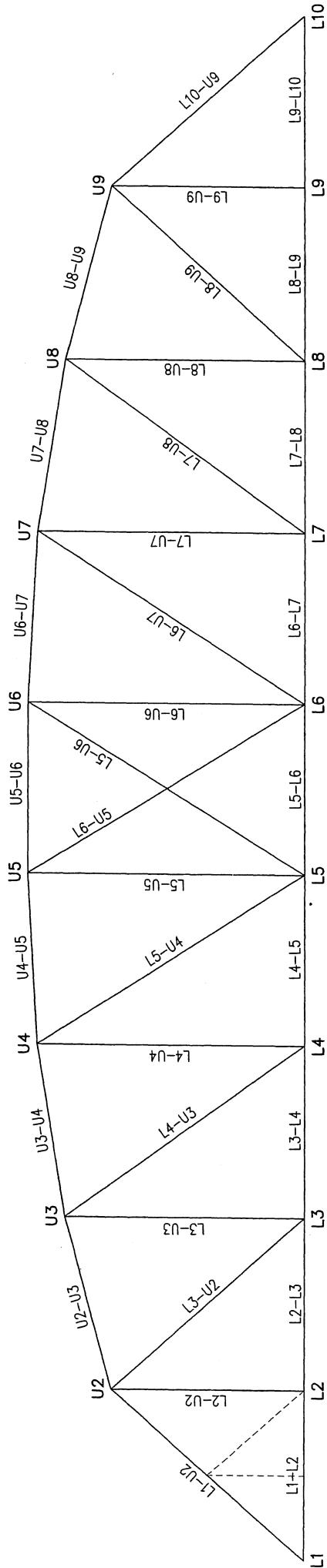
Show span lengths, structure / beam depths.

Truck	Rating Factor	Location	Limit State ①	Notes / Comments
HS 20 Inventory	0.76	1.0	COMPRESSION	
HS 20 Operating	1.27			
Standard A	1.16			
Standard B	1.04			
Standard C ③	0.98			
Standard P 411 ③	0.95			
Standard P 413 ③	0.91	↓	↓	

① Choose from: service or ultimate; shear or moment

② Elevation may be on back or another sheet if it won't fit here.

③ If the bridge needs posting, change these trucks to the posting trucks.



Form TusssR		Bridge Rating Details		Bridge No: 9090
		Rated RAM		Date 2/13/08
		Checked JWS		Sheet 4 of 5
Member	Inventory	Operating	Location / Comments	
Stringer				
FASCIA	1.25	2.09		
INTERIOR	1.06	1.78		
Floor Beam				
END F.B. 1	1.54	2.57		
INT. F.B.'S	0.92	1.54		
END F.B. 10	1.52	2.54		
Truss				
L1-L2	8.01	13.36		
L2-L3	2.71	4.53		
L3-L4	1.12	1.87		
L4-L5	1.13	1.88		
L5-L6	1.18	1.97		
L6-L7	1.13	1.89		
L7-L8	1.13	1.89		
L8-L9	2.28	3.80		
L9-L0	2.28	3.80		
U2-U3	1.23	2.06		
U3-U4	1.10	1.84		
U4-U5	1.19	1.98		
U5-U6	1.20	2.00		
U6-U7	1.19	1.99		
U7-U8	1.11	1.85		
U8-U9	1.25	2.08		
L2-U2	3.36	5.62		
L3-U3	2.22	3.71		
L4-U4	3.60	6.01		
L5-U5	4.64	7.74		
L6-U6	24.26	40.49		
L7-U7	3.57	5.95		
L8-U8	2.20	3.67		

Mn/DOT Structure Inventory Report

Bridge ID: 9090 US 2 over RED RIVER & CITY ST

Date: 02/22/2008

+ G E N E R A L +		+ R O A D W A Y +		+ I N S P E C T I O N +	
Agency Br. No.		Bridge Match ID (TIS) 1		Deficient Status ADEQ	
District 2	Maint. Area 2B	Roadway O/U Key 1-ON		Sufficiency Rating 83.4	
County 60 - POLK		Route Sys/Nbr USTH 2		Last Inspection Date 05-09-2007	
City EAST GRAND FORKS		Roadway Name or Description US 2		Inspection Frequency 12	
Township		Roadway Function MAINLINE		Inspector Name DISTRICT2	
Desc. Loc. AT N DAKOTA STATE LINE		Roadway Type 2 WAY TRAF		Structure A-OPEN	
Sect., Twp., Range 02 - 151N - 50W		Control Section (TH Only) 6018		+ C O N D I T I O N C O D E S +	
Latitude 47d 55m 59.78s		Ref. Point (TH Only) 000+00.000		Deck	6
Longitude 97d 02m 13.84s		Date Opened to Traffic 01-01-1963		Superstructure	7
Custodian STATE HWY		Detour Length 2 mi.		Substructure	6
Owner STATE HWY		Lanes 4 Lanes ON Bridge		Channel	7
Inspection By DISTRICT 2		ADT (YEAR) 21,500 (2004)		Culvert	N
BMU Agreement No.		HCADT 1,935		+ A P P R A I S A L R A T I N G S +	
Year Built 1963		Functional Class. URB/OTH PR ART		Structure Evaluation	6
Year Fed Rehab		+ R D W Y D I M E N S I O N S +		Deck Geometry	5
Year Remodeled		If Divided	NB-EB SB-WB	Underclearances	4
Temp		Roadway Width	28.0 ft	Waterway Adequacy	6
Plan Avail. CENTRAL		Vertical Clearance	19.9 ft	Approach Alignment	7
+ S T R U C T U R E +		Max. Vert. Clear.	19.9 ft	+ S A F E T Y F E A T U R E S +	
Service On HWY;PED		Horizontal Clear.	28.0 ft	Bridge Railing	1-MEETS STANDARDS
Service Under HWY;STREAM		Lateral Clr. - Lt/Rt		Appr. Guardrail	1-MEETS STANDARDS
Main Span Type STEEL HIGH TRUSS		Appr. Surface Width	60.0 ft	GR Transition	1-MEETS STANDARDS
Main Span Detail PARKER		Roadway Width	56.0 ft	GR Termini	1-MEETS STANDARDS
Appr. Span Type STEEL BM SPAN		Median Width	4.0 ft	+ I N D E P T H I N S P . +	
Appr. Span Detail		+ M I S C . B R I D G E D A T A +		Frac. Critical	Y 24 mo 06/2007
Skew		Structure Flared	NO	Underwater	Y 60 mo 07/2004
Culvert Type		Parallel Structure	NONE	Pinned Asbly.	Y 48 mo 06/2007
Barrel Length		Field Conn. ID	RIVETED	Spec. Feat.	
Number of Spans		Cantilever ID	PIN & HINGE	+ W A T E R W A Y +	
MAIN: 2 APPR: 11 TOTAL: 13		Foundations		Drainage Area	
Main Span Length 279.0 ft		Abut.	CONC - FTG PILE	Waterway Opening	29000 sq ft
Structure Length 1,261.0 ft		Pier	STEEL - FTG PILE	Navigation Control	NO PRMT REQD
Deck Width 65.0 ft		+ P A I N T +		Pier Protection	
Deck Material C-I-P CONCRETE		Year Painted	1996	Nav. Vert./Horz. Clr.	
Wear Surf Type LOW SLUMP CONC		Pct. Unsound	5 %	Nav. Vert. Lift Bridge Clear.	
Wear Surf Install Year 1984		Painted Area	183,102 sf	MN Scour Code	L-STBL;LOW RISK
Wear Course/Fill Depth 0.17 ft		Primer Type	OTHER	Scour Evaluation Year	1997
Deck Membrane NONE		Finish Type	URETHANE	+ C A P A C I T Y R A T I N G S +	
Deck Rebars N/A		+ B R I D G E S I G N S +		Design Load	HS20
Deck Rebars Install Year		Posted Load	NOT REQUIRED	Operating Rating	HS 35.4
Structure Area 81,965 sq ft		Traffic	NOT REQUIRED	Inventory Rating	HS 21.3
Roadway Area 70,611 sq ft		Horizontal	OBJECT MARKERS	Posting	
Sidewalk Width - L/R 2.5 ft	2.5 ft	Vertical	NOT REQUIRED	Rating Date	11-01-1995
Curb Height - L/R 0.75 ft	0.75 ft	Mn/DOT Permit Codes		A: 1	B: 1
Rail Codes - L/R 19	19			C: 1	

Overall Summary

FINAL RATING SUMMARY TABLE FOR BRIDGE NO. 9090 (USING A 95% MnDOT MODIFIER, Ψ)							COMPLETED BY: RAM		CHECKED BY: CJM	
							DATE: 03-12-08		DATE: 03-20-08	
Bridge Members	HS Inventory	HS Operating	Standard A	Standard B	Standard C	P411	P413	Type M3	Type M3-S2	Type M3-3
End Floorbeam @ L1	1.43	2.39	2.65	2.04	1.91	1.94	2.06	3.09	3.30	3.45
Int. Floorbeam @ L2-L9	0.82	1.37	1.26	1.11	1.04	0.96	1.03	1.84	1.94	1.94
End Floorbeam @ L10	1.41	2.36	2.65	2.02	1.93	1.94	2.03	3.09	3.27	3.42
Fascia Stringer	1.17	1.96	1.85	1.45	1.35	1.51	1.45	2.27	2.47	2.30
Interior Stringer	1.00	1.66	1.57	1.23	1.15	1.28	1.23	1.93	2.09	1.95
Truss (Member L6-U5)	0.80	1.34	1.22	1.10	1.03	1.00	0.96	2.01	1.54	1.46

COMPUTED BY VIRTIS
SOFTWARE

5% CRF is for truss only

Floor beams and stringers have good condition based on 2007 FCDM report, no LOS were recorded. Y6 @ 9/3/08

bridge controlled
by Truss

USING 100% MNDOT Modified

FINAL RATING SUMMARY TABLE FOR BRIDGE NO. 9090							COMPLETED BY: RAM		CHECKED BY: CJM	
							DATE: 01-31-08		DATE: 02-13-08	
Bridge Members	HS Inventory	HS Operating	Standard A	Standard B	Standard C	P411	P413	Type M3	Type M3-S2	Type M3-3
End Floorbeam @ L1	1.54	2.57	2.85	2.20	2.05	2.09	2.21	3.32	3.55	3.71
Int. Floorbeam @ L2-L9	0.92	1.54	1.41	1.24	1.16	1.07	1.15	2.06	2.18	2.17
End Floorbeam @ L10	1.52	2.54	2.85	2.17	2.08	2.09	2.18	3.32	3.51	3.67
Fascia Stringer	1.25	2.09	1.98	1.55	1.45	1.61	1.55	2.43	2.64	2.46
Interior Stringer	1.06	1.78	1.68	1.32	1.23	1.37	1.32	2.06	2.24	2.09
Truss (Member L6-U5)	0.76	1.27	1.16	1.04	0.98	0.95	0.91	1.91	1.46	1.39

COMPUTED BY VIRTIS
SOFTWARE

Used for final rating. Y6 @ 9/20/08

Yihong Gao - RE: 9090

From: "Jon Siiter" <Jon.Siiter@lhbcorp.com>
To: "Yihong Gao" <Yihong.Gao@dot.state.mn.us>
Date: 9/3/2008 9:05 AM
Subject: RE: 9090
CC: "Joe Litman" <Joe.Litman@lhbcorp.com>

Hi, Yihong. Regarding your question on Bridge 9090 (Kennedy Bridge in East Grand Forks): We believe those additional members were fabricated in the position shown as a temporary bearing location at L 1/2 to aid in field erection of the bridge. In fact, we modeled the truss with support at L ½ & L 0' and were able to match the loads in the truss members very closely. With supports at L 0 and L 0' (as the truss exists currently), there is very little load in those additional members. It appears the design intent was for symmetrical behavior in the final position.

If you look through the old plans you will notice that the adjacent members (bottom chord from L 0 to L 1, for instance) are much heavier than their counterparts on the opposite end of the bridge. Since the bridge is mostly geometrically symmetrical it behaves symmetrical when the supports are at L 0 & L 0'. Leaving those additional members out of the final analysis gives us conservative results at the L 0 end, and the results at the L 0' end control anyway since those members are smaller sections. It also allows for symmetrical assumption for coincidental load calculations as the influence ordinates for members in similar positions are the same.

Sorry for the long explanation, but I hope this helps. You are correct in recalling that we discussed this in our meeting last spring. It was towards the end, though, and we may not have held a clear discussion at the time. Give me a call with any further questions. Thanks.

From: Yihong Gao [mailto:Yihong.Gao@dot.state.mn.us]
Sent: Wednesday, September 03, 2008 8:03 AM
To: Jon Siiter
Subject: 9090

Hi Jon,

I am making a summary for each truss bridge and working on 9090 right now. I have a question on members at mid point of L1-L2 and L1-U2. You ignore these two members in the model for DL and LL but it seems these two members were carrying the loads for original design. I think we had a discussion on this issue but can not remember what was the reason for excluding them. Do you remember the reason? Thanks

Yihong

Yihong Gao, PE
Design Engineer
Bridge Office
Minnesota Department of Transportation
T... (651)366-4492
F... (651)366-4509

FINAL RATING SUMMARY TABLE FOR BRIDGE NO. 9090 (USING A 85% MnDOT MODIFIER, α)							COMPLETED BY: RAM		CHECKED BY: CJM	
Bridge Members	HS Inventory	HS Operating	Standard A	Standard B	Standard C	P411	DATE: 03-12-08		DATE: 03-20-08	
							P413	Type M3	Type M3-S2	Type M3-3
End Floorbeam @ L1	1.22	2.03	2.26	1.74	1.62	1.65	1.75	2.62	2.81	2.93
Int. Floorbeam @ L2-L9	0.63	1.04	0.96	0.84	0.79	0.73	0.78	1.40	1.48	1.47
End Floorbeam @ L10	1.20	2.01	2.26	1.72	1.65	1.65	1.73	2.62	2.78	2.91
Fascia Stringer	0.96	1.60	1.51	1.18	1.11	1.23	1.19	1.85	2.02	1.88
Interior Stringer	0.81	1.36	1.28	1.00	0.94	1.04	1.00	1.56	1.70	1.59
Truss (Member L6-U5)	0.72	1.19	1.09	0.98	0.92	0.89	0.86	1.79	1.38	1.31

COMPUTED BY VIRTIS
SOFTWARE

LOAD AND RATING SUMMARY TABLE FOR BRIDGE NO. 9090 (USING A 95% MnDOT MODIFIER, Ψ)

PLETED BY: RAM
E: 03-12-08

HECKED BY: CJM

NOTE THAT NODE AND MEMBER LABELS DO NOT MATCH ORIGINAL PLAN - SOFTWARE USED REQUIRES FIRST NODE TO BE L1 INSTEAD OF L0. SEE ANALYSIS DATA FOR DRAWING SHOWING MEMBER/JOINT LABELS USED BELOW.

(a) Indicates the lane closest to the truss occupied by a permit truck and remaining three lanes occupied by HS traffic.

LOAD AND RATING SUMMARY TABLE FOR BRIDGE NO. 9090 (USING A 85% MnDOT MODIFIER, Ω)

COMPLETED BY: RAM

DATE: 03-12-08

CHECKED BY: CJM

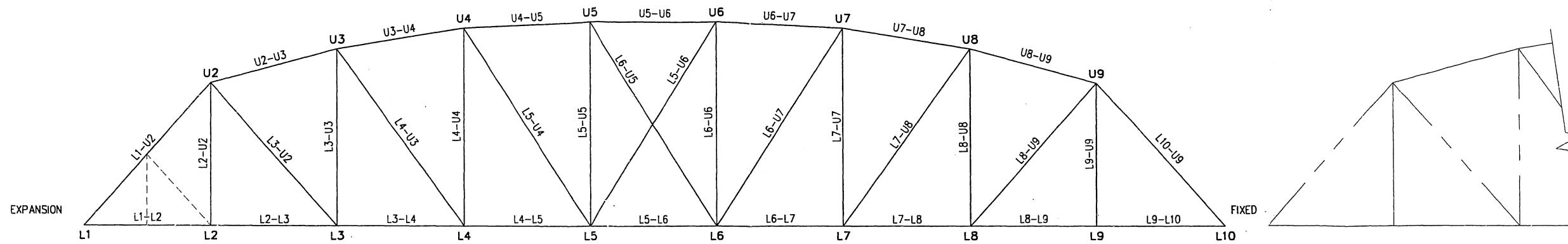
DATE: 03-20-08

NOTE THAT NODE AND MEMBER LABELS DO NOT MATCH ORIGINAL PLAN - SOFTWARE USED REQUIRES FIRST NODE TO BE L1 INSTEAD OF L0. SEE ANALYSIS DATA FOR DRAWING SHOWING MEMBER/JOINT LABELS USED BELOW.

Members	BOTTOM CHORD									TOP CHORD								VERTICAL MEMBERS								DIAGONAL MEMBERS								
	L1-L2	L2-L3	L3-L4	L4-L5	L5-L6	L6-L7	L7-L8	L8-L9	L9-L10	U2-U3	U3-U4	U4-U5	U5-U6	U6-U7	U7-U8	U8-U9	L2-U2	L3-U3	L4-U4	L5-U5	L6-U6	L7-U7	L8-U8	L9-U9	L1-U2	L3-U2	L4-U3	L5-U4	L5-U6	L6-U5	L6-U7	L7-U8	L8-U9	L10-U9
Gross Area (in ²)	114.50	58.25	58.25	67.25	73.25	67.25	58.25	58.25	67.25	73.25	79.25	79.25	79.25	73.25	67.25	28.22	28.22	28.22	28.22	28.22	28.22	28.22	28.22	73.25	41.01	22.63	18.80	18.80	18.80	18.80	18.80	28.22	73.25	
Net Area (in ²)	107.50	49.38	49.38	56.88	61.88	56.88	49.38	49.38	67.25	73.25	79.25	79.25	79.25	73.25	67.25	28.22	28.22	28.22	24.90	24.90	28.22	28.22	24.90	73.25	31.60	19.31	16.06	16.06	16.06	16.06	16.06	24.90	73.25	
Steel Yield Strength (ksi)	36.0	36.0	36.0	36.0	36.0	36.0	33.0	33.0	42.0	42.0	42.0	42.0	42.0	42.0	42.0	33.0	33.0	33.0	33.0	33.0	33.0	33.0	33.0	42.0	36.0	40.0	40.0	33.0	33.0	33.0	40.0	36.0	40.0	
Steel Tensile Strength (ksi)	58.0	58.0	58.0	58.0	58.0	58.0	60.0	60.0	63.0	63.0	63.0	63.0	63.0	63.0	63.0	60.0	60.0	60.0	60.0	60.0	60.0	60.0	60.0	63.0	58.0	60.0	60.0	60.0	60.0	60.0	60.0	58.0	63.0	
KL/r	55.61	42.49	42.49	41.75	42.33	41.75	42.49	42.49	43.23	42.87	42.01	41.95	42.01	42.87	43.23	77.49	95.94	107.01	110.70	110.70	107.01	95.94	77.49	63.83	101.64	161.45	178.51	182.90	182.90	178.51	165.64	103.52	63.83	
Impact	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.267	1.300	1.250	1.217	1.145	1.250	1.300	1.267	1.124	1.138	1.152	1.168	1.189	1.189	1.168	1.152	1.138	1.124	
Service Dead Load (kips)	735.90	735.90	1036.00	1193.50	1282.30	1190.90	1031.60	729.60	729.60	-1072.80	-1208.90	-1284.20	-1281.50	-1283.40	-1206.30	-1068.20	179.50	-162.30	-44.00	40.50	39.20	-47.10	-165.40	172.70	-1109.90	452.70	270.60	164.50	0.00	-1.50	167.70	273.90	455.40	-1100.50
Service Live Load + Impact (kips)																																		
HS-20 (max.)	159.08	159.08	224.87	259.20	278.39	259.20	224.87	159.08	159.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	114.57	66.53	71.08	68.76	15.00	71.08	66.53	114.57	0.00	124.26	99.45	90.80	0.00	73.64	90.80	99.45	124.26	0.00
HS-20 (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-232.84	-262.55	-278.79	-278.39	-278.79	-262.55	-232.84	0.00	-65.01	-53.94	-51.17	0.00	-53.94	-65.01	0.00	-257.81	-38.17	-56.74	-61.03	-61.03	-56.74	-38.17	-257.81	-0.00	
Standard A Truck (max.)	152.49	152.49	215.10	247.49	265.26	247.49	215.10	152.49	152.49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	118.31	71.77	78.65	77.20	14.29	78.65	77.20	118.31	0.00	120.85	100.30	95.07	0.00	80.53	95.07	100.30	120.85	0.00
Standard A Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-222.73	-250.68	-265.65	-265.26	-250.68	-222.73	0.00	-68.45	-59.53	-57.46	0.00	-59.53	-68.45	0.00	-240.96	-37.41	-60.84	-67.44	-67.44	-60.84	-37.41	-240.96	-0.00		
Standard B Truck (max.)	168.21	168.21	237.16	273.06	292.25	273.06	237.16	168.21	168.21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	124.97	78.20	87.22	86.34	15.75	78.20	87.22	124.97	0.00	133.48	111.25	105.77	0.00	89.76	105.77	111.25	133.48	0.00
Standard B Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-245.57	-276.59	-292.68	-292.25	-276.59	-245.57	0.00	-67.40	-66.71	-64.26	0.00	-66.71	-76.40	0.00	-264.67	-39.11	-66.04	-74.68	-74.68	-66.04	-39.11	-264.67	-0.00		
Standard C Truck (max.)	178.80	178.80	252.17	290.14	310.38	290.14	252.17	178.80	178.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	128.75	81.24	92.53	92.13	16.72	92.53	81.24	128.75	0.00	141.90	118.41	112.60	0.00	95.40	112.60	118.41	141.90	0.00
Standard C Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-261.11	-293.89	-310.83	-310.38	-293.89	-261.11	0.00	-81.61	-71.30	-68.42	0.00	-71.30	-81.61	0.00	-280.64	-40.79	-68.62	-79.00	-79.00	-68.62	-40.79	-280.64	-0.00		
P411 Truck (max.)	194.90	194.90	274.55	313.64	334.41	313.64	274.55	194.90	194.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	133.83	76.90	91.49	95.71	18.02	91.49	76.90	133.83	0.00	153.38	127.03	119.22	0.00	98.72	119.22	127.03	153.38	0.00
P411 Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-284.29	-317.68	-334.90	-334.41	-334.90	-284.29	0.00	-87.88	-75.64	-70.47	0.00	-75.64	-87.88	0.00	-304.93	-42.21	-64.73	-77.62	-77.62	-64.73	-42.21	-304.93	-0.00		
P413 Truck (max.)	211.13	211.13	296.00	338.77	362.16	338.77	296.00	211.13	211.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	129.39	79.24	92.36	99.19	19.51	92.36</td												

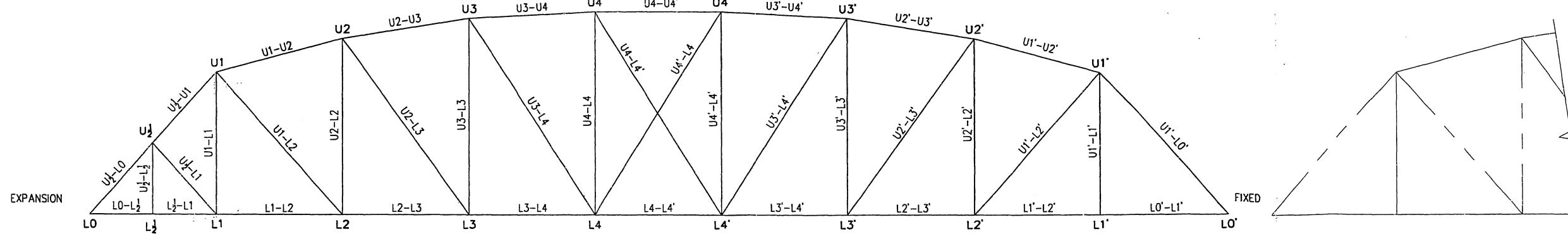
USING 100% MN DOT MODIFIER

LOAD AND RATING SUMMARY TABLE FOR BRIDGE NO. 9090																			COMPLETED BY: RAM				CHECKED BY: CJM														
																			DATE: 01-31-08				DATE: 02-13-08														
NOTE THAT NODE AND MEMBER LABELS DO NOT MATCH ORIGINAL PLAN - SOFTWARE USED REQUIRES FIRST NODE TO BE L1 INSTEAD OF L0. SEE ANALYSIS DATA FOR DRAWING SHOWING MEMBER/JOINT LABELS USED BELOW.																																					
Members	L1-L2	L2-L3	L3-L4	L4-L5	L5-L6	L6-L7	L7-L8	L8-L9	L9-L10	U2-U3	U3-U4	U4-U5	U5-U6	U6-U7	U7-U8	U8-U9	L2-U2	L3-U3	L4-U4	L5-U5	L6-U6	L7-U7	L8-U8	L9-U9	L1-U2	L3-U2	L4-U3	L5-U4	L5-U6	L6-U5	L6-U7	L7-U8	L8-U9	L10-U9			
Gross Area (in ²)	114.50	58.25	58.25	67.25	73.25	67.25	58.25	58.25	67.25	73.25	79.25	79.25	79.25	79.25	73.25	67.25	28.22	28.22	28.22	28.22	28.22	28.22	28.22	28.22	73.25	41.01	22.63	18.80	18.80	18.80	18.80	18.80	18.80	28.22	73.25		
Net Area (in ²)	107.50	49.38	49.38	56.88	61.88	56.88	49.38	49.38	67.25	73.25	79.25	79.25	79.25	79.25	73.25	67.25	28.22	28.22	28.22	24.90	24.90	28.22	28.22	24.90	73.25	31.60	19.31	16.06	16.06	16.06	16.06	16.06	16.06	24.90	73.25		
Steel Yield Strength (ksi)	36.0	36.0	36.0	36.0	36.0	36.0	33.0	33.0	42.0	42.0	42.0	42.0	42.0	42.0	42.0	42.0	33.0	33.0	33.0	33.0	33.0	33.0	33.0	33.0	42.0	36.0	40.0	40.0	33.0	33.0	40.0	36.0	40.0				
Steel Tensile Strength (ksi)	58.0	58.0	58.0	58.0	58.0	58.0	60.0	60.0	63.0	63.0	63.0	63.0	63.0	63.0	63.0	63.0	60.0	60.0	60.0	60.0	60.0	60.0	60.0	60.0	63.0	58.0	60.0	60.0	60.0	60.0	60.0	60.0	63.0				
KL/r	55.61	42.49	42.49	41.75	42.33	41.75	42.49	42.49	43.23	42.87	42.01	41.95	42.01	42.87	43.23	77.49	95.94	107.01	110.70	110.70	107.01	95.94	77.49	63.83	101.64	161.45	178.51	182.90	182.90	178.51	165.64	103.52	63.83				
Impact	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.124	1.267	1.300	1.250	1.217	1.145	1.250	1.300	1.267	1.124	1.138	1.152	1.168	1.189	1.168	1.152	1.138	1.124					
Service Dead Load (kips)	735.90	735.90	1036.00	1193.50	1282.30	1190.90	1031.60	729.60	729.60	-1072.80	-1208.90	-1284.20	-1281.50	-1283.40	-1206.30	-1068.20	179.50	-162.30	-44.00	40.50	39.20	-47.10	-165.40	172.70	-1109.90	452.70	270.60	164.50	0.00	-1.50	167.70	273.90	455.40	-1100.50			
Service Live Load + Impact (kips)																																					
HS-20 (max.)	159.08	159.08	224.87	259.20	278.39	259.20	224.87	159.08	159.08	0.00	0.00	0.00	0.00	-232.84	-262.55	-278.79	-278.79	-262.55	-232.84	0.00	-65.01	-53.94	-51.17	0.00	-53.94	-65.01	0.00	-257.81	-38.17	-56.74	-61.03	0.00	-73.64	90.80	99.45	124.26	0.00
HS-20 (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-232.84	-262.55	-278.79	-278.79	-262.55	-232.84	0.00	-65.01	-53.94	-51.17	0.00	-53.94	-65.01	0.00	-257.81	-38.17	-56.74	-61.03	0.00	-73.64	90.80	99.45	124.26	0.00				
Standard A Truck (max.)	152.49	152.49	215.10	247.49	265.26	247.49	215.10	152.49	152.49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	118.31	71.77	78.65	77.20	14.29	78.65	71.77	118.31	0.00	120.85	100.30	95.07	0.00	80.53	95.07	100.30	120.85	0.00			
Standard A Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-222.73	-250.68	-265.65	-265.65	-250.68	-222.73	0.00	-68.45	-59.53	-57.46	0.00	-59.53	-68.45	0.00	-240.96	-37.41	-60.84	-67.44	0.00	-80.53	95.07	100.30	120.85	0.00				
Standard B Truck (max.)	168.21	168.21	237.16	273.06	292.25	273.06	237.16	168.21	168.21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	124.97	78.20	87.22	86.34	15.75	87.22	78.20	124.97	0.00	133.48	111.25	105.77	0.00	89.76	105.77	111.25	133.48	0.00			
Standard B Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-245.57	-276.59	-292.68	-292.68	-276.59	-245.57	0.00	-66.71	-64.26	-60.00	0.00	-66.71	-76.40	0.00	-264.67	-39.11	-66.04	-74.68	0.00	-89.76	105.77	111.25	133.48	0.00				
Standard C Truck (max.)	178.80	178.80	252.17	290.14	310.38	290.14	252.17	178.80	178.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	128.75	81.24	92.53	92.13	16.72	92.53	81.24	128.75	0.00	141.90	112.60	95.40	0.00	118.41	141.90	128.75	141.90	0.00			
Standard C Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-261.11	-293.89	-310.83	-310.83	-293.89	-261.11	0.00	-81.61	-71.30	-68.42	0.00	-71.30	-81.61	0.00	-280.64	-40.79	-68.62	-79.00	0.00	-95.40	-79.00	-68.62	-40.79	-280.64				
P411 Truck (max.)	194.90	194.90	274.55	313.64	334.41	313.64	274.55	194.90	194.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	133.83	76.90	91.49	95.71	18.02	91.49	76.90	133.83	0.00	153.38	127.03	119.22	0.00	98.72	119.22	127.03	153.38	0.00			
P411 Truck (min.)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-284.29	-317.68	-334.41	-334.41	-317.68	-284.29	0.00	-88.88	-75.64	-70.47	0.00	-75.64	-88.88	0.00	-304.93	-42.21	-64.73	-77.62	0.00	-98.72	-77.62	-64.73	-42.21	-304.93				
P413 Truck (max.)	211.13	211.13	296.00	338.77	362.16	338.77	296.00	211.13	211.13	0.00	0.00	0.00																									



BRIDGE NO. 9090 - TRUSS MEMBER AND JOINT LABELS USED IN RATING ANALYSIS

SCALE: 0 15'



BRIDGE NO. 9090 - TRUSS MEMBER AND JOINT LABELS USED IN ORIGINAL PLAN

SCALE: 0 15'

TITLE:
TRUSS ELEVATION

DES: RAM	DR: RAM	APPROVED:
CHK: JWS	CHK: JWS	
Sheet No. 1 of 1 Sheet		

Bridge No.
9090

Memoranda

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TABLE 1.6 MEMBER DATA

MEM NO	LCTN FRM	MEM TO REL	LOADED MEM			MEM DEPTH (IN)	MEMBER AREA				YIELD STRSS (ksi)	INF LIN OPT	EFF LNG FAC	TEMP CHNG	
			SEQ	DEK	LCN		GYZRATON (IN)	GROSS (SQIN)	NET						
1	L	1	L	2	0	1	0.00	6.02	26.50	114.5	0.0	36.0	1	0.90	0.0
2	L	2	L	3	0	0	0.00	7.88	24.75	58.3	0.0	36.0	1	0.90	0.0
3	L	3	L	4	0	0	0.00	7.88	24.75	58.3	0.0	36.0	1	0.90	0.0
4	L	4	L	5	0	0	0.00	8.02	24.75	67.2	0.0	36.0	1	0.90	0.0
5	L	5	L	6	0	0	0.00	7.91	24.75	73.3	0.0	36.0	1	0.90	0.0
6	L	6	L	7	0	0	0.00	8.02	24.75	67.2	0.0	36.0	1	0.90	0.0
7	L	7	L	8	0	0	0.00	7.88	24.75	58.3	0.0	36.0	1	0.90	0.0
8	L	8	L	9	0	0	0.00	7.88	24.75	58.3	0.0	33.0	1	0.90	0.0
9	L	9	L	10	0	0	0.00	7.88	24.75	58.3	0.0	33.0	1	0.90	0.0
10	U	2	U	3	0	0	0.00	8.02	25.25	67.2	0.0	42.0	1	0.90	0.0
11	U	3	U	4	0	0	0.00	7.91	25.25	73.3	0.0	42.0	1	0.90	0.0
12	U	4	U	5	0	0	0.00	7.98	25.25	79.2	0.0	42.0	1	0.90	0.0
13	U	5	U	6	0	0	0.00	7.98	25.25	79.2	0.0	42.0	1	0.90	0.0
14	U	6	U	7	0	0	0.00	7.98	25.25	79.2	0.0	42.0	1	0.90	0.0
15	U	7	U	8	0	0	0.00	7.91	25.25	73.3	0.0	42.0	1	0.90	0.0
16	U	8	U	9	0	0	0.00	8.02	25.25	67.2	0.0	42.0	1	0.90	0.0
17	L	2	U	2	0	2	0.00	2.71	18.16	28.2	0.0	42.0	1	0.50	0.0
18	L	3	U	3	0	3	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
19	L	4	U	4	0	4	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
20	L	5	U	5	0	5	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
21	L	6	U	6	0	6	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
22	L	7	U	7	0	7	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
23	L	8	U	8	0	8	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
24	L	9	U	9	0	9	0.00	2.71	18.16	28.2	0.0	33.0	1	0.50	0.0
25	L	1	U	2	0	0	0.00	7.91	25.25	73.3	0.0	42.0	1	0.90	0.0
26	L	3	U	2	0	0	0.00	2.76	18.48	41.0	0.0	36.0	1	0.50	0.0
27	L	4	U	3	0	0	0.00	1.98	18.16	22.6	0.0	40.0	1	0.50	0.0
28	L	5	U	4	0	0	0.00	1.93	17.87	18.8	0.0	40.0	1	0.50	0.0
29	L	5	U	6	1	0	0.00	1.93	17.87	18.8	0.0	33.0	1	0.50	0.0
30	L	6	U	5	0	0	0.00	1.93	17.87	18.8	0.0	33.0	1	0.50	0.0
31	L	6	U	7	0	0	0.00	1.93	17.87	18.8	0.0	33.0	1	0.50	0.0
32	L	7	U	8	0	0	0.00	1.93	17.87	18.8	0.0	40.0	1	0.50	0.0
33	L	8	U	9	0	0	0.00	2.71	18.16	28.2	0.0	36.0	1	0.50	0.0
34	L	10	U	9	0	10	0.00	7.91	25.25	73.3	0.0	42.0	1	0.90	0.0

Allowable force
summary

TABLE 15.1 ALLOWABLE FORCE SUMMARY FOR LOWER CHORD MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	POSTING	POSTING
	AASHTO	AASHTO	STA. VEH.	SPE. TR.
	TENS. COMP.	TENS. COMP.	TENS. COMP.	TENS. COMP.
L 1 L 2	4122.00	4122.00	4122.00	4122.00
	3162.94	3162.94	3162.94	3162.94
L 2 L 3	2097.00	2097.00	2097.00	2097.00
	1681.28	1681.28	1681.28	1681.28
L 3 L 4	2097.00	2097.00	2097.00	2097.00
	1681.28	1681.28	1681.28	1681.28
L 4 L 5	2421.00	2421.00	2421.00	2421.00
	1945.09	1945.09	1945.09	1945.09
L 5 L 6	2637.00	2637.00	2637.00	2637.00
	2115.19	2115.19	2115.19	2115.19
L 6 L 7	2421.00	2421.00	2421.00	2421.00
	1945.09	1945.09	1945.09	1945.09
L 7 L 8	2097.00	2097.00	2097.00	2097.00
	1681.28	1681.28	1681.28	1681.28
L 8 L 9	1922.25	1922.25	1922.25	1922.25
	1548.90	1548.90	1548.90	1548.90
L 9 L10	1922.25	1922.25	1922.25	1922.25
	1548.90	1548.90	1548.90	1548.90

TABLE 15.2 ALLOWABLE FORCE SUMMARY FOR UPPER CHORD MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	POSTING	POSTING
	AASHTO	AASHTO	STA. VEH.	SPE. TR.
	TENS. COMP.	TENS. COMP.	TENS. COMP.	TENS. COMP.
U 2 U 3	2824.50 2236.26	2824.50 2236.26	2824.50 2236.26	2824.50 2236.26
U 3 U 4	3076.50 2438.69	3076.50 2438.69	3076.50 2438.69	3076.50 2438.69
U 4 U 5	3328.50 2646.00	3328.50 2646.00	3328.50 2646.00	3328.50 2646.00
U 5 U 6	3328.50 2646.53	3328.50 2646.53	3328.50 2646.53	3328.50 2646.53
U 6 U 7	3328.50 2646.00	3328.50 2646.00	3328.50 2646.00	3328.50 2646.00
U 7 U 8	3076.50 2438.69	3076.50 2438.69	3076.50 2438.69	3076.50 2438.69
U 8 U 9	2824.50 2236.26	2824.50 2236.26	2824.50 2236.26	2824.50 2236.26

TABLE 15.4 ALLOWABLE FORCE SUMMARY FOR VERTICAL MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	POSTING	POSTING
	AASHTO	AASHTO	STA. VEH.	SPE. TR.
	TENS. COMP.	TENS. COMP.	TENS. COMP.	TENS. COMP.
L 2 U 2B	1185.24 785.53	1185.24 785.53	1185.24 785.53	1185.24 785.53
L 3 U 3B	931.26 581.59	931.26 581.59	931.26 581.59	931.26 581.59
L 4 U 4B	931.26 530.33	931.26 530.33	931.26 530.33	931.26 530.33
L 5 U 5B	931.26 511.96	931.26 511.96	931.26 511.96	931.26 511.96
L 6 U 6B	931.26 511.96	931.26 511.96	931.26 511.96	931.26 511.96

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TABLE 15.4 ALLOWABLE FORCE SUMMARY FOR VERTICAL MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	POSTING	POSTING
	AASHTO	AASHTO	STA. VEH.	SPE. TR.
	TENS. COMP.	TENS. COMP.	TENS. COMP.	TENS. COMP.
L 7 U 7B	931.26 530.33	931.26 530.33	931.26 530.33	931.26 530.33
L 8 U 8B	931.26 581.59	931.26 581.59	931.26 581.59	931.26 581.59
L 9 U 9B	931.26 654.57	931.26 654.57	931.26 654.57	931.26 654.57

TABLE 15.5 ALLOWABLE FORCE SUMMARY FOR DIAGONAL MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	POSTING	POSTING
	AASHTO	AASHTO	STA. VEH.	SPE. TR.
	TENS. COMP.	TENS. COMP.	TENS. COMP.	TENS. COMP.
L 1 U 2	3076.50	3076.50	3076.50	3076.50
	2224.09	2224.09	2224.09	2224.09
U 2 L 3	1476.36	1476.36	1476.36	1476.36
	847.25	847.25	847.25	847.25
U 3 L 4	905.20	905.20	905.20	905.20
	211.22	211.22	211.22	211.22
U 4 L 5	752.00	752.00	752.00	752.00
	143.55	143.55	143.55	143.55
L 5 U 6	620.40	620.40	620.40	620.40
	136.74	136.74	136.74	136.74
U 5 L 6	620.40	620.40	620.40	620.40
	136.74	136.74	136.74	136.74
L 6 U 7	620.40	620.40	620.40	620.40
	143.55	143.55	143.55	143.55
L 7 U 8	752.00	752.00	752.00	752.00
	166.73	166.73	166.73	166.73
L 8 U 9	1015.92	1015.92	1015.92	1015.92
	572.57	572.57	572.57	572.57
U 9 L10	3076.50	3076.50	3076.50	3076.50
	2224.09	2224.09	2224.09	2224.09

Service Dead Loads

TABLE 3.9 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN LOWER CHORD (UNFACTORED)

MEMBER	TOTAL STEEL		TOTAL DEAD LOAD	
	FORCE (K)	ADJ LENGTH (FT)	FORCE (K)	ADJ LENGTH (FT)
L 1 L 2	735.9	31.0069	735.9	31.0069
L 2 L 3	735.9	31.0135	735.9	31.0135
L 3 L 4	1036.0	31.0190	1036.0	31.0190
L 4 L 5	1193.5	31.0190	1193.5	31.0190
L 5 L 6	1282.3	31.0187	1282.3	31.0187
L 6 L 7	1190.9	31.0189	1190.9	31.0189
L 7 L 8	1031.6	31.0189	1031.6	31.0189
L 8 L 9	729.6	31.0134	729.6	31.0134
L 9 L 10	729.6	31.0134	729.6	31.0134

TABLE 3.10 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN UPPER CHORD (UNFACTORIED)

MEMBER	TOTAL STEEL		TOTAL DEAD LOAD	
	FORCE (K)	ADJ LENGTH (FT)	FORCE (K)	ADJ LENGTH (FT)
U 2 U 3	-1072.8	32.0820	-1072.8	32.0820
U 3 U 4	-1208.9	31.3828	-1208.9	31.3828
U 4 U 5	-1284.2	31.0276	-1284.2	31.0276
U 5 U 6	-1281.5	30.9827	-1281.5	30.9827
U 6 U 7	-1283.4	31.0276	-1283.4	31.0276
U 7 U 8	-1206.3	31.3828	-1206.3	31.3828
U 8 U 9	-1068.2	32.0821	-1068.2	32.0821

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TABLE 3.12 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN VERT. MEMBERS (UNFACTORED)

MEMBER	TOTAL STEEL			TOTAL DEAD LOAD		
	FORCE		ADJ LENGTH	FORCE		ADJ LENGTH
	TOP (K)	BOTTOM (K)	(FT)	TOP (K)	BOTTOM (K)	(FT)
L 2 U 2	179.5	179.5	34.9923	179.5	179.5	34.9923
L 3 U 3	-162.3	-162.3	43.3386	-162.3	-162.3	43.3386
L 4 U 4	-44.0	-44.0	48.3326	-44.0	-44.0	48.3326
L 5 U 5	40.5	40.5	49.9975	40.5	40.5	49.9975
L 6 U 6	39.2	39.2	49.9976	39.2	39.2	49.9976
L 7 U 7	-47.1	-47.1	48.3328	-47.1	-47.1	48.3328
L 8 U 8	-165.4	-165.4	43.3388	-165.4	-165.4	43.3388
L 9 U 9	172.7	172.7	34.9926	172.7	172.7	34.9926

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TABLE 3.13 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN DIAG. MEMBERS (UNFACTORIED)

MEMBER	TOTAL STEEL		TOTAL DEAD LOAD	
	FORCE (K)	ADJ LENGTH (FT)	FORCE (K)	ADJ LENGTH (FT)
L 1 U 2	-1109.9	46.7303	-1109.9	46.7303
U 2 L 3	452.7	46.7725	452.7	46.7725
U 3 L 4	270.6	53.2994	270.6	53.2994
U 4 L 5	164.5	57.4350	164.5	57.4350
L 5 U 6	0.0	58.8303	0.0	58.8303
U 5 L 6	-1.5	58.8301	-1.5	58.8301
L 6 U 7	167.7	57.4353	167.7	57.4353
L 7 U 8	273.9	53.3042	273.9	53.3042
L 8 U 9	455.4	46.7807	455.4	46.7807
U 9 L 10	-1100.5	46.7305	-1100.5	46.7305

Service Line Loads

TABLE 5.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORIED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	141.56	159.08	L	0.00	0.00	
L 2 L 3	141.56	159.08	L	0.00	0.00	
L 3 L 4	200.10	224.87	L	0.00	0.00	
L 4 L 5	230.66	259.20	L	0.00	0.00	
L 5 L 6	247.73	278.39	L	0.00	0.00	
L 6 L 7	230.66	259.20	L	0.00	0.00	
L 7 L 8	200.10	224.87	L	0.00	0.00	
L 8 L 9	141.56	159.08	L	0.00	0.00	
L 9 L10	141.56	159.08	L	0.00	0.00	

TABLE 5.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00		-207.20	-232.84	L
U 3 U 4	0.00	0.00		-233.64	-262.55	L
U 4 U 5	0.00	0.00		-248.09	-278.79	L
U 5 U 6	0.00	0.00		-247.73	-278.39	L
U 6 U 7	0.00	0.00		-248.09	-278.79	L
U 7 U 8	0.00	0.00		-233.64	-262.55	L
U 8 U 9	0.00	0.00		-207.20	-232.84	L

TABLE 5.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	90.40	114.57	HS	0.00	0.00	
L 2 U 2 B	0.00	0.00		0.00	0.00	
L 3 U 3 T	51.18	66.53	HS	-57.12	-65.01	L
L 3 U 3 B	21.98	28.58	HS	-75.31	-85.71	L
L 4 U 4 T	56.86	71.08	HS	-46.80	-53.94	L
L 4 U 4 B	36.92	46.15	HS	-64.02	-73.78	L
L 5 U 5 T	56.52	68.76	HS	-43.80	-51.17	HS
L 5 U 5 B	42.23	51.37	HS	-58.96	-68.89	L
L 6 U 6 T	13.10	15.00	L	0.00	0.00	
L 6 U 6 B	8.63	9.88	L	-81.98	-104.38	HS
L 7 U 7 T	56.86	71.08	HS	-46.80	-53.94	L
L 7 U 7 B	36.92	46.15	HS	-64.02	-73.78	L
L 8 U 8 T	51.18	66.53	HS	-57.12	-65.01	L
L 8 U 8 B	21.98	28.58	HS	-75.31	-85.71	L
L 9 U 9 T	90.40	114.57	HS	0.00	0.00	
L 9 U 9 B	0.00	0.00		0.00	0.00	

TABLE 5.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00		-229.42	-257.81	L
U 2 L 3	109.18	124.26	L	-29.36	-38.17	HS
U 3 L 4	86.30	99.45	L	-45.39	-56.74	HS
U 4 L 5	77.71	90.80	L	-50.17	-61.03	HS
L 5 U 6	0.00	0.00		0.00	0.00	
U 5 L 6	61.91	73.64	L	-61.91	-73.64	L
L 6 U 7	77.71	90.80	L	-50.17	-61.03	HS
L 7 U 8	86.30	99.45	L	-45.39	-56.74	HS
L 8 U 9	109.18	124.26	L	-29.36	-38.17	HS
U 9 L10	0.00	0.00		-229.42	-257.81	L

TABLE 5.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

ASSHTO LOADING RESULTS FOR 3 LANES TO BE ADDED TO ONE LANE OF
PERMIT TRUCKS (A,B,C,P411, P413)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	86.83	97.57	L	0.00	0.00	
L 2 L 3	86.83	97.57	L	0.00	0.00	
L 3 L 4	122.74	137.93	L	0.00	0.00	
L 4 L 5	141.48	158.99	L	0.00	0.00	
L 5 L 6	151.95	170.75	L	0.00	0.00	
L 6 L 7	141.48	158.99	L	0.00	0.00	
L 7 L 8	122.74	137.93	L	0.00	0.00	
L 8 L 9	86.83	97.57	L	0.00	0.00	
L 9 L10	86.83	97.57	L	0.00	0.00	

TABLE 5.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00		-127.09	-142.82	L
U 3 U 4	0.00	0.00		-143.31	-161.04	L
U 4 U 5	0.00	0.00		-152.17	-171.00	L
U 5 U 6	0.00	0.00		-151.95	-170.75	L
U 6 U 7	0.00	0.00		-152.17	-171.00	L
U 7 U 8	0.00	0.00		-143.31	-161.04	L
U 8 U 9	0.00	0.00		-127.09	-142.82	L

TABLE 5.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	55.45	70.27	HS	0.00	0.00	
L 2 U 2 B	0.00	0.00		0.00	0.00	
L 3 U 3 T	31.39	40.81	HS	-35.03	-39.87	L
L 3 U 3 B	13.48	17.53	HS	-46.19	-52.57	L
L 4 U 4 T	34.88	43.60	HS	-28.71	-33.08	L
L 4 U 4 B	22.64	28.31	HS	-39.27	-45.25	L
L 5 U 5 T	34.67	42.17	HS	-26.86	-31.39	HS
L 5 U 5 B	25.90	31.51	HS	-36.16	-42.25	L
L 6 U 6 T	8.03	9.20	L	0.00	0.00	
L 6 U 6 B	5.29	6.06	L	-50.28	-64.02	HS
L 7 U 7 T	34.88	43.60	HS	-28.71	-33.08	L
L 7 U 7 B	22.64	28.31	HS	-39.27	-45.25	L
L 8 U 8 T	31.39	40.81	HS	-35.03	-39.87	L
L 8 U 8 B	13.48	17.53	HS	-46.19	-52.57	L
L 9 U 9 T	55.45	70.27	HS	0.00	0.00	
L 9 U 9 B	0.00	0.00		0.00	0.00	

TABLE 5.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

ASSHTO LOADING RESULTS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00		-140.72	-158.13	L
U 2 L 3	66.97	76.22	L	-18.01	-23.41	HS
U 3 L 4	52.93	61.00	L	-27.84	-34.80	HS
U 4 L 5	47.67	55.69	L	-30.77	-37.43	HS
L 5 U 6	0.00	0.00		0.00	0.00	
U 5 L 6	37.97	45.17	L	-37.97	-45.17	L
L 6 U 7	47.67	55.69	L	-30.77	-37.43	HS
L 7 U 8	52.93	61.00	L	-27.84	-34.80	HS
L 8 U 9	66.97	76.22	L	-18.01	-23.41	HS
U 9 L10	0.00	0.00		-140.72	-158.13	L

TABLE 9.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 4) STANDARD A ONE LANE TO BE ADDED TO
THREE LANES OF HS TRUCKS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	48.87	54.92	S1	0.00	0.00	S1
L 2 L 3	48.87	54.92	S1	0.00	0.00	S1
L 3 L 4	68.67	77.17	S1	0.00	0.00	S1
L 4 L 5	78.75	88.50	S1	0.00	0.00	S1
L 5 L 6	84.10	94.51	S1	0.00	0.00	S1
L 6 L 7	78.75	88.50	S1	0.00	0.00	S1
L 7 L 8	68.67	77.17	S1	0.00	0.00	S1
L 8 L 9	48.87	54.92	S1	0.00	0.00	S1
L 9 L10	48.87	54.92	S1	0.00	0.00	S1

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TABLE 9.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	S1	-71.11	-79.91	S1
U 3 U 4	0.00	0.00	S1	-79.77	-89.64	S1
U 4 U 5	0.00	0.00	S1	-84.23	-94.65	S1
U 5 U 6	0.00	0.00	S1	-84.10	-94.51	S1
U 6 U 7	0.00	0.00	S1	-84.23	-94.65	S1
U 7 U 8	0.00	0.00	S1	-79.77	-89.64	S1
U 8 U 9	0.00	0.00	S1	-71.11	-79.91	S1

TABLE 9.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	37.90	48.04	S1	0.00	0.00	S1
L 2 U 2 B	0.00	0.00	S1	0.00	0.00	S1
L 3 U 3 T	23.82	30.96	S1	-25.11	-28.58	S1
L 3 U 3 B	8.06	10.48	S1	-29.36	-33.41	S1
L 4 U 4 T	28.04	35.05	S1	-22.95	-26.45	S1
L 4 U 4 B	16.95	21.18	S1	-27.74	-31.97	S1
L 5 U 5 T	28.80	35.03	S1	-22.31	-26.07	S1
L 5 U 5 B	20.76	25.26	S1	-28.37	-33.15	S1
L 6 U 6 T	4.45	5.09	S1	0.00	0.00	S1
L 6 U 6 B	3.38	3.87	S1	-33.43	-42.56	S1
L 7 U 7 T	28.04	35.05	S1	-22.95	-26.45	S1
L 7 U 7 B	16.95	21.18	S1	-27.74	-31.97	S1
L 8 U 8 T	23.82	30.96	S1	-25.11	-28.58	S1
L 8 U 8 B	8.06	10.48	S1	-29.36	-33.41	S1
L 9 U 9 T	37.90	48.04	S1	0.00	0.00	S1
L 9 U 9 B	0.00	0.00	S1	0.00	0.00	S1

TABLE 9.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	S1	-73.70	-82.83	S1
U 2 L 3	39.22	44.63	S1	-10.77	-14.00	S1
U 3 L 4	34.11	39.30	S1	-20.84	-26.04	S1
U 4 L 5	33.70	39.38	S1	-24.67	-30.01	S1
L 5 U 6	0.00	0.00	S1	0.00	0.00	S1
U 5 L 6	29.73	35.36	S1	-29.73	-35.36	S1
L 6 U 7	33.70	39.38	S1	-24.67	-30.01	S1
L 7 U 8	34.11	39.30	S1	-20.84	-26.04	S1
L 8 U 9	39.22	44.63	S1	-10.77	-14.00	S1
U 9 L10	0.00	0.00	S1	-73.70	-82.83	S1

TABLE 9.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 4) STANDARDS ONE LANE TO BE ADDED TO
THREE LANES OF HS TRUCKS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	62.86	70.64	S1	0.00	0.00	S1
L 2 L 3	62.86	70.64	S1	0.00	0.00	S1
L 3 L 4	88.30	99.23	S1	0.00	0.00	S1
L 4 L 5	101.51	114.07	S1	0.00	0.00	S1
L 5 L 6	108.12	121.50	S1	0.00	0.00	S1
L 6 L 7	101.51	114.07	S1	0.00	0.00	S1
L 7 L 8	88.30	99.23	S1	0.00	0.00	S1
L 8 L 9	62.86	70.64	S1	0.00	0.00	S1
L 9 L10	62.86	70.64	S1	0.00	0.00	S1

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TABLE 9.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	S1	-91.44	-102.75	S1
U 3 U 4	0.00	0.00	S1	-102.82	-115.55	S1
U 4 U 5	0.00	0.00	S1	-108.28	-121.68	S1
U 5 U 6	0.00	0.00	S1	-108.12	-121.50	S1
U 6 U 7	0.00	0.00	S1	-108.28	-121.68	S1
U 7 U 8	0.00	0.00	S1	-102.82	-115.55	S1
U 8 U 9	0.00	0.00	S1	-91.44	-102.75	S1

TABLE 9.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	43.16	54.70	S1	0.00	0.00	S1
L 2 U 2 B	0.00	0.00	S1	0.00	0.00	S1
L 3 U 3 T	28.76	37.39	S1	-32.10	-36.53	S1
L 3 U 3 B	9.04	11.75	S1	-37.67	-42.87	S1
L 4 U 4 T	34.90	43.62	S1	-29.18	-33.63	S1
L 4 U 4 B	20.32	25.41	S1	-35.46	-40.86	S1
L 5 U 5 T	36.31	44.17	S1	-28.14	-32.87	S1
L 5 U 5 B	25.77	31.35	S1	-36.08	-42.15	S1
L 6 U 6 T	5.72	6.55	S1	0.00	0.00	S1
L 6 U 6 B	4.26	4.87	S1	-37.42	-47.65	S1
L 7 U 7 T	34.90	43.62	S1	-29.18	-33.63	S1
L 7 U 7 B	20.32	25.41	S1	-35.46	-40.86	S1
L 8 U 8 T	28.76	37.39	S1	-32.10	-36.53	S1
L 8 U 8 B	9.04	11.75	S1	-37.67	-42.87	S1
L 9 U 9 T	43.16	54.70	S1	0.00	0.00	S1
L 9 U 9 B	0.00	0.00	S1	0.00	0.00	S1

TABLE 9.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	S1	-94.81	-106.54	S1
U 2 L 3	50.32	57.26	S1	-12.08	-15.70	S1
U 3 L 4	43.60	50.25	S1	-24.99	-31.24	S1
U 4 L 5	42.86	50.08	S1	-30.62	-37.25	S1
L 5 U 6	0.00	0.00	S1	0.00	0.00	S1
U 5 L 6	37.49	44.59	S1	-37.49	-44.59	S1
L 6 U 7	42.86	50.08	S1	-30.62	-37.25	S1
L 7 U 8	43.60	50.25	S1	-24.99	-31.24	S1
L 8 U 9	50.32	57.26	S1	-12.08	-15.70	S1
U 9 L10	0.00	0.00	S1	-94.81	-106.54	S1

TABLE 9.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 4) STANDARD C ONE LANE TO BE ADDED TO
THREE LANES OF HS TRUCKS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	72.29	81.23	S1	0.00	0.00	S1
L 2 L 3	72.29	81.23	S1	0.00	0.00	S1
L 3 L 4	101.66	114.24	S1	0.00	0.00	S1
L 4 L 5	116.71	131.15	S1	0.00	0.00	S1
L 5 L 6	124.25	139.63	S1	0.00	0.00	S1
L 6 L 7	116.71	131.15	S1	0.00	0.00	S1
L 7 L 8	101.66	114.24	S1	0.00	0.00	S1
L 8 L 9	72.29	81.23	S1	0.00	0.00	S1
L 9 L10	72.29	81.23	S1	0.00	0.00	S1

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TABLE 9.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	S1	-105.26	-118.29	S1
U 3 U 4	0.00	0.00	S1	-118.22	-132.85	S1
U 4 U 5	0.00	0.00	S1	-124.43	-139.83	S1
U 5 U 6	0.00	0.00	S1	-124.25	-139.63	S1
U 6 U 7	0.00	0.00	S1	-124.43	-139.83	S1
U 7 U 8	0.00	0.00	S1	-118.22	-132.85	S1
U 8 U 9	0.00	0.00	S1	-105.26	-118.29	S1

TABLE 9.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	46.15	58.48	S1	0.00	0.00	S1
L 2 U 2 B	0.00	0.00	S1	0.00	0.00	S1
L 3 U 3 T	31.10	40.43	S1	-36.68	-41.74	S1
L 3 U 3 B	10.01	13.01	S1	-43.20	-49.16	S1
L 4 U 4 T	39.14	48.93	S1	-33.17	-38.22	S1
L 4 U 4 B	22.01	27.51	S1	-40.52	-46.69	S1
L 5 U 5 T	41.07	49.96	S1	-31.69	-37.03	S1
L 5 U 5 B	28.76	34.99	S1	-41.00	-47.90	S1
L 6 U 6 T	6.57	7.52	S1	0.00	0.00	S1
L 6 U 6 B	4.80	5.49	S1	-39.61	-50.43	S1
L 7 U 7 T	39.14	48.93	S1	-33.17	-38.22	S1
L 7 U 7 B	22.01	27.51	S1	-40.52	-46.69	S1
L 8 U 8 T	31.10	40.43	S1	-36.68	-41.74	S1
L 8 U 8 B	10.01	13.01	S1	-43.20	-49.16	S1
L 9 U 9 T	46.15	58.48	S1	0.00	0.00	S1
L 9 U 9 B	0.00	0.00	S1	0.00	0.00	S1

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TABLE 9.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	S1	-109.02	-122.51	S1
U 2 L 3	57.71	65.68	S1	-13.37	-17.38	S1
U 3 L 4	49.82	57.41	S1	-27.06	-33.82	S1
U 4 L 5	48.71	56.91	S1	-34.17	-41.57	S1
L 5 U 6	0.00	0.00	S1	0.00	0.00	S1
U 5 L 6	42.23	50.23	S1	-42.23	-50.23	S1
L 6 U 7	48.71	56.91	S1	-34.17	-41.57	S1
L 7 U 8	49.82	57.41	S1	-27.06	-33.82	S1
L 8 U 9	57.71	65.68	S1	-13.37	-17.38	S1
U 9 L10	0.00	0.00	S1	-109.02	-122.51	S1

TABLE 9.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 4) PHII ONE LANE TO BE ADDED TO
THREE LANES OF HS TRUCKS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	86.61	97.33	S1	0.00	0.00	S1
L 2 L 3	86.61	97.33	S1	0.00	0.00	S1
L 3 L 4	121.57	136.62	S1	0.00	0.00	S1
L 4 L 5	137.61	154.65	S1	0.00	0.00	S1
L 5 L 6	145.63	163.66	S1	0.00	0.00	S1
L 6 L 7	137.61	154.65	S1	0.00	0.00	S1
L 7 L 8	121.57	136.62	S1	0.00	0.00	S1
L 8 L 9	86.61	97.33	S1	0.00	0.00	S1
L 9 L10	86.61	97.33	S1	0.00	0.00	S1

TABLE 9.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	S1	-125.89	-141.47	S1
U 3 U 4	0.00	0.00	S1	-139.39	-156.64	S1
U 4 U 5	0.00	0.00	S1	-145.84	-163.90	S1
U 5 U 6	0.00	0.00	S1	-145.63	-163.66	S1
U 6 U 7	0.00	0.00	S1	-145.84	-163.90	S1
U 7 U 8	0.00	0.00	S1	-139.39	-156.64	S1
U 8 U 9	0.00	0.00	S1	-125.89	-141.47	S1

TABLE 9.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	50.15	63.56	S1	0.00	0.00	S1
L 2 U 2 B	0.00	0.00	S1	0.00	0.00	S1
L 3 U 3 T	27.76	36.09	S1	-42.18	-48.01	S1
L 3 U 3 B	10.83	14.07	S1	-50.75	-57.76	S1
L 4 U 4 T	38.31	47.89	S1	-36.93	-42.56	S1
L 4 U 4 B	19.47	24.34	S1	-46.60	-53.70	S1
L 5 U 5 T	44.02	53.54	S1	-33.45	-39.08	S1
L 5 U 5 B	27.81	33.83	S1	-45.77	-53.47	S1
L 6 U 6 T	7.70	8.82	S1	0.00	0.00	S1
L 6 U 6 B	5.05	5.78	S1	-42.95	-54.68	S1
L 7 U 7 T	38.31	47.89	S1	-36.93	-42.56	S1
L 7 U 7 B	19.47	24.34	S1	-46.60	-53.70	S1
L 8 U 8 T	27.76	36.09	S1	-42.18	-48.01	S1
L 8 U 8 B	10.83	14.07	S1	-50.75	-57.76	S1
L 9 U 9 T	50.15	63.56	S1	0.00	0.00	S1
L 9 U 9 B	0.00	0.00	S1	0.00	0.00	S1

TABLE 9.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	S1	-130.63	-146.80	S1
U 2 L 3	67.80	77.16	S1	-14.46	-18.80	S1
U 3 L 4	57.30	66.03	S1	-23.95	-29.93	S1
U 4 L 5	54.37	63.53	S1	-33.04	-40.19	S1
L 5 U 6	0.00	0.00	S1	0.00	0.00	S1
U 5 L 6	45.02	53.55	S1	-45.02	-53.55	S1
L 6 U 7	54.37	63.53	S1	-33.04	-40.19	S1
L 7 U 8	57.30	66.03	S1	-23.95	-29.93	S1
L 8 U 9	67.80	77.16	S1	-14.46	-18.80	S1
U 9 L10	0.00	0.00	S1	-130.63	-146.80	S1

TABLE 9.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 4) P413 ONE LANE TO BE ADDED TO
THREE LANES OF HS TRUCKS

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	101.06	113.56	S1	0.00	0.00	S1
L 2 L 3	101.06	113.56	S1	0.00	0.00	S1
L 3 L 4	140.66	158.07	S1	0.00	0.00	S1
L 4 L 5	159.98	179.78	S1	0.00	0.00	S1
L 5 L 6	170.33	191.41	S1	0.00	0.00	S1
L 6 L 7	159.98	179.78	S1	0.00	0.00	S1
L 7 L 8	140.66	158.07	S1	0.00	0.00	S1
L 8 L 9	101.06	113.56	S1	0.00	0.00	S1
L 9 L10	101.06	113.56	S1	0.00	0.00	S1

TABLE 9.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	S1	-145.65	-163.67	S1
U 3 U 4	0.00	0.00	S1	-162.04	-182.10	S1
U 4 U 5	0.00	0.00	S1	-170.58	-191.69	S1
U 5 U 6	0.00	0.00	S1	-170.33	-191.41	S1
U 6 U 7	0.00	0.00	S1	-170.58	-191.69	S1
U 7 U 8	0.00	0.00	S1	-162.04	-182.10	S1
U 8 U 9	0.00	0.00	S1	-145.65	-163.67	S1

TABLE 9.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

 (FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	46.65	59.12	S1	0.00	0.00	S1
L 2 U 2 B	0.00	0.00	S1	0.00	0.00	S1
L 3 U 3 T	29.56	38.43	S1	-47.53	-54.10	S1
L 3 U 3 B	9.54	12.40	S1	-58.34	-66.40	S1
L 4 U 4 T	39.01	48.76	S1	-40.52	-46.70	S1
L 4 U 4 B	20.77	25.97	S1	-52.75	-60.79	S1
L 5 U 5 T	46.87	57.02	S1	-35.57	-41.56	S1
L 5 U 5 B	28.33	34.46	S1	-50.89	-59.46	S1
L 6 U 6 T	9.01	10.31	S1	0.00	0.00	S1
L 6 U 6 B	5.27	6.04	S1	-38.88	-49.50	S1
L 7 U 7 T	39.01	48.76	S1	-40.52	-46.70	S1
L 7 U 7 B	20.77	25.97	S1	-52.75	-60.79	S1
L 8 U 8 T	29.56	38.43	S1	-47.53	-54.10	S1
L 8 U 8 B	9.54	12.40	S1	-58.34	-66.40	S1
L 9 U 9 T	46.65	59.12	S1	0.00	0.00	S1
L 9 U 9 B	0.00	0.00	S1	0.00	0.00	S1

TABLE 9.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 4)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	S1	-152.41	-171.28	S1
U 2 L 3	77.93	88.70	S1	-12.74	-16.56	S1
U 3 L 4	64.86	74.75	S1	-25.54	-31.93	S1
U 4 L 5	60.46	70.64	S1	-33.66	-40.94	S1
L 5 U 6	0.00	0.00	S1	0.00	0.00	S1
U 5 L 6	47.97	57.05	S1	-47.97	-57.05	S1
L 6 U 7	60.46	70.64	S1	-33.66	-40.94	S1
L 7 U 8	64.86	74.75	S1	-25.54	-31.93	S1
L 8 U 9	77.93	88.70	S1	-12.74	-16.56	S1
U 9 L10	0.00	0.00	S1	-152.41	-171.28	S1

TABLE 6.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 1) **TYPE M3**

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	64.00	71.92	T1	0.00	0.00	T1
L 2 L 3	64.00	71.92	T1	0.00	0.00	T1
L 3 L 4	90.06	101.21	T1	0.00	0.00	T1
L 4 L 5	103.20	115.98	T1	0.00	0.00	T1
L 5 L 6	110.62	124.31	T1	0.00	0.00	T1
L 6 L 7	103.20	115.98	T1	0.00	0.00	T1
L 7 L 8	90.06	101.21	T1	0.00	0.00	T1
L 8 L 9	64.00	71.92	T1	0.00	0.00	T1
L 9 L10	64.00	71.92	T1	0.00	0.00	T1

TABLE 6.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 1)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	T1	-93.26	-104.80	T1
U 3 U 4	0.00	0.00	T1	-104.54	-117.47	T1
U 4 U 5	0.00	0.00	T1	-110.78	-124.49	T1
U 5 U 6	0.00	0.00	T1	-110.62	-124.31	T1
U 6 U 7	0.00	0.00	T1	-110.78	-124.49	T1
U 7 U 8	0.00	0.00	T1	-104.54	-117.47	T1
U 8 U 9	0.00	0.00	T1	-93.26	-104.80	T1

TABLE 6.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 1)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	67.15	85.10	T1	0.00	0.00	T1
L 2 U 2 B	0.00	0.00	T1	0.00	0.00	T1
L 3 U 3 T	36.82	47.86	T1	-33.48	-38.11	T1
L 3 U 3 B	16.60	21.58	T1	-38.74	-44.09	T1
L 4 U 4 T	40.38	50.47	T1	-31.06	-35.80	T1
L 4 U 4 B	26.56	33.20	T1	-36.99	-42.62	T1
L 5 U 5 T	39.90	48.54	T1	-30.92	-36.12	T1
L 5 U 5 B	29.99	36.48	T1	-38.40	-44.86	T1
L 6 U 6 T	5.85	6.70	T1	0.00	0.00	T1
L 6 U 6 B	4.68	5.36	T1	-61.22	-77.95	T1
L 7 U 7 T	40.38	50.47	T1	-31.06	-35.80	T1
L 7 U 7 B	26.56	33.20	T1	-36.99	-42.62	T1
L 8 U 8 T	36.82	47.86	T1	-33.48	-38.11	T1
L 8 U 8 B	16.60	21.58	T1	-38.74	-44.09	T1
L 9 U 9 T	67.15	85.10	T1	0.00	0.00	T1
L 9 U 9 B	0.00	0.00	T1	0.00	0.00	T1

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TABLE 6.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 1)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	T1	-96.52	-108.47	T1
U 2 L 3	51.75	58.90	T1	-22.17	-28.83	T1
U 3 L 4	45.48	52.41	T1	-32.66	-40.82	T1
U 4 L 5	45.62	53.30	T1	-35.63	-43.34	T1
L 5 U 6	0.00	0.00	T1	0.00	0.00	T1
U 5 L 6	41.19	48.99	T1	-41.19	-48.99	T1
L 6 U 7	45.62	53.30	T1	-35.63	-43.34	T1
L 7 U 8	45.48	52.41	T1	-32.66	-40.82	T1
L 8 U 9	51.75	58.90	T1	-22.17	-28.83	T1
U 9 L10	0.00	0.00	T1	-96.52	-108.47	T1

TABLE 7.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORED)

(FOR TRUCK 2) **TYPE M3-S2**

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	87.88	98.75	T2	0.00	0.00	T2
L 2 L 3	87.88	98.75	T2	0.00	0.00	T2
L 3 L 4	122.99	138.22	T2	0.00	0.00	T2
L 4 L 5	141.51	159.02	T2	0.00	0.00	T2
L 5 L 6	151.23	169.94	T2	0.00	0.00	T2
L 6 L 7	141.51	159.02	T2	0.00	0.00	T2
L 7 L 8	122.99	138.22	T2	0.00	0.00	T2
L 8 L 9	87.88	98.75	T2	0.00	0.00	T2
L 9 L10	87.88	98.75	T2	0.00	0.00	T2

TABLE 7.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORED)

(FOR TRUCK 2)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	T2	-127.36	-143.12	T2
U 3 U 4	0.00	0.00	T2	-143.34	-161.08	T2
U 4 U 5	0.00	0.00	T2	-151.45	-170.19	T2
U 5 U 6	0.00	0.00	T2	-151.23	-169.94	T2
U 6 U 7	0.00	0.00	T2	-151.45	-170.19	T2
U 7 U 8	0.00	0.00	T2	-143.34	-161.08	T2
U 8 U 9	0.00	0.00	T2	-127.36	-143.12	T2

TABLE 7.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 2)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	68.99	87.43	T2	0.00	0.00	T2
L 2 U 2 B	0.00	0.00	T2	0.00	0.00	T2
L 3 U 3 T	42.39	55.11	T2	-45.20	-51.44	T2
L 3 U 3 B	14.12	18.36	T2	-52.81	-60.11	T2
L 4 U 4 T	50.56	63.19	T2	-41.35	-47.65	T2
L 4 U 4 B	30.42	38.02	T2	-49.93	-57.54	T2
L 5 U 5 T	51.95	63.19	T2	-40.25	-47.03	T2
L 5 U 5 B	37.55	45.67	T2	-51.11	-59.71	T2
L 6 U 6 T	8.00	9.16	T2	0.00	0.00	T2
L 6 U 6 B	6.09	6.97	T2	-60.95	-77.60	T2
L 7 U 7 T	50.56	63.19	T2	-41.35	-47.65	T2
L 7 U 7 B	30.42	38.02	T2	-49.93	-57.54	T2
L 8 U 8 T	42.39	55.11	T2	-45.20	-51.44	T2
L 8 U 8 B	14.12	18.36	T2	-52.81	-60.11	T2
L 9 U 9 T	68.99	87.43	T2	0.00	0.00	T2
L 9 U 9 B	0.00	0.00	T2	0.00	0.00	T2

TABLE 7.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 2)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	T2	-132.54	-148.94	T2
U 2 L 3	70.55	80.30	T2	-18.86	-24.52	T2
U 3 L 4	61.39	70.75	T2	-37.40	-46.75	T2
U 4 L 5	60.72	70.94	T2	-44.61	-54.26	T2
L 5 U 6	0.00	0.00	T2	0.00	0.00	T2
U 5 L 6	53.63	63.79	T2	-53.63	-63.79	T2
L 6 U 7	60.72	70.94	T2	-44.61	-54.26	T2
L 7 U 8	61.39	70.75	T2	-37.40	-46.75	T2
L 8 U 9	70.55	80.30	T2	-18.86	-24.52	T2
U 9 L10	0.00	0.00	T2	-132.54	-148.94	T2

TABLE 8.1 MAXIMUM LIVE LOAD FORCE IN LOWER CHORDS (UNFACTORIED)

(FOR TRUCK 3) **TYPE MB-3**

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 L 2	95.39	107.19	T3	0.00	0.00	T3
L 2 L 3	95.39	107.19	T3	0.00	0.00	T3
L 3 L 4	133.37	149.87	T3	0.00	0.00	T3
L 4 L 5	152.17	171.00	T3	0.00	0.00	T3
L 5 L 6	163.19	183.39	T3	0.00	0.00	T3
L 6 L 7	152.17	171.00	T3	0.00	0.00	T3
L 7 L 8	133.37	149.87	T3	0.00	0.00	T3
L 8 L 9	95.39	107.19	T3	0.00	0.00	T3
L 9 L10	95.39	107.19	T3	0.00	0.00	T3

TABLE 8.2 MAXIMUM LIVE LOAD FORCE IN UPPER CHORDS (UNFACTORIED)

(FOR TRUCK 3)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
U 2 U 3	0.00	0.00	T3	-138.10	-155.19	T3
U 3 U 4	0.00	0.00	T3	-154.13	-173.21	T3
U 4 U 5	0.00	0.00	T3	-163.43	-183.65	T3
U 5 U 6	0.00	0.00	T3	-163.19	-183.39	T3
U 6 U 7	0.00	0.00	T3	-163.43	-183.65	T3
U 7 U 8	0.00	0.00	T3	-154.13	-173.21	T3
U 8 U 9	0.00	0.00	T3	-138.10	-155.19	T3

TABLE 8.4 MAXIMUM LIVE LOAD FORCE IN VERTICAL MEMBERS (UNFACTORED)

(FOR TRUCK 3)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 2 U 2 T	64.66	81.95	T3	0.00	0.00	T3
L 2 U 2 B	0.00	0.00	T3	0.00	0.00	T3
L 3 U 3 T	42.00	54.60	T3	-48.63	-55.35	T3
L 3 U 3 B	13.92	18.10	T3	-57.12	-65.01	T3
L 4 U 4 T	52.18	65.22	T3	-44.16	-50.89	T3
L 4 U 4 B	29.76	37.20	T3	-53.72	-61.91	T3
L 5 U 5 T	54.82	66.69	T3	-42.48	-49.63	T3
L 5 U 5 B	38.75	47.14	T3	-54.59	-63.78	T3
L 6 U 6 T	8.63	9.88	T3	0.00	0.00	T3
L 6 U 6 B	6.43	7.36	T3	-55.93	-71.21	T3
L 7 U 7 T	52.18	65.22	T3	-44.16	-50.89	T3
L 7 U 7 B	29.76	37.20	T3	-53.72	-61.91	T3
L 8 U 8 T	42.00	54.60	T3	-48.63	-55.35	T3
L 8 U 8 B	13.92	18.10	T3	-57.12	-65.01	T3
L 9 U 9 T	64.66	81.95	T3	0.00	0.00	T3
L 9 U 9 B	0.00	0.00	T3	0.00	0.00	T3

TABLE 8.5 MAXIMUM LIVE LOAD FORCE IN DIAGONAL MEMBERS (UNFACTORED)

(FOR TRUCK 3)

MEMBER	MAX TENSILE FORCE			MAX COMPRESSIVE FORCE		
	LL (K)	LL+I (K)	LOAD TYPE	LL (K)	LL+I (K)	LOAD TYPE
L 1 U 2	0.00	0.00	T3	-143.87	-161.67	T3
U 2 L 3	76.30	86.84	T3	-18.60	-24.18	T3
U 3 L 4	66.06	76.13	T3	-36.60	-45.75	T3
U 4 L 5	64.85	75.77	T3	-46.04	-56.01	T3
L 5 U 6	0.00	0.00	T3	0.00	0.00	T3
U 5 L 6	56.60	67.32	T3	-56.60	-67.32	T3
L 6 U 7	64.85	75.77	T3	-46.04	-56.01	T3
L 7 U 8	66.06	76.13	T3	-36.60	-45.75	T3
L 8 U 9	76.30	86.84	T3	-18.60	-24.18	T3
U 9 L10	0.00	0.00	T3	-143.87	-161.67	T3

Factored Force
Summary

TABLE 10.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE	
	TOTAL DEAD	TENSION		COMPRESSION	DL+LL+I TYPE
	LOAD	LL+I TYPE		LL+I TYPE	(K)
L 1 L 2	956.65	344.67	L	0.00	1301.32
L 2 L 3	956.66	344.67	L	0.00	1301.32
L 3 L 4	1346.82	487.21	L	0.00	1834.04
L 4 L 5	1551.52	561.61	L	0.00	2113.13
L 5 L 6	1667.00	603.17	L	0.00	2270.17
L 6 L 7	1548.23	561.61	L	0.00	2109.84
L 7 L 8	1341.05	487.21	L	0.00	1828.26
L 8 L 9	948.54	344.67	L	0.00	1293.21
L 9 L10	948.54	344.67	L	0.00	1293.21

TABLE 10.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM	
	TOTAL	TENSION	DEAD	COMPRESSION	MEMBER FORCE	MEMBER FORCE	DL+LL+I	TYPE
	LOAD	LL+I	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
U 2 U 3	-1394.60	0.00	-504.50	L	-1394.60	-1899.10	L	
U 3 U 4	-1571.57	0.00	-568.87	L	-1571.57	-2140.44	L	
U 4 U 5	-1669.42	0.00	-604.04	L	-1669.42	-2273.46	L	
U 5 U 6	-1665.94	0.00	-603.17	L	-1665.94	-2269.11	L	
U 6 U 7	-1668.36	0.00	-604.04	L	-1668.36	-2272.40	L	
U 7 U 8	-1568.24	0.00	-568.87	L	-1568.24	-2137.10	L	
U 8 U 9	-1388.62	0.00	-504.50	L	-1388.62	-1893.11	L	

TABLE 10.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER LCT	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		LL+I TYPE		LL+I TYPE		DL+LL+I TYPE		DL+LL+I TYPE	
		(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)
L 2 U 2 T	233.39	248.23	HS	0.00		481.62	HS	233.39	
L 2 U 2 B	233.39	0.00		0.00		233.39		233.39	
L 3 U 3 T	-210.98	144.15	HS	-140.85	L	-66.84	HS	-351.84	L
L 3 U 3 B	-210.98	61.92	HS	-185.71	L	-149.07	HS	-396.70	L
L 4 U 4 T	-57.26	154.00	HS	-116.86	L	96.74	HS	-174.12	L
L 4 U 4 B	-57.26	99.99	HS	-159.85	L	42.73	HS	-217.11	L
L 5 U 5 T	52.67	148.97	HS	-110.87	HS	201.64	HS	-58.20	HS
L 5 U 5 B	52.67	111.30	HS	-149.25	L	163.97	HS	-96.58	L
L 6 U 6 T	50.90	32.49	L	0.00		83.39	L	50.90	
L 6 U 6 B	50.90	21.40	L	-226.15	HS	72.31	L	-175.25	HS
L 7 U 7 T	-61.21	154.00	HS	-116.86	L	92.79	HS	-178.07	L
L 7 U 7 B	-61.21	99.99	HS	-159.85	L	38.78	HS	-221.06	L
L 8 U 8 T	-215.01	144.15	HS	-140.85	L	-70.86	HS	-355.86	L
L 8 U 8 B	-215.01	61.92	HS	-185.71	L	-153.09	HS	-400.72	L
L 9 U 9 T	224.53	248.23	HS	0.00		472.76	HS	224.53	
L 9 U 9 B	224.53	0.00		0.00		224.53		224.53	

TABLE 10.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM	
	TOTAL	TENSION	DEAD	---	---	---	---	---
	LOAD	LL+I TYPE	LL+I TYPE	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)		(K)	(K)	(K)	(K)	
L 1 U 2	-1442.84	0.00		-558.60	L	-1442.84	-2001.44	L
U 2 L 3	588.46	269.23	L	-82.71	HS	857.69	505.75	HS
U 3 L 4	351.79	215.48	L	-122.94	HS	567.27	228.85	HS
U 4 L 5	213.89	196.73	L	-132.23	HS	410.62	81.66	HS
L 5 U 6	0.00	0.00		0.00		0.00	0.00	
U 5 L 6	-2.01	159.55	L	-159.55	L	157.54	-161.56	L
L 6 U 7	218.02	196.73	L	-132.23	HS	414.75	85.79	HS
L 7 U 8	356.07	215.48	L	-122.94	HS	571.55	233.13	HS
L 8 U 9	591.98	269.23	L	-82.71	HS	861.21	509.27	HS
U 9 L10	-1430.60	0.00		-558.60	L	-1430.60	-1989.20	L

TABLE 10.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

AASHTO LOADING RESULTS ~~FOR THREE LANES TO BE ADDED TO ONE~~
~~LANE OF PERMIT TRUCKS (A, B, C, P411, P413)~~

MEMBER	MAXIMUM TOTAL DEAD		MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
	LOAD	LL+I TYPE	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)
L 1 L 2	956.65	211.41	L	0.00	1168.06	L	956.65			
L 2 L 3	956.66	211.41	L	0.00	1168.06	L	956.66			
L 3 L 4	1346.82	298.84	L	0.00	1645.66	L	1346.82			
L 4 L 5	1551.52	344.47	L	0.00	1895.99	L	1551.52			
L 5 L 6	1667.00	369.96	L	0.00	2036.96	L	1667.00			
L 6 L 7	1548.23	344.47	L	0.00	1892.70	L	1548.23			
L 7 L 8	1341.05	298.84	L	0.00	1639.89	L	1341.05			
L 8 L 9	948.54	211.41	L	0.00	1159.95	L	948.54			
L 9 L10	948.54	211.41	L	0.00	1159.95	L	948.54			

TABLE 10.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE		
	TOTAL DEAD	TENSION		COMPRESSION	DL+LL+I TYPE	
	LOAD	LL+I TYPE		LL+I TYPE	DL+LL+I TYPE	
U 2 U 3	-1394.60	0.00	-309.44	L	-1394.60	-1704.04 L
U 3 U 4	-1571.57	0.00	-348.92	L	-1571.57	-1920.50 L
U 4 U 5	-1669.42	0.00	-370.50	L	-1669.42	-2039.92 L
U 5 U 6	-1665.94	0.00	-369.96	L	-1665.94	-2035.90 L
U 6 U 7	-1668.36	0.00	-370.50	L	-1668.36	-2038.85 L
U 7 U 8	-1568.24	0.00	-348.92	L	-1568.24	-1917.16 L
U 8 U 9	-1388.62	0.00	-309.44	L	-1388.62	-1698.06 L

TABLE 10.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER LCT	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
L 2 U 2 T	233.39	152.25	HS	0.00		385.64	HS	233.39	
L 2 U 2 B	233.39	0.00		0.00		233.39		233.39	
L 3 U 3 T	-210.98	88.42	HS	-86.39	L	-122.57	HS	-297.38	L
L 3 U 3 B	-210.98	37.98	HS	-113.91	L	-173.01	HS	-324.89	L
L 4 U 4 T	-57.26	94.46	HS	-71.68	L	37.20	HS	-128.94	L
L 4 U 4 B	-57.26	61.33	HS	-98.05	L	4.07	HS	-155.31	L
L 5 U 5 T	52.67	91.37	HS	-68.00	HS	144.04	HS	-15.33	HS
L 5 U 5 B	52.67	68.27	HS	-91.55	L	120.94	HS	-38.88	L
L 6 U 6 T	50.90	19.93	L	0.00		70.83	L	50.90	
L 6 U 6 B	50.90	13.13	L	-138.71	HS	64.03	L	-87.81	HS
L 7 U 7 T	-61.21	94.46	HS	-71.68	L	33.25	HS	-132.89	L
L 7 U 7 B	-61.21	61.33	HS	-98.05	L	0.12	HS	-159.26	L
L 8 U 8 T	-215.01	88.42	HS	-86.39	L	-126.60	HS	-301.40	L
L 8 U 8 B	-215.01	37.98	HS	-113.91	L	-177.03	HS	-328.92	L
L 9 U 9 T	224.53	152.25	HS	0.00		376.78	HS	224.53	
L 9 U 9 B	224.53	0.00		0.00		224.53		224.53	

TABLE 10.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

AASHTO LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE	
	TOTAL DEAD	TENSION		COMPRESSION	MEMBER TYPE
	LOAD	LL+I TYPE		LL+I TYPE	DL+LL+I TYPE
	(K)	(K)	(K)	(K)	(K)
L 1 U 2	-1442.84	0.00	-342.62	L	-1442.84
U 2 L 3	588.46	165.13	L	-50.73	HS
U 3 L 4	351.79	132.17	L	-75.41	HS
U 4 L 5	213.89	120.66	L	-81.11	HS
L 5 U 6	0.00	0.00		0.00	
U 5 L 6	-2.01	97.86	L	-97.86	L
L 6 U 7	218.02	120.66	L	-81.11	HS
L 7 U 8	356.07	132.17	L	-75.41	HS
L 8 U 9	591.98	165.13	L	-50.73	HS
U 9 L10	-1430.60	0.00	-342.62	L	-1430.60
					-1773.23
					L

TABLE 14.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS **STANDARD A FOR ONE LANE TO BE ADDED
TO THREE LANES OF HS TRUCKS**

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM			
	TOTAL	TENSION	DEAD	- - - - -	LOAD	LL+I TYPE	LL+I	TYPE	MEMBER FORCE	MEMBER FORCE
	(K)	(K)	(K)	- - - - -	(K)	(K)	(K)	- - - - -	(K)	(K)
L 1 L 2	956.65	71.39	S1		0.00	S1	1028.05	S1	956.65	S1
L 2 L 3	956.66	71.39	S1		0.00	S1	1028.05	S1	956.66	S1
L 3 L 4	1346.82	100.32	S1		0.00	S1	1447.15	S1	1346.82	S1
L 4 L 5	1551.52	115.05	S1		0.00	S1	1666.57	S1	1551.52	S1
L 5 L 6	1667.00	122.87	S1		0.00	S1	1789.87	S1	1667.00	S1
L 6 L 7	1548.23	115.05	S1		0.00	S1	1663.28	S1	1548.23	S1
L 7 L 8	1341.05	100.32	S1		0.00	S1	1441.37	S1	1341.05	S1
L 8 L 9	948.54	71.39	S1		0.00	S1	1019.93	S1	948.54	S1
L 9 L10	948.54	71.39	S1		0.00	S1	1019.93	S1	948.54	S1

TABLE 14.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL DEAD	TENSION	COMPRESSION	MEMBER FORCE	MEMBER FORCE	DL+LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE	
	LOAD	LL+I (K)	LL+I (K)	DL+LL+I (K)	DL+LL+I (K)	DL+LL+I (K)	DL+LL+I (K)	DL+LL+I (K)	
U 2 U 3	-1394.60	0.00	S1	-103.88	S1	-1394.60	S1	-1498.48	S1
U 3 U 4	-1571.57	0.00	S1	-116.54	S1	-1571.57	S1	-1688.11	S1
U 4 U 5	-1669.42	0.00	S1	-123.05	S1	-1669.42	S1	-1792.46	S1
U 5 U 6	-1665.94	0.00	S1	-122.87	S1	-1665.94	S1	-1788.81	S1
U 6 U 7	-1668.36	0.00	S1	-123.05	S1	-1668.36	S1	-1791.40	S1
U 7 U 8	-1568.24	0.00	S1	-116.54	S1	-1568.24	S1	-1684.77	S1
U 8 U 9	-1388.62	0.00	S1	-103.88	S1	-1388.62	S1	-1492.50	S1

TABLE 14.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER LCT	TOTAL LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		DEAD (K)	LL+I TYPE	LL+I TYPE (K)	S1	DL+LL+I TYPE (K)	S1	DL+LL+I TYPE (K)	S1
L 2 U 2 T	233.39	62.45	S1	0.00	S1	295.84	S1	233.39	S1
L 2 U 2 B	233.39	0.00	S1	0.00	S1	233.39	S1	233.39	S1
L 3 U 3 T	-210.98	40.25	S1	-37.15	S1	-170.74	S1	-248.13	S1
L 3 U 3 B	-210.98	13.63	S1	-43.44	S1	-197.36	S1	-254.42	S1
L 4 U 4 T	-57.26	45.57	S1	-34.38	S1	-11.69	S1	-91.64	S1
L 4 U 4 B	-57.26	27.54	S1	-41.56	S1	-29.72	S1	-98.81	S1
L 5 U 5 T	52.67	45.54	S1	-33.89	S1	98.21	S1	18.78	S1
L 5 U 5 B	52.67	32.83	S1	-43.09	S1	85.50	S1	9.58	S1
L 6 U 6 T	50.90	6.62	S1	0.00	S1	57.52	S1	50.90	S1
L 6 U 6 B	50.90	5.02	S1	-55.33	S1	55.93	S1	-4.42	S1
L 7 U 7 T	-61.21	45.57	S1	-34.38	S1	-15.64	S1	-95.59	S1
L 7 U 7 B	-61.21	27.54	S1	-41.56	S1	-33.67	S1	-102.76	S1
L 8 U 8 T	-215.01	40.25	S1	-37.15	S1	-174.76	S1	-252.16	S1
L 8 U 8 B	-215.01	13.63	S1	-43.44	S1	-201.38	S1	-258.45	S1
L 9 U 9 T	224.53	62.45	S1	0.00	S1	286.98	S1	224.53	S1
L 9 U 9 B	224.53	0.00	S1	0.00	S1	224.53	S1	224.53	S1

TABLE 14.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	TOTAL	MAXIMUM TENSION	MAXIMUM COMPRESSION	MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE				
	DEAD	-----	-----	-----	-----				
	LOAD	LL+I TYPE (K)	LL+I TYPE (K)	DL+LL+I TYPE (K)	DL+LL+I TYPE (K)				
L 1 U 2	-1442.84	0.00	S1	-107.67	S1	-1442.84	S1	-1550.51	S1
U 2 L 3	588.46	58.03	S1	-18.21	S1	646.49	S1	570.26	S1
U 3 L 4	351.79	51.10	S1	-33.86	S1	402.89	S1	317.94	S1
U 4 L 5	213.89	51.19	S1	-39.01	S1	265.08	S1	174.88	S1
L 5 U 6	0.00	0.00	S1	0.00	S1	0.00	S1	0.00	S1
U 5 L 6	-2.01	45.97	S1	-45.97	S1	43.96	S1	-47.98	S1
L 6 U 7	218.02	51.19	S1	-39.01	S1	269.22	S1	179.02	S1
L 7 U 8	356.07	51.10	S1	-33.86	S1	407.17	S1	322.21	S1
L 8 U 9	591.98	58.03	S1	-18.21	S1	650.01	S1	573.78	S1
U 9 L10	-1430.60	0.00	S1	-107.67	S1	-1430.60	S1	-1538.27	S1

TABLE 14.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORIED)

STATE VEHICLE S1 LOADING RESULTS **STANDARD IS ONE LANE TO BE ADDED
TO THREE LANES OF HS TRUCKS**

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	- - - - -	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)	- - - - -	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)
L 1 L 2	956.65	91.83	S1		0.00	S1	1048.49	S1	956.65	S1		
L 2 L 3	956.66	91.83	S1		0.00	S1	1048.49	S1	956.66	S1		
L 3 L 4	1346.82	129.00	S1		0.00	S1	1475.83	S1	1346.82	S1		
L 4 L 5	1551.52	148.30	S1		0.00	S1	1699.81	S1	1551.52	S1		
L 5 L 6	1667.00	157.95	S1		0.00	S1	1824.95	S1	1667.00	S1		
L 6 L 7	1548.23	148.30	S1		0.00	S1	1696.53	S1	1548.23	S1		
L 7 L 8	1341.05	129.00	S1		0.00	S1	1470.05	S1	1341.05	S1		
L 8 L 9	948.54	91.83	S1		0.00	S1	1040.37	S1	948.54	S1		
L 9 L10	948.54	91.83	S1		0.00	S1	1040.37	S1	948.54	S1		

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TABLE 14.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL DEAD	TENSION	COMPRESSION	MEMBER FORCE	MEMBER FORCE	DL+LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE	
	LOAD	LL+I TYPE	LL+I TYPE	(K)	(K)	(K)	(K)	(K)	
U 2 U 3	-1394.60	0.00	S1	-133.58	S1	-1394.60	S1	-1528.18	S1
U 3 U 4	-1571.57	0.00	S1	-150.21	S1	-1571.57	S1	-1721.78	S1
U 4 U 5	-1669.42	0.00	S1	-158.18	S1	-1669.42	S1	-1827.60	S1
U 5 U 6	-1665.94	0.00	S1	-157.95	S1	-1665.94	S1	-1823.89	S1
U 6 U 7	-1668.36	0.00	S1	-158.18	S1	-1668.36	S1	-1826.54	S1
U 7 U 8	-1568.24	0.00	S1	-150.21	S1	-1568.24	S1	-1718.45	S1
U 8 U 9	-1388.62	0.00	S1	-133.58	S1	-1388.62	S1	-1522.20	S1

TABLE 14.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER LCT	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
L 2 U 2 T	233.39	71.11	S1	0.00	S1	304.50	S1	233.39	S1
L 2 U 2 B	233.39	0.00	S1	0.00	S1	233.39	S1	233.39	S1
L 3 U 3 T	-210.98	48.60	S1	-47.49	S1	-162.38	S1	-258.48	S1
L 3 U 3 B	-210.98	15.28	S1	-55.73	S1	-195.70	S1	-266.71	S1
L 4 U 4 T	-57.26	56.71	S1	-43.72	S1	-0.55	S1	-100.98	S1
L 4 U 4 B	-57.26	33.03	S1	-53.12	S1	-24.23	S1	-110.38	S1
L 5 U 5 T	52.67	57.43	S1	-42.74	S1	110.09	S1	9.93	S1
L 5 U 5 B	52.67	40.76	S1	-54.80	S1	93.43	S1	-2.13	S1
L 6 U 6 T	50.90	8.51	S1	0.00	S1	59.41	S1	50.90	S1
L 6 U 6 B	50.90	6.34	S1	-61.94	S1	57.24	S1	-11.04	S1
L 7 U 7 T	-61.21	56.71	S1	-43.72	S1	-4.50	S1	-104.93	S1
L 7 U 7 B	-61.21	33.03	S1	-53.12	S1	-28.18	S1	-114.33	S1
L 8 U 8 T	-215.01	48.60	S1	-47.49	S1	-166.41	S1	-262.50	S1
L 8 U 8 B	-215.01	15.28	S1	-55.73	S1	-199.73	S1	-270.74	S1
L 9 U 9 T	224.53	71.11	S1	0.00	S1	295.64	S1	224.53	S1
L 9 U 9 B	224.53	0.00	S1	0.00	S1	224.53	S1	224.53	S1

TABLE 14.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL DEAD	TENSION	COMPRESSION	MEMBER FORCE	MEMBER FORCE				
	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE	(K)	(K)		
L 1 U 2	-1442.84	0.00	S1	-138.50	S1	-1442.84	S1	-1581.34	S1
U 2 L 3	588.46	74.44	S1	-20.41	S1	662.90	S1	568.05	S1
U 3 L 4	351.79	65.32	S1	-40.61	S1	417.11	S1	311.18	S1
U 4 L 5	213.89	65.10	S1	-48.42	S1	278.99	S1	165.47	S1
L 5 U 6	0.00	0.00	S1	0.00	S1	0.00	S1	0.00	S1
U 5 L 6	-2.01	57.97	S1	-57.97	S1	55.96	S1	-59.98	S1
L 6 U 7	218.02	65.10	S1	-48.42	S1	283.12	S1	169.60	S1
L 7 U 8	356.07	65.32	S1	-40.61	S1	421.39	S1	315.46	S1
L 8 U 9	591.98	74.44	S1	-20.41	S1	666.43	S1	571.57	S1
U 9 L10	-1430.60	0.00	S1	-138.50	S1	-1430.60	S1	-1569.10	S1

TABLE 14.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS **STANDARD C ONE LANE TO BE ABLEED
TO THREE LANES OF HS TRUCKS**

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)
L 1 L 2	956.65	105.60	S1		0.00	S1	1062.26	S1	956.65	S1		
L 2 L 3	956.66	105.60	S1		0.00	S1	1062.26	S1	956.66	S1		
L 3 L 4	1346.82	148.51	S1		0.00	S1	1495.33	S1	1346.82	S1		
L 4 L 5	1551.52	170.50	S1		0.00	S1	1722.02	S1	1551.52	S1		
L 5 L 6	1667.00	181.52	S1		0.00	S1	1848.52	S1	1667.00	S1		
L 6 L 7	1548.23	170.50	S1		0.00	S1	1718.73	S1	1548.23	S1		
L 7 L 8	1341.05	148.51	S1		0.00	S1	1489.56	S1	1341.05	S1		
L 8 L 9	948.54	105.60	S1		0.00	S1	1054.14	S1	948.54	S1		
L 9 L10	948.54	105.60	S1		0.00	S1	1054.14	S1	948.54	S1		

TABLE 14.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE
	(K)	(K)	(K)				(K)		(K)
U 2 U 3	-1394.60	0.00	S1	-153.78	S1	-1394.60	S1	-1548.38	S1
U 3 U 4	-1571.57	0.00	S1	-172.70	S1	-1571.57	S1	-1744.27	S1
U 4 U 5	-1669.42	0.00	S1	-181.78	S1	-1669.42	S1	-1851.20	S1
U 5 U 6	-1665.94	0.00	S1	-181.52	S1	-1665.94	S1	-1847.46	S1
U 6 U 7	-1668.36	0.00	S1	-181.78	S1	-1668.36	S1	-1850.13	S1
U 7 U 8	-1568.24	0.00	S1	-172.70	S1	-1568.24	S1	-1740.94	S1
U 8 U 9	-1388.62	0.00	S1	-153.78	S1	-1388.62	S1	-1542.39	S1

TABLE 14.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER LCT	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		(K)	LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE
L 2 U 2 T	233.39	76.03	S1	0.00	S1	309.42	S1	233.39	S1
L 2 U 2 B	233.39	0.00	S1	0.00	S1	233.39	S1	233.39	S1
L 3 U 3 T	-210.98	52.57	S1	-54.27	S1	-158.42	S1	-265.25	S1
L 3 U 3 B	-210.98	16.91	S1	-63.91	S1	-194.07	S1	-274.90	S1
L 4 U 4 T	-57.26	63.61	S1	-49.69	S1	6.35	S1	-106.95	S1
L 4 U 4 B	-57.26	35.76	S1	-60.70	S1	-21.50	S1	-117.96	S1
L 5 U 5 T	52.67	64.95	S1	-48.14	S1	117.61	S1	4.53	S1
L 5 U 5 B	52.67	45.49	S1	-62.27	S1	98.16	S1	-9.60	S1
L 6 U 6 T	50.90	9.78	S1	0.00	S1	60.68	S1	50.90	S1
L 6 U 6 B	50.90	7.14	S1	-65.56	S1	58.04	S1	-14.66	S1
L 7 U 7 T	-61.21	63.61	S1	-49.69	S1	2.40	S1	-110.90	S1
L 7 U 7 B	-61.21	35.76	S1	-60.70	S1	-25.45	S1	-121.91	S1
L 8 U 8 T	-215.01	52.57	S1	-54.27	S1	-162.45	S1	-269.28	S1
L 8 U 8 B	-215.01	16.91	S1	-63.91	S1	-198.10	S1	-278.92	S1
L 9 U 9 T	224.53	76.03	S1	0.00	S1	300.56	S1	224.53	S1
L 9 U 9 B	224.53	0.00	S1	0.00	S1	224.53	S1	224.53	S1

TABLE 14.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	TOTAL	MAXIMUM TENSION	MAXIMUM COMPRESSION	MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE				
	DEAD	-----	-----	-----	-----				
	LOAD	LL+I TYPE (K)	LL+I TYPE (K)	DL+LL+I TYPE (K)	DL+LL+I TYPE (K)				
L 1 U 2	-1442.84	0.00	S1	-159.27	S1	-1442.84	S1	-1602.11	S1
U 2 L 3	588.46	85.38	S1	-22.59	S1	673.84	S1	565.87	S1
U 3 L 4	351.79	74.64	S1	-43.97	S1	426.43	S1	307.82	S1
U 4 L 5	213.89	73.98	S1	-54.04	S1	287.87	S1	159.85	S1
L 5 U 6	0.00	0.00	S1	0.00	S1	0.00	S1	0.00	S1
U 5 L 6	-2.01	65.30	S1	-65.30	S1	63.28	S1	-67.31	S1
L 6 U 7	218.02	73.98	S1	-54.04	S1	292.01	S1	163.98	S1
L 7 U 8	356.07	74.64	S1	-43.97	S1	430.71	S1	312.10	S1
L 8 U 9	591.98	85.38	S1	-22.59	S1	677.36	S1	569.39	S1
U 9 L10	-1430.60	0.00	S1	-159.27	S1	-1430.60	S1	-1589.87	S1

TABLE 14.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS P411 FOR ONE LANE TO BE ADDED
TO THREE LANES OF HS TRUCKS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	-	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)				(K)		(K)		(K)	
L 1 L 2	956.65	126.53	S1		0.00	S1	1083.18	S1	956.65	S1		
L 2 L 3	956.66	126.53	S1		0.00	S1	1083.19	S1	956.66	S1		
L 3 L 4	1346.82	177.61	S1		0.00	S1	1524.43	S1	1346.82	S1		
L 4 L 5	1551.52	201.04	S1		0.00	S1	1752.56	S1	1551.52	S1		
L 5 L 6	1667.00	212.76	S1		0.00	S1	1879.76	S1	1667.00	S1		
L 6 L 7	1548.23	201.04	S1		0.00	S1	1749.27	S1	1548.23	S1		
L 7 L 8	1341.05	177.61	S1		0.00	S1	1518.65	S1	1341.05	S1		
L 8 L 9	948.54	126.53	S1		0.00	S1	1075.07	S1	948.54	S1		
L 9 L10	948.54	126.53	S1		0.00	S1	1075.07	S1	948.54	S1		

TABLE 14.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	---	---	---	---	---	
	LOAD	LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
U 2 U 3	-1394.60	0.00	S1	-183.91	S1	-1394.60	S1	-1578.51	S1
U 3 U 4	-1571.57	0.00	S1	-203.64	S1	-1571.57	S1	-1775.21	S1
U 4 U 5	-1669.42	0.00	S1	-213.06	S1	-1669.42	S1	-1882.48	S1
U 5 U 6	-1665.94	0.00	S1	-212.76	S1	-1665.94	S1	-1878.70	S1
U 6 U 7	-1668.36	0.00	S1	-213.06	S1	-1668.36	S1	-1881.42	S1
U 7 U 8	-1568.24	0.00	S1	-203.64	S1	-1568.24	S1	-1771.87	S1
U 8 U 9	-1388.62	0.00	S1	-183.91	S1	-1388.62	S1	-1572.52	S1

TABLE 14.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER LCT	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE	
	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	
L 2 U 2 T	233.39	82.63	S1	0.00	S1	316.02	S1	233.39	S1
L 2 U 2 B	233.39	0.00	S1	0.00	S1	233.39	S1	233.39	S1
L 3 U 3 T	-210.98	46.91	S1	-62.41	S1	-164.07	S1	-273.40	S1
L 3 U 3 B	-210.98	18.30	S1	-75.09	S1	-192.69	S1	-286.07	S1
L 4 U 4 T	-57.26	62.25	S1	-55.33	S1	5.00	S1	-112.59	S1
L 4 U 4 B	-57.26	31.65	S1	-69.82	S1	-25.61	S1	-127.07	S1
L 5 U 5 T	52.67	69.61	S1	-50.81	S1	122.28	S1	1.86	S1
L 5 U 5 B	52.67	43.98	S1	-69.51	S1	96.65	S1	-16.84	S1
L 6 U 6 T	50.90	11.46	S1	0.00	S1	62.36	S1	50.90	S1
L 6 U 6 B	50.90	7.52	S1	-71.09	S1	58.42	S1	-20.19	S1
L 7 U 7 T	-61.21	62.25	S1	-55.33	S1	1.05	S1	-116.54	S1
L 7 U 7 B	-61.21	31.65	S1	-69.82	S1	-29.56	S1	-131.03	S1
L 8 U 8 T	-215.01	46.91	S1	-62.41	S1	-168.10	S1	-277.42	S1
L 8 U 8 B	-215.01	18.30	S1	-75.09	S1	-196.72	S1	-290.10	S1
L 9 U 9 T	224.53	82.63	S1	0.00	S1	307.16	S1	224.53	S1
L 9 U 9 B	224.53	0.00	S1	0.00	S1	224.53	S1	224.53	S1

TABLE 14.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		LL+I (K)	TYPE (K)	LL+I (K)	TYPE (K)	DL+LL+I (K)	TYPE (K)	DL+LL+I (K)	TYPE (K)
		(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)
L 1 U 2	-1442.84	0.00	S1	-190.84	S1	-1442.84	S1	-1633.68	S1
U 2 L 3	588.46	100.31	S1	-24.44	S1	688.77	S1	564.02	S1
U 3 L 4	351.79	85.84	S1	-38.91	S1	437.64	S1	312.88	S1
U 4 L 5	213.89	82.58	S1	-52.25	S1	296.48	S1	161.64	S1
L 5 U 6	0.00	0.00	S1	0.00	S1	0.00	S1	0.00	S1
U 5 L 6	-2.01	69.61	S1	-69.61	S1	67.60	S1	-71.62	S1
L 6 U 7	218.02	82.58	S1	-52.25	S1	300.61	S1	165.78	S1
L 7 U 8	356.07	85.84	S1	-38.91	S1	441.91	S1	317.16	S1
L 8 U 9	591.98	100.31	S1	-24.44	S1	692.29	S1	567.54	S1
U 9 L10	-1430.60	0.00	S1	-190.84	S1	-1430.60	S1	-1621.44	S1

TABLE 14.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORIED)

STATE VEHICLE S1 LOADING RESULTS P413 FOR ONE LANE TO BE ADDED
TO THREE LANES OF HS TRUCKS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)				(K)		(K)		(K)	
L 1 L 2	956.65	147.63	S1		0.00	S1	1104.29	S1	956.65	S1		
L 2 L 3	956.66	147.63	S1		0.00	S1	1104.29	S1	956.66	S1		
L 3 L 4	1346.82	205.49	S1		0.00	S1	1552.31	S1	1346.82	S1		
L 4 L 5	1551.52	233.71	S1		0.00	S1	1785.23	S1	1551.52	S1		
L 5 L 6	1667.00	248.84	S1		0.00	S1	1915.84	S1	1667.00	S1		
L 6 L 7	1548.23	233.71	S1		0.00	S1	1781.94	S1	1548.23	S1		
L 7 L 8	1341.05	205.49	S1		0.00	S1	1546.53	S1	1341.05	S1		
L 8 L 9	948.54	147.63	S1		0.00	S1	1096.17	S1	948.54	S1		
L 9 L10	948.54	147.63	S1		0.00	S1	1096.17	S1	948.54	S1		

TABLE 14.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	COMPRESSION	MEMBER	FORCE	MEMBER	FORCE	
	LOAD	LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
U 2 U 3	-1394.60	0.00	S1	-212.78	S1	-1394.60	S1	-1607.38	S1
U 3 U 4	-1571.57	0.00	S1	-236.73	S1	-1571.57	S1	-1808.30	S1
U 4 U 5	-1669.42	0.00	S1	-249.20	S1	-1669.42	S1	-1918.62	S1
U 5 U 6	-1665.94	0.00	S1	-248.84	S1	-1665.94	S1	-1914.78	S1
U 6 U 7	-1668.36	0.00	S1	-249.20	S1	-1668.36	S1	-1917.56	S1
U 7 U 8	-1568.24	0.00	S1	-236.73	S1	-1568.24	S1	-1804.97	S1
U 8 U 9	-1388.62	0.00	S1	-212.78	S1	-1388.62	S1	-1601.39	S1

TABLE 14.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER LCT	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM	
	TOTAL LOAD	DEAD LOAD	TENSION LL+I TYPE	COMPRESSION LL+I TYPE	MEMBER FORCE DL+LL+I TYPE	MEMBER FORCE DL+LL+I TYPE		
	(K)	(K)	(K)	(K)	(K)	(K)		
L 2 U 2 T	233.39	76.85	S1	0.00	S1	310.25	S1	233.39
L 2 U 2 B	233.39	0.00	S1	0.00	S1	233.39	S1	233.39
L 3 U 3 T	-210.98	49.96	S1	-70.33	S1	-161.03	S1	-281.31
L 3 U 3 B	-210.98	16.12	S1	-86.32	S1	-194.87	S1	-297.30
L 4 U 4 T	-57.26	63.39	S1	-60.71	S1	6.13	S1	-117.96
L 4 U 4 B	-57.26	33.76	S1	-79.03	S1	-23.50	S1	-136.29
L 5 U 5 T	52.67	74.12	S1	-54.03	S1	126.79	S1	-1.36
L 5 U 5 B	52.67	44.80	S1	-77.29	S1	97.47	S1	-24.63
L 6 U 6 T	50.90	13.41	S1	0.00	S1	64.31	S1	50.90
L 6 U 6 B	50.90	7.85	S1	-64.36	S1	58.75	S1	-13.45
L 7 U 7 T	-61.21	63.39	S1	-60.71	S1	2.18	S1	-121.91
L 7 U 7 B	-61.21	33.76	S1	-79.03	S1	-27.45	S1	-140.24
L 8 U 8 T	-215.01	49.96	S1	-70.33	S1	-165.05	S1	-285.34
L 8 U 8 B	-215.01	16.12	S1	-86.32	S1	-198.90	S1	-301.33
L 9 U 9 T	224.53	76.85	S1	0.00	S1	301.39	S1	224.53
L 9 U 9 B	224.53	0.00	S1	0.00	S1	224.53	S1	224.53

TABLE 14.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE S1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE
	(K)	(K)	(K)				(K)	(K)	(K)
L 1 U 2	-1442.84	0.00	S1	-222.66	S1	-1442.84	S1	-1665.50	S1
U 2 L 3	588.46	115.31	S1	-21.53	S1	703.77	S1	566.93	S1
U 3 L 4	351.79	97.17	S1	-41.51	S1	448.97	S1	310.29	S1
U 4 L 5	213.89	91.83	S1	-53.22	S1	305.72	S1	160.67	S1
L 5 U 6	0.00	0.00	S1	0.00	S1	0.00	S1	0.00	S1
U 5 L 6	-2.01	74.17	S1	-74.17	S1	72.16	S1	-76.18	S1
L 6 U 7	218.02	91.83	S1	-53.22	S1	309.85	S1	164.80	S1
L 7 U 8	356.07	97.17	S1	-41.51	S1	453.25	S1	314.56	S1
L 8 U 9	591.98	115.31	S1	-21.53	S1	707.29	S1	570.46	S1
U 9 L10	-1430.60	0.00	S1	-222.66	S1	-1430.60	S1	-1653.26	S1

TABLE 11.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORIED)

STATE VEHICLE T1 LOADING RESULTS **TYPE M3**

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-	-	-	-	-	
	LOAD	LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE	(K)
L 1 L 2	956.65	93.49	T1	0.00	T1	1050.15	T1	956.65	T1
L 2 L 3	956.66	93.49	T1	0.00	T1	1050.15	T1	956.66	T1
L 3 L 4	1346.82	131.57	T1	0.00	T1	1478.40	T1	1346.82	T1
L 4 L 5	1551.52	150.77	T1	0.00	T1	1702.29	T1	1551.52	T1
L 5 L 6	1667.00	161.60	T1	0.00	T1	1828.60	T1	1667.00	T1
L 6 L 7	1548.23	150.77	T1	0.00	T1	1699.00	T1	1548.23	T1
L 7 L 8	1341.05	131.57	T1	0.00	T1	1472.62	T1	1341.05	T1
L 8 L 9	948.54	93.49	T1	0.00	T1	1042.03	T1	948.54	T1
L 9 L10	948.54	93.49	T1	0.00	T1	1042.03	T1	948.54	T1

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TABLE 11.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE T1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-----	COMPRESSION	MEMBER FORCE	-----	MEMBER FORCE	
	LOAD	LL+I TYPE	LOAD	-----	LL+I TYPE	DL+LL+I TYPE	-----	DL+LL+I TYPE	
U 2 U 3	-1394.60	0.00	T1	-136.24	T1	-1394.60	T1	-1530.84	T1
U 3 U 4	-1571.57	0.00	T1	-152.72	T1	-1571.57	T1	-1724.29	T1
U 4 U 5	-1669.42	0.00	T1	-161.83	T1	-1669.42	T1	-1831.25	T1
U 5 U 6	-1665.94	0.00	T1	-161.60	T1	-1665.94	T1	-1827.54	T1
U 6 U 7	-1668.36	0.00	T1	-161.83	T1	-1668.36	T1	-1830.19	T1
U 7 U 8	-1568.24	0.00	T1	-152.72	T1	-1568.24	T1	-1720.95	T1
U 8 U 9	-1388.62	0.00	T1	-136.24	T1	-1388.62	T1	-1524.86	T1

TABLE 11.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE T1 LOADING RESULTS

MEMBER LCT	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	LOAD	LL+I	TYPE	LL+I	TYPE	MEMBER FORCE
	(K)	MEMBER FORCE							
L 2 U 2 T	233.39	110.63	T1	0.00	T1	344.02	T1	233.39	T1
L 2 U 2 B	233.39	0.00	T1	0.00	T1	233.39	T1	233.39	T1
L 3 U 3 T	-210.98	62.22	T1	-49.54	T1	-148.76	T1	-260.52	T1
L 3 U 3 B	-210.98	28.05	T1	-57.32	T1	-182.93	T1	-268.31	T1
L 4 U 4 T	-57.26	65.62	T1	-46.54	T1	8.36	T1	-103.80	T1
L 4 U 4 B	-57.26	43.16	T1	-55.41	T1	-14.10	T1	-112.67	T1
L 5 U 5 T	52.67	63.10	T1	-46.96	T1	115.77	T1	5.71	T1
L 5 U 5 B	52.67	47.43	T1	-58.32	T1	100.09	T1	-5.66	T1
L 6 U 6 T	50.90	8.71	T1	0.00	T1	59.61	T1	50.90	T1
L 6 U 6 B	50.90	6.96	T1	-101.34	T1	57.86	T1	-50.44	T1
L 7 U 7 T	-61.21	65.62	T1	-46.54	T1	4.41	T1	-107.75	T1
L 7 U 7 B	-61.21	43.16	T1	-55.41	T1	-18.05	T1	-116.62	T1
L 8 U 8 T	-215.01	62.22	T1	-49.54	T1	-152.79	T1	-264.55	T1
L 8 U 8 B	-215.01	28.05	T1	-57.32	T1	-186.96	T1	-272.33	T1
L 9 U 9 T	224.53	110.63	T1	0.00	T1	335.16	T1	224.53	T1
L 9 U 9 B	224.53	0.00	T1	0.00	T1	224.53	T1	224.53	T1

TABLE 11.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE T1 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE
	(K)	(K)	(K)		(K)		(K)		(K)
L 1 U 2	-1442.84	0.00	T1	-141.01	T1	-1442.84	T1	-1583.85	T1
U 2 L 3	588.46	76.57	T1	-37.47	T1	665.03	T1	550.99	T1
U 3 L 4	351.79	68.13	T1	-53.07	T1	419.93	T1	298.73	T1
U 4 L 5	213.89	69.29	T1	-56.34	T1	283.18	T1	157.55	T1
L 5 U 6	0.00	0.00	T1	0.00	T1	0.00	T1	0.00	T1
U 5 L 6	-2.01	63.69	T1	-63.69	T1	61.68	T1	-65.70	T1
L 6 U 7	218.02	69.29	T1	-56.34	T1	287.31	T1	161.68	T1
L 7 U 8	356.07	68.13	T1	-53.07	T1	424.20	T1	303.00	T1
L 8 U 9	591.98	76.57	T1	-37.47	T1	668.56	T1	554.51	T1
U 9 L10	-1430.60	0.00	T1	-141.01	T1	-1430.60	T1	-1571.61	T1

TABLE 12.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

STATE VEHICLE T2 LOADING RESULTS **TYPE M3-S2**

MEMBER	MAXIMUM			MAXIMUM			MAXIMUM			MINIMUM	
	TOTAL	TENSION		COMPRESSION		MEMBER FORCE		MEMBER FORCE		MEMBER FORCE	
	DEAD	LOAD	TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)		(K)		(K)		(K)		(K)	
L 1 L 2	956.65	128.38	T2	0.00	T2	1085.03	T2	956.65	T2		
L 2 L 3	956.66	128.38	T2	0.00	T2	1085.03	T2	956.66	T2		
L 3 L 4	1346.82	179.68	T2	0.00	T2	1526.50	T2	1346.82	T2		
L 4 L 5	1551.52	206.73	T2	0.00	T2	1758.25	T2	1551.52	T2		
L 5 L 6	1667.00	220.93	T2	0.00	T2	1887.93	T2	1667.00	T2		
L 6 L 7	1548.23	206.73	T2	0.00	T2	1754.96	T2	1548.23	T2		
L 7 L 8	1341.05	179.68	T2	0.00	T2	1520.73	T2	1341.05	T2		
L 8 L 9	948.54	128.38	T2	0.00	T2	1076.92	T2	948.54	T2		
L 9 L10	948.54	128.38	T2	0.00	T2	1076.92	T2	948.54	T2		

TABLE 12.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE T2 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)				(K)		(K)		(K)	
U 2 U 3	-1394.60	0.00	T2	-186.05	T2	-1394.60	T2	-1394.60	T2	-1580.66	T2	
U 3 U 4	-1571.57	0.00	T2	-209.40	T2	-1571.57	T2	-1571.57	T2	-1780.97	T2	
U 4 U 5	-1669.42	0.00	T2	-221.25	T2	-1669.42	T2	-1669.42	T2	-1890.67	T2	
U 5 U 6	-1665.94	0.00	T2	-220.93	T2	-1665.94	T2	-1665.94	T2	-1886.87	T2	
U 6 U 7	-1668.36	0.00	T2	-221.25	T2	-1668.36	T2	-1668.36	T2	-1889.60	T2	
U 7 U 8	-1568.24	0.00	T2	-209.40	T2	-1568.24	T2	-1568.24	T2	-1777.64	T2	
U 8 U 9	-1388.62	0.00	T2	-186.05	T2	-1388.62	T2	-1388.62	T2	-1574.67	T2	

TABLE 12.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE T2 LOADING RESULTS

MEMBER LCT	MAXIMUM		MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE	
	TOTAL DEAD	TENSION		DL+LL+I TYPE	DL+LL+I TYPE
	LOAD	LL+I TYPE	(K)	(K)	(K)
L 2 U 2 T	233.39	113.66	T2	0.00	T2
L 2 U 2 B	233.39	0.00	T2	0.00	T2
L 3 U 3 T	-210.98	71.64	T2	-66.87	T2
L 3 U 3 B	-210.98	23.86	T2	-78.14	T2
L 4 U 4 T	-57.26	82.15	T2	-61.94	T2
L 4 U 4 B	-57.26	49.42	T2	-74.80	T2
L 5 U 5 T	52.67	82.15	T2	-61.14	T2
L 5 U 5 B	52.67	59.38	T2	-77.63	T2
L 6 U 6 T	50.90	11.90	T2	0.00	T2
L 6 U 6 B	50.90	9.06	T2	-100.88	T2
L 7 U 7 T	-61.21	82.15	T2	-61.94	T2
L 7 U 7 B	-61.21	49.42	T2	-74.80	T2
L 8 U 8 T	-215.01	71.64	T2	-66.87	T2
L 8 U 8 B	-215.01	23.86	T2	-78.14	T2
L 9 U 9 T	224.53	113.66	T2	0.00	T2
L 9 U 9 B	224.53	0.00	T2	0.00	T2

TABLE 12.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE T2 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM		
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE
	(K)	(K)	(K)		(K)		(K)		(K)
L 1 U 2	-1442.84	0.00	T2	-193.62	T2	-1442.84	T2	-1636.46	T2
U 2 L 3	588.46	104.39	T2	-31.88	T2	692.85	T2	556.58	T2
U 3 L 4	351.79	91.97	T2	-60.77	T2	443.77	T2	291.02	T2
U 4 L 5	213.89	92.22	T2	-70.54	T2	306.12	T2	143.35	T2
L 5 U 6	0.00	0.00	T2	0.00	T2	0.00	T2	0.00	T2
U 5 L 6	-2.01	82.93	T2	-82.93	T2	80.92	T2	-84.94	T2
L 6 U 7	218.02	92.22	T2	-70.54	T2	310.25	T2	147.48	T2
L 7 U 8	356.07	91.97	T2	-60.77	T2	448.04	T2	295.30	T2
L 8 U 9	591.98	104.39	T2	-31.88	T2	696.37	T2	560.11	T2
U 9 L10	-1430.60	0.00	T2	-193.62	T2	-1430.60	T2	-1624.22	T2

TABLE 13.1 DL+LL+I FORCE SUMMARY FOR LOWER CHORD MEMBERS (FACTORED)

STATE VEHICLE T3 LOADING RESULTS **TYPE M3-3**

MEMBER	MAXIMUM		MAXIMUM MEMBER FORCE	MINIMUM					
	TOTAL	TENSION		COMPRESSION	MEMBER FORCE				
	DEAD	-----		-----	-----				
	LOAD	LL+I TYPE	LL+I TYPE	DL+LL+I TYPE	DL+LL+I TYPE				
	(K)	(K)	(K)	(K)	(K)				
L 1 L 2	956.65	139.35	T3	0.00	T3	1096.01	T3	956.65	T3
L 2 L 3	956.66	139.35	T3	0.00	T3	1096.01	T3	956.66	T3
L 3 L 4	1346.82	194.84	T3	0.00	T3	1541.66	T3	1346.82	T3
L 4 L 5	1551.52	222.30	T3	0.00	T3	1773.82	T3	1551.52	T3
L 5 L 6	1667.00	238.40	T3	0.00	T3	1905.40	T3	1667.00	T3
L 6 L 7	1548.23	222.30	T3	0.00	T3	1770.53	T3	1548.23	T3
L 7 L 8	1341.05	194.84	T3	0.00	T3	1535.88	T3	1341.05	T3
L 8 L 9	948.54	139.35	T3	0.00	T3	1087.89	T3	948.54	T3
L 9 L10	948.54	139.35	T3	0.00	T3	1087.89	T3	948.54	T3

TABLE 13.2 DL+LL+I FORCE SUMMARY FOR UPPER CHORD MEMBERS (FACTORED)

STATE VEHICLE T3 LOADING RESULTS

MEMBER	TOTAL	MAXIMUM TENSION	MAXIMUM COMPRESSION	MAXIMUM MEMBER FORCE	MINIMUM MEMBER FORCE
	DEAD	-----	-----	-----	-----
	LOAD	LL+I TYPE (K)	LL+I TYPE (K)	DL+LL+I TYPE (K)	DL+LL+I TYPE (K)
U 2 U 3	-1394.60	0.00	T3 -201.75	T3 -1394.60	T3 -1596.35
U 3 U 4	-1571.57	0.00	T3 -225.17	T3 -1571.57	T3 -1796.75
U 4 U 5	-1669.42	0.00	T3 -238.75	T3 -1669.42	T3 -1908.17
U 5 U 6	-1665.94	0.00	T3 -238.40	T3 -1665.94	T3 -1904.34
U 6 U 7	-1668.36	0.00	T3 -238.75	T3 -1668.36	T3 -1907.10
U 7 U 8	-1568.24	0.00	T3 -225.17	T3 -1568.24	T3 -1793.41
U 8 U 9	-1388.62	0.00	T3 -201.75	T3 -1388.62	T3 -1590.37

TABLE 13.4 DL+LL+I FORCE SUMMARY FOR VERTICAL MEMBERS (FACTORED)

STATE VEHICLE T3 LOADING RESULTS

MEMBER LCT	TOTAL DEAD LOAD	MAXIMUM TENSION		MAXIMUM COMPRESSION		MAXIMUM MEMBER FORCE		MINIMUM MEMBER FORCE	
		(K)	LL+I TYPE	(K)	LL+I TYPE	(K)	DL+LL+I TYPE	(K)	DL+LL+I TYPE
L 2 U 2 T	233.39	106.54	T3	0.00	T3	339.93	T3	233.39	T3
L 2 U 2 B	233.39	0.00	T3	0.00	T3	233.39	T3	233.39	T3
L 3 U 3 T	-210.98	70.98	T3	-71.95	T3	-140.01	T3	-282.94	T3
L 3 U 3 B	-210.98	23.53	T3	-84.51	T3	-187.46	T3	-295.49	T3
L 4 U 4 T	-57.26	84.79	T3	-66.16	T3	27.53	T3	-123.41	T3
L 4 U 4 B	-57.26	48.37	T3	-80.49	T3	-8.89	T3	-137.74	T3
L 5 U 5 T	52.67	86.70	T3	-64.52	T3	139.37	T3	-11.85	T3
L 5 U 5 B	52.67	61.28	T3	-82.91	T3	113.95	T3	-30.24	T3
L 6 U 6 T	50.90	12.84	T3	0.00	T3	63.74	T3	50.90	T3
L 6 U 6 B	50.90	9.57	T3	-92.58	T3	60.47	T3	-41.68	T3
L 7 U 7 T	-61.21	84.79	T3	-66.16	T3	23.58	T3	-127.37	T3
L 7 U 7 B	-61.21	48.37	T3	-80.49	T3	-12.84	T3	-141.70	T3
L 8 U 8 T	-215.01	70.98	T3	-71.95	T3	-144.04	T3	-286.96	T3
L 8 U 8 B	-215.01	23.53	T3	-84.51	T3	-191.48	T3	-299.52	T3
L 9 U 9 T	224.53	106.54	T3	0.00	T3	331.07	T3	224.53	T3
L 9 U 9 B	224.53	0.00	T3	0.00	T3	224.53	T3	224.53	T3

TABLE 13.5 DL+LL+I FORCE SUMMARY FOR DIAGONAL MEMBERS (FACTORED)

STATE VEHICLE T3 LOADING RESULTS

MEMBER	MAXIMUM		MAXIMUM		MAXIMUM		MINIMUM					
	TOTAL	TENSION	DEAD	-----	LOAD	LL+I TYPE	LL+I	TYPE	DL+LL+I	TYPE	DL+LL+I	TYPE
	(K)	(K)	(K)		(K)		(K)		(K)		(K)	
L 1 U 2	-1442.84	0.00	T3	-210.17	T3	-1442.84	T3	-1442.84	T3	-1653.01	T3	
U 2 L 3	588.46	112.89	T3	-31.43	T3	701.35	T3	557.03	T3	557.03	T3	
U 3 L 4	351.79	98.96	T3	-59.47	T3	450.76	T3	292.33	T3	292.33	T3	
U 4 L 5	213.89	98.50	T3	-72.81	T3	312.39	T3	141.08	T3	141.08	T3	
L 5 U 6	0.00	0.00	T3	0.00	T3	0.00	T3	0.00	T3	0.00	T3	
U 5 L 6	-2.01	87.52	T3	-87.52	T3	85.51	T3	-89.53	T3	-89.53	T3	
L 6 U 7	218.02	98.50	T3	-72.81	T3	316.52	T3	145.22	T3	145.22	T3	
L 7 U 8	356.07	98.96	T3	-59.47	T3	455.04	T3	296.60	T3	296.60	T3	
L 8 U 9	591.98	112.89	T3	-31.43	T3	704.88	T3	560.55	T3	560.55	T3	
U 9 L10	-1430.60	0.00	T3	-210.17	T3	-1430.60	T3	-1640.78	T3	-1640.78	T3	

Rating Factory
Summary

TABLE 16.7 SUMMARY OF INVENTORY AND OPERATING RATING (L F D)

AASHTO LIVE LOADING

INVENTORY RATING DATA	OPERATING RATING DATA	MILITARY LOADING
AASHTO LOAD NAME	AASHTO LOAD NAME	YES OR NO
HS-20 0.55 0.60	HS-20 0.75 0.90	NO
+		
+		

RATING ANALYSIS SUMMARY

INVENTORY RATING RESULTS			OPERATING RATING RESULTS		
RATING FACTOR	CRITICAL MEMBER	CONTROLLING LIVE LOAD	RATING FACTOR	CRITICAL MEMBER	CONTROLLING LIVE LOAD
0.84	U 5 L 6	L	1.41	U 5 L 6	L
+					

NOTE: For capacity less than force due to dead load, rating will be 0

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TABLE 16.8 SUMMARY OF POSTING VEHICLE RATING (L F D)

STATE VEHICULAR LOADING - T1

VEHICLE NAME	SAFE LOAD CAPACITY	CRITICAL MEMBER
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TYPE 3	2.12	U 5 L 6
--------	------	---------

STATE VEHICULAR LOADING - T2

VEHICLE NAME	SAFE LOAD CAPACITY	CRITICAL MEMBER
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TYPE 3S2	1.62	U 5 L 6
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STATE VEHICULAR LOADING - T3

VEHICLE NAME	SAFE LOAD CAPACITY	CRITICAL MEMBER
-----------------	-----------------------	--------------------

TYPE 3-3	1.54	U 5 L 6
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SPECIAL TRUCK LOADING - S1

VEHICLE NAME	DESCRIPTION	RATING RESULTS
		SAFE LOAD CRITICAL
	NO OF AXLES	CAPACITY MEMBER
	TOTAL WEIGHT (K or KN)	FACTOR
0	0.00	99.00 L 1 L 2

NOTE: For capacity less than force due to dead load, rating will be 0

TABLE 16.1 DL+LL+I RATING SUMMARY FOR LOWER CHORD MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	STATE	STATE	STATE	SPECIAL	SPECIAL
	AASHTO	AASHTO	VEHICLE 1	VEHICLE 2	VEHICLE 3	VEHICLE 1	VEHICLE 2
	MAX T & C	MAX T & C	MAX T & C	MAX T & C	MAX T & C	MAX T & C	MAX T & C
L 1 L 2	9.18 99.00	15.31 99.00	33.86 99.00	24.66 99.00	22.71 99.00	99.00 99.00	0.00 0.00
L 2 L 3	3.31 99.00	5.51 99.00	12.20 99.00	8.88 99.00	8.18 99.00	99.00 99.00	0.00 0.00
L 3 L 4	1.54 99.00	2.57 99.00	5.70 99.00	4.18 99.00	3.85 99.00	99.00 99.00	0.00 0.00
L 4 L 5	1.55 99.00	2.58 99.00	5.77 99.00	4.21 99.00	3.91 99.00	99.00 99.00	0.00 0.00
L 5 L 6	1.61 99.00	2.68 99.00	6.00 99.00	4.39 99.00	4.07 99.00	99.00 99.00	0.00 0.00
L 6 L 7	1.55 99.00	2.59 99.00	5.79 99.00	4.22 99.00	3.93 99.00	99.00 99.00	0.00 0.00
L 7 L 8	1.55 99.00	2.59 99.00	5.75 99.00	4.21 99.00	3.88 99.00	99.00 99.00	0.00 0.00
L 8 L 9	2.83 99.00	4.71 99.00	10.41 99.00	7.58 99.00	6.99 99.00	99.00 99.00	0.00 0.00
L 9 L10	2.83 99.00	4.71 99.00	10.41 99.00	7.58 99.00	6.99 99.00	99.00 99.00	0.00 0.00

TABLE 16.2 DL+LL+I RATING SUMMARY FOR UPPER CHORD MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	STATE	STATE	STATE	SPECIAL	SPECIAL
	AASHTO	AASHTO	VEHICLE 1	VEHICLE 2	VEHICLE 3	VEHICLE 1	VEHICLE 2
	MAX T & C						
U 2 U 3	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.67	2.78	6.18	4.52	4.17	99.00	0.00
U 3 U 4	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.52	2.54	5.68	4.14	3.85	99.00	0.00
U 4 U 5	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.62	2.69	6.03	4.41	4.09	99.00	0.00
U 5 U 6	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.63	2.71	6.07	4.44	4.11	99.00	0.00
U 6 U 7	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.62	2.70	6.04	4.42	4.09	99.00	0.00
U 7 U 8	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.53	2.55	5.70	4.16	3.87	99.00	0.00
U 8 U 9	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.68	2.80	6.22	4.56	4.20	99.00	0.00

TABLE 16.4 DL+LL+I RATING SUMMARY FOR VERTICAL MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	STATE	STATE	STATE	SPECIAL	SPECIAL
	AASHTO	AASHTO	VEHICLE 1	VEHICLE 2	VEHICLE 3	VEHICLE 1	VEHICLE 2
	MAX T & C						
L 2 U 2T	3.83	6.39	8.60	8.37	8.93	99.00	0.00
	99.00	99.00	99.00	99.00	99.00	99.00	0.00
L 2 U 2B	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	99.00	99.00	99.00	99.00	99.00	99.00	0.00
L 3 U 3T	2.57	4.28	5.96	5.17	5.22	99.00	0.00
	2.63	4.39	7.48	5.54	5.15	99.00	0.00
L 3 U 3B	99.00	9.98	99.00	99.00	99.00	99.00	0.00
	2.00	3.33	6.47	4.74	4.39	99.00	0.00
L 4 U 4T	6.42	10.70	15.06	12.03	11.66	99.00	0.00
	4.05	6.75	10.17	7.64	7.15	99.00	0.00
L 4 U 4B	99.00	16.48	99.00	99.00	99.00	99.00	0.00
	2.96	4.93	8.54	6.32	5.88	99.00	0.00
L 5 U 5T	5.90	9.83	13.92	10.69	10.13	99.00	0.00
	5.09	8.49	18.71	9.24	8.75	99.00	0.00
L 5 U 5B	99.00	13.16	99.00	99.00	99.00	99.00	0.00
	3.78	6.31	9.68	7.27	6.81	99.00	0.00
L 6 U 6T	27.09	45.16	99.00	73.97	68.55	99.00	0.00
	99.00	99.00	99.00	99.00	99.00	99.00	0.00
L 6 U 6B	99.00	68.55	99.00	99.00	99.00	99.00	0.00
	2.49	4.15	5.55	5.58	6.08	99.00	0.00

TABLE 16.4 DL+LL+I RATING SUMMARY FOR VERTICAL MEMBERS (L F D)

TABLE 16.5 DL+LL+I RATING SUMMARY FOR DIAGONAL MEMBERS (L F D)

MEMBER	INVENTORY	OPERATING	STATE	STATE	STATE	SPECIAL	SPECIAL
	AASHTO	AASHTO	VEHICLE 1	VEHICLE 2	VEHICLE 3	VEHICLE 1	VEHICLE 2
	MAX T & C						
L 1 U 2	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.40	2.33	5.54	4.03	3.72	99.00	0.00
U 2 L 3	3.30	5.50	11.60	8.51	7.87	99.00	0.00
	10.74	17.89	23.69	27.85	28.25	99.00	0.00
U 3 L 4	2.57	4.28	8.12	6.02	5.59	99.00	0.00
	4.50	7.50	10.43	9.11	9.31	99.00	0.00
U 4 L 5	2.74	4.56	7.77	5.83	5.46	99.00	0.00
	4.07	6.78	9.55	7.63	7.39	99.00	0.00
L 5 U 6	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	99.00	99.00	99.00	99.00	99.00	99.00	0.00
U 5 L 6	3.90	6.50	9.77	7.51	7.11	99.00	0.00
	0.84	1.41	2.12	1.62	1.54	99.00	0.00
L 6 U 7	2.05	3.41	5.81	4.36	4.09	99.00	0.00
	3.04	5.07	7.14	5.70	5.53	99.00	0.00
L 7 U 8	1.84	3.06	5.81	4.30	4.00	99.00	0.00
	3.22	5.37	7.46	6.52	6.66	99.00	0.00
L 8 U 9	1.57	2.62	5.54	4.06	3.76	99.00	0.00
	5.13	8.54	11.31	13.30	13.49	99.00	0.00
U 9 L10	99.00	99.00	99.00	99.00	99.00	99.00	0.00
	1.42	2.37	5.63	4.10	3.78	99.00	0.00

**RATING FACTORS FOR PERMIT
TRUCKS CALCULATED
MANUALLY. REFER TO LOAD
AND RATING SUMMARY
SPREADSHEET FOR
INFORMATION.**

Member Latifuna
LNU Latifuna

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unit force
apply to bottom
chord only.



Project: Mn/DOT Truss Ratings
Bridge No. 9090 - TH 2 Over Red River - Grand Forks
LHB Project No: 070745.30

UNIT FORCE INFLUENCE LINES

	PANEL POINTS										
Members	1	2	3	4	5	6	7	8	9	10	
BOTTOM CHORD	L1-L2	0.000	0.787	0.689	0.590	0.492	0.394	0.295	0.197	0.098	0.000
	L2-L3	0.000	0.787	0.689	0.590	0.492	0.394	0.295	0.197	0.098	0.000
	L3-L4	0.000	0.556	1.113	0.954	0.795	0.636	0.477	0.318	0.159	0.000
	L4-L5	0.000	0.428	0.855	1.283	1.069	0.855	0.641	0.428	0.214	0.000
	L5-L6	0.000	0.344	0.689	1.033	1.378	1.102	0.827	0.551	0.276	0.000
	L6-L7	0.000	0.214	0.428	0.641	0.855	1.069	1.283	0.855	0.428	0.000
	L7-L8	0.000	0.159	0.318	0.477	0.636	0.795	0.954	1.113	0.556	0.000
	L8-L9	0.000	0.098	0.197	0.295	0.394	0.492	0.590	0.689	0.787	0.000
	L9-L10	0.000	0.098	0.197	0.295	0.394	0.492	0.590	0.689	0.787	0.000
	U2-U3	0.000	-0.576	-1.152	-0.988	-0.823	-0.659	-0.494	-0.329	-0.165	0.000
TOP CHORD	U3-U4	0.000	-0.433	-0.866	-1.299	-1.083	-0.866	-0.650	-0.433	-0.217	0.000
	U4-U5	0.000	-0.345	-0.690	-1.035	-1.380	-1.104	-0.828	-0.552	-0.276	0.000
	U5-U6	0.000	-0.276	-0.551	-0.827	-1.102	-1.378	-1.033	-0.689	-0.344	0.000
	U6-U7	0.000	-0.276	-0.552	-0.828	-1.104	-1.380	-1.035	-0.690	-0.345	0.000
	U7-U8	0.000	-0.217	-0.433	-0.650	-0.866	-1.083	-1.299	-0.866	-0.433	0.000
	U8-U9	0.000	-0.165	-0.329	-0.494	-0.659	-0.823	-0.988	-1.152	-0.576	0.000
	L2-U2	0.000	1.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
	L3-U3	0.000	0.261	0.521	-0.410	-0.342	-0.274	-0.205	-0.137	-0.068	0.000
		0.000	0.261	-0.479	-0.410	-0.342	-0.274	-0.205	-0.137	-0.068	0.000
VERTICAL MEMBERS	L4-U4	0.000	0.180	0.360	0.540	-0.383	-0.307	-0.230	-0.153	-0.077	0.000
		0.000	0.180	0.360	-0.460	-0.383	-0.307	-0.230	-0.153	-0.077	0.000
	L5-U5	0.000	0.130	0.259	0.389	0.519	-0.385	-0.289	-0.193	-0.096	0.000
		0.000	0.130	0.259	0.389	-0.481	0.385	-0.289	-0.193	-0.096	0.000
	L6-U6	0.000	0.015	0.030	0.045	0.059	0.074	0.056	0.037	0.019	0.000
		0.000	0.015	0.030	0.045	0.059	-0.926	0.056	0.037	0.019	0.000
	L7-U7	0.000	-0.077	-0.153	-0.230	-0.307	-0.383	0.540	0.360	0.180	0.000
		0.000	-0.077	-0.153	-0.230	-0.307	-0.383	-0.460	0.360	0.180	0.000
	L8-U8	0.000	-0.068	-0.137	-0.205	-0.274	-0.342	-0.410	0.521	0.261	0.000
		0.000	-0.068	-0.137	-0.205	-0.274	-0.342	-0.410	-0.479	0.261	0.000
DIAGONAL MEMBERS	L9-U9	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000
		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
	L1-U2	0.000	-1.187	-1.039	-0.891	-0.742	-0.594	-0.445	-0.297	-0.148	0.000
	L3-U2	0.000	-0.348	0.640	0.548	0.457	0.365	0.274	0.183	0.091	0.000
	L4-U3	0.000	-0.221	-0.443	0.565	0.471	0.377	0.283	0.188	0.094	0.000
	L5-U4	0.000	-0.154	-0.308	-0.462	0.572	0.457	0.343	0.229	0.114	0.000
	L5-U6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
	L6-U5	0.000	-0.131	-0.261	-0.392	-0.523	0.523	0.392	0.261	0.131	0.000
	L6-U7	0.000	0.114	0.229	0.343	0.457	0.572	-0.462	-0.308	-0.154	0.000
	L7-U8	0.000	0.094	0.188	0.283	0.377	0.471	0.565	-0.443	-0.221	0.000
	L8-U9	0.000	0.091	0.183	0.274	0.365	0.457	0.548	0.640	-0.348	0.000
	L10-U9	0.000	-0.148	-0.297	-0.445	-0.594	-0.742	-0.891	-1.039	-1.187	0.000

Unit force load applied to the top chord for information only

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 1 L 2

PP NO	ORDINATE								
1	0.000	2	0.787	3	0.689	4	0.590	5	0.492
6	0.394	7	0.295	8	0.197	9	0.098	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 2 L 3

PP NO	ORDINATE								
1	0.000	2	0.787	3	0.689	4	0.590	5	0.492
6	0.394	7	0.295	8	0.197	9	0.098	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 3 L 4

PP NO	ORDINATE								
1	0.000	2	0.556	3	1.113	4	0.954	5	0.795
6	0.636	7	0.477	8	0.318	9	0.159	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 4 L 5

PP NO	ORDINATE								
1	0.000	2	0.428	3	0.855	4	1.283	5	1.069
6	0.855	7	0.641	8	0.428	9	0.214	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 5 L 6

PP NO	ORDINATE								
1	0.000	2	0.344	3	0.689	4	1.033	5	1.378
6	1.102	7	0.827	8	0.551	9	0.276	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 6 L 7

PP NO	ORDINATE								
1	0.000	2	0.214	3	0.428	4	0.641	5	0.855
6	1.069	7	1.283	8	0.855	9	0.428	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 7 L 8

PP NO	ORDINATE								
1	0.000	2	0.159	3	0.318	4	0.477	5	0.636
6	0.795	7	0.954	8	1.113	9	0.556	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 8 L 9

PP NO	ORDINATE								
1	0.000	2	0.098	3	0.197	4	0.295	5	0.394
6	0.492	7	0.590	8	0.689	9	0.787	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 9 L10

PP NO	ORDINATE								
1	0.000	2	0.098	3	0.197	4	0.295	5	0.394
6	0.492	7	0.590	8	0.689	9	0.787	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 2 U 3

PP NO	ORDINATE								
1	0.000	2	-0.576	3	-1.152	4	-0.988	5	-0.823
6	-0.659	7	-0.494	8	-0.329	9	-0.165	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 3 U 4

PP NO	ORDINATE								
1	0.000	2	-0.433	3	-0.866	4	-1.299	5	-1.083
6	-0.866	7	-0.650	8	-0.433	9	-0.217	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 4 U 5

PP NO	ORDINATE								
1	0.000	2	-0.345	3	-0.690	4	-1.035	5	-1.380
6	-1.104	7	-0.828	8	-0.552	9	-0.276	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 5 U 6

PP NO	ORDINATE								
1	0.000	2	-0.276	3	-0.551	4	-0.827	5	-1.102
6	-1.378	7	-1.033	8	-0.689	9	-0.344	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 6 U 7

PP NO	ORDINATE								
1	0.000	2	-0.276	3	-0.552	4	-0.828	5	-1.104
6	-1.380	7	-1.035	8	-0.690	9	-0.345	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 7 U 8

PP NO	ORDINATE								
1	0.000	2	-0.217	3	-0.433	4	-0.650	5	-0.866
6	-1.083	7	-1.299	8	-0.866	9	-0.433	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 8 U 9

PP NO	ORDINATE								
1	0.000	2	-0.165	3	-0.329	4	-0.494	5	-0.659
6	-0.823	7	-0.988	8	-1.152	9	-0.576	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 2 U 2

PP NO	ORDINATE								
1	0.000	2	1.000	3	0.000	4	0.000	5	0.000
6	0.000	7	0.000	8	0.000	9	0.000	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 2 U 2

PP NO	ORDINATE								
1	0.000	2	0.000	3	0.000	4	0.000	5	0.000
6	0.000	7	0.000	8	0.000	9	0.000	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 3 U 3

PP NO	ORDINATE								
1	0.000	2	0.261	3	0.521	4	-0.410	5	-0.342
6	-0.274	7	-0.205	8	-0.137	9	-0.068	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 3 U 3

PP NO	ORDINATE								
1	0.000	2	0.261	3	-0.479	4	-0.410	5	-0.342
6	-0.274	7	-0.205	8	-0.137	9	-0.068	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 4 U 4

PP NO	ORDINATE								
1	0.000	2	0.180	3	0.360	4	0.540	5	-0.383
6	-0.307	7	-0.230	8	-0.153	9	-0.077	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 4 U 4

PP NO	ORDINATE								
1	0.000	2	0.180	3	0.360	4	-0.460	5	-0.383
6	-0.307	7	-0.230	8	-0.153	9	-0.077	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 5 U 5

PP NO	ORDINATE								
1	0.000	2	0.130	3	0.259	4	0.389	5	0.519
6	-0.385	7	-0.289	8	-0.193	9	-0.096	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 5 U 5

PP NO	ORDINATE								
1	0.000	2	0.130	3	0.259	4	0.389	5	-0.481
6	-0.385	7	-0.289	8	-0.193	9	-0.096	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 6 U 6

PP NO	ORDINATE								
1	0.000	2	0.015	3	0.030	4	0.045	5	0.059
6	0.074	7	0.056	8	0.037	9	0.019	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 6 U 6

PP NO	ORDINATE								
1	0.000	2	0.015	3	0.030	4	0.045	5	0.059
6	-0.926	7	0.056	8	0.037	9	0.019	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 7 U 7

PP NO	ORDINATE								
1	0.000	2	-0.077	3	-0.153	4	-0.230	5	-0.307
6	-0.383	7	0.540	8	0.360	9	0.180	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 7 U 7

PP NO	ORDINATE								
1	0.000	2	-0.077	3	-0.153	4	-0.230	5	-0.307
6	-0.383	7	-0.460	8	0.360	9	0.180	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 8 U 8

PP NO	ORDINATE								
1	0.000	2	-0.068	3	-0.137	4	-0.205	5	-0.274
6	-0.342	7	-0.410	8	0.521	9	0.261	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 8 U 8

PP NO	ORDINATE								
1	0.000	2	-0.068	3	-0.137	4	-0.205	5	-0.274
6	-0.342	7	-0.410	8	-0.479	9	0.261	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 9 U 9

PP NO	ORDINATE								
1	0.000	2	0.000	3	0.000	4	0.000	5	0.000
6	0.000	7	0.000	8	0.000	9	1.000	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 9 U 9

PP NO	ORDINATE								
1	0.000	2	0.000	3	0.000	4	0.000	5	0.000
6	0.000	7	0.000	8	0.000	9	0.000	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 1 U 2

PP NO	ORDINATE								
1	0.000	2	-1.187	3	-1.039	4	-0.891	5	-0.742
6	-0.594	7	-0.445	8	-0.297	9	-0.148	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 2 L 3

PP NO	ORDINATE								
1	0.000	2	-0.348	3	0.640	4	0.548	5	0.457
6	0.365	7	0.274	8	0.183	9	0.091	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 3 L 4

PP NO	ORDINATE								
1	0.000	2	-0.221	3	-0.443	4	0.565	5	0.471
6	0.377	7	0.283	8	0.188	9	0.094	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 4 L 5

PP NO	ORDINATE								
1	0.000	2	-0.154	3	-0.308	4	-0.462	5	0.572
6	0.457	7	0.343	8	0.229	9	0.114	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 5 U 6

PP NO	ORDINATE								
1	0.000	2	0.000	3	0.000	4	0.000	5	0.000
6	0.000	7	0.000	8	0.000	9	0.000	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 5 L 6

PP NO	ORDINATE								
1	0.000	2	-0.131	3	-0.261	4	-0.392	5	-0.523
6	0.523	7	0.392	8	0.261	9	0.131	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 6 U 7

PP NO	ORDINATE								
1	0.000	2	0.114	3	0.229	4	0.343	5	0.457
6	0.572	7	-0.462	8	-0.308	9	-0.154	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 7 U 8

PP NO	ORDINATE								
1	0.000	2	0.094	3	0.188	4	0.283	5	0.377
6	0.471	7	0.565	8	-0.443	9	-0.221	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER L 8 U 9

PP NO	ORDINATE								
1	0.000	2	0.091	3	0.183	4	0.274	5	0.365
6	0.457	7	0.548	8	0.640	9	-0.348	10	0.000

TABLE 4.1 MEMBER INFLUENCE LINE VALUES

INFLUENCE LINE ORDINATES FOR TRUSS MEMBER U 9 L10

PP NO	ORDINATE								
1	0.000	2	-0.148	3	-0.297	4	-0.445	5	-0.594
6	-0.742	7	-0.891	8	-1.039	9	-1.187	10	0.000

CONFIDENTIAL MEMBERS

Lvads

BRIDGE NO. 9090 - COINCIDENT MEMBER LOADS AT TRUSS JOINTS - HS20 LOADING

COMPLETED BY: JWS

CHECKED BY: JDL

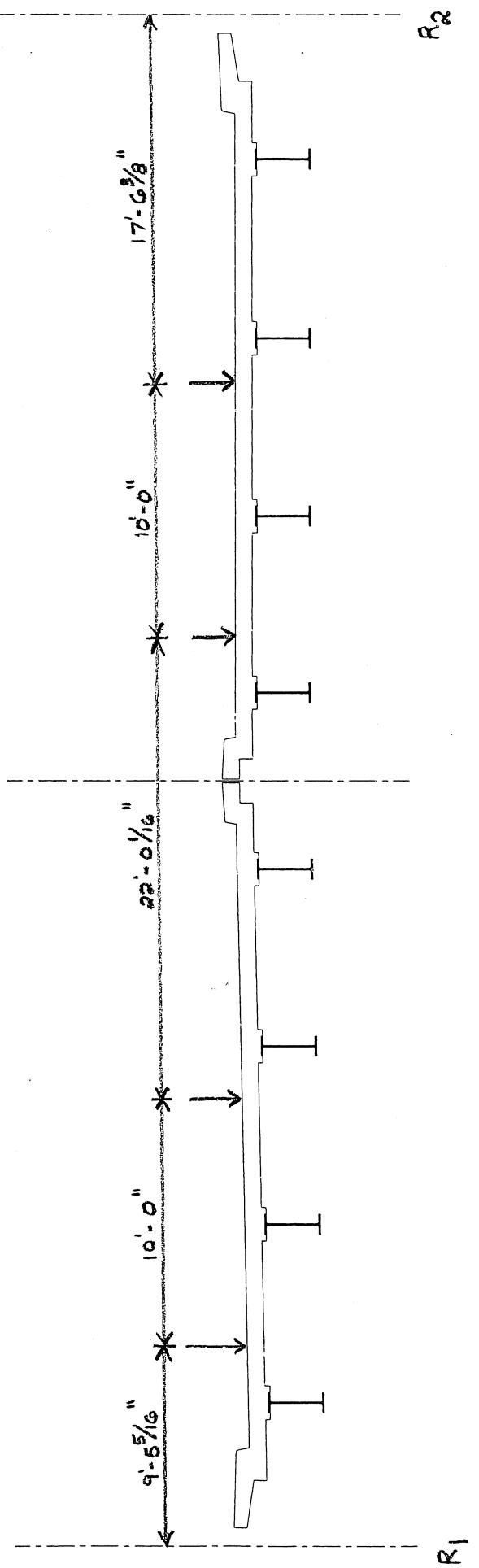
DATE: 02-12-08

DATE: 02-12-08

JOINT NUMBER	NUMBER OF MEMBERS AT JOINT	COINCIDENT MEMBER LOADS - SERVICE LOAD WITH IMPACT INCLUDED (BOLD NUMBERS ARE MAXIMUM LOAD AT JOINT)																																			
		NOTE THAT NODE AND MEMBER LABELS DO NOT MATCH ORIGINAL PLAN - SOFTWARE USED REQUIRES FIRST NODE TO BE L1 INSTEAD OF L0. SEE ANALYSIS DATA FOR DRAWING SHOWING MEMBER/JOINT LABELS USED BELOW.																																			
		MEMBER LOADS - BOTTOM CHORD (KIPS)					MEMBER LOADS - TOP CHORD (KIPS)					MEMBER LOADS - VERTICAL MEMBERS (KIPS)					MEMBER LOADS - DIAGONAL MEMBERS (KIPS)																				
L1	2	L1-L2	L2-L3	L3-L4	L4-L5	L5-L6	L6-L7	L7-L8	L8-L9	L9-L10	U2-U3	U3-U4	U4-U5	U5-U6	U6-U7	U7-U8	U8-U9	L2-U2	L3-U3	L4-U4	L5-U5	L6-U6	L7-U7	L8-U8	L9-U9	L1-U2	L3-U2	L4-U3	L5-U4	L5-U6	L6-U5	L6-U7	L7-U8	L8-U9	L10-U9		
L1	2	159.1																						-239.9													
		159.1																						-257.8													
L2	3	159.1	159.1															71.3																			
		159.1	159.1															71.3																			
		90.1	90.1															114.6																			
L3	4	159.1	206.0															-15.6									70.8										
		155.7	224.9															-6.8									104.3										
		138.9	221.0															-10.0									124.3										
		86.3	60.9															-28.6									38.2										
		108.4	142.6															66.5									51.6										
L4	4		98.9	159.9														65.0									91.8										
			224.9	244.8														9.6									34.1										
			219.5	259.2														15.7									68.3										
			146.9	169.2														71.1									38.3										
			119.9	161.2														53.9									71.0										
L5	5		177.3	234.9														2.9									99.5										
			142.5	109.5														46.1									56.7										
			259.2	266.8														25.7									13.9	0 (A)									
			252.0	278.4														30.1									49.0	0 (A)									
			162.8	182.9														68.8									37.4	0 (A)									
L6	5		113.5	146.3														51.2									60.7	0 (A)									
			180.0	229.1														8.5									90.8	0 (A)									
			169.3	136.4														51.3									61.0	0 (A)									
			278.4	244.8														14.5									-17.7	45.1									
			259.8	259.2														14.4									13.3	13.9									
L7	4		264.6	264.1														15.0									13.5	14.2									
			167.4	198.0														11.1									73.6	15.2									
			206.2	129.9														9.0									73.6	69.4									
			231.3	180.0														12.3									-4.5	90.8									
			109.1	169.3														7.4									51.7	61.0									
L8	4		259.2	219.5														15.7									68.3										
			244.8	224.9														9.6									34.1										

(A) - LOADS ARE ZERO SINCE "COUNTER" WAS MODELED AS INACTIVE TO APPROXIMATE ORIGINAL DESIGN INTENT. FOR GUSSET PLATE ANALYSIS LOAD RANGES AS LISTED FOR MEMBER L6-U5 SHOULD BE CONSIDERED.

Calculations



$$R_1 = \frac{17' - 6\frac{3}{8}'' + 27' - 6\frac{3}{8}'' + 49' - 6\frac{7}{16}'' + 59' - 6\frac{7}{16}''}{69' - 0''} = 2.234$$

$$D.F. = 2.234 \times .75 = 1.676$$

TO DATE TRUSS DEAD LOAD SUMMARY																
Loads	Stringers	Floorbeam	Diaphragms	Deck	Railing	Vertical Gusset Plates	Bottom Chord Horizontal Gusset Plates	Top Chord Horizontal Gusset Plates	Bottom Lateral Bracing	Top lateral Bracing	Vertical Bracing (sway)	Portal	Total Load Entire Bridge	Dead Load Detail Factor	Total Load with DL Factor	TOTAL PER TRUSS (KIPS)
Point Load Loc.																
L1	12276	23299.6	911.6	128623.7	7750	2845	350		2306.2				178362.1	0.05	179103.2	89.6
L2	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L3	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L4	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L5	24552	21325.5	1823.2	257247.3	15500	2845	220		5320.9				328833.9	0.05	329679.7	164.8
L6	24552	21325.5	1823.2	257247.3	15500	2845	220		5320.9				328833.9	0.05	329679.7	164.8
L7	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L8	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L9	24552	21325.5	1823.2	257247.3	15500	2845	220		4612.4				328125.4	0.05	328935.8	164.5
L10	12276	21110.8	911.6	128623.7	7750	2845	350		2306.2				176173.3	0.05	176870.6	88.4
U2						2845	1110			3862.7	17356.0	10857.3	36031.0	0.05	37832.6	18.9
U3						2845	1110			7660.7	18411.7		30027.4	0.05	31528.8	15.8
U4						2845	1110			7563.1	19211.0		30729.1	0.05	32265.6	16.1
U5						2845	1110			8681.4	19005.3		31641.7	0.05	33223.8	16.6
U6						2845	1110			8681.4	19005.3		31641.7	0.05	33223.8	16.6
U7						2845	1110			7563.1	19211.0		30729.1	0.05	32265.6	16.1
U8						2845	1110			7660.7	18411.7		30027.4	0.05	31528.8	15.8
U9						2845	1110			3862.7	17356.0	10857.3	36031.0	0.05	37832.6	18.9

FLOORBEAMS HAVE DEAD LOAD DETAIL FACTOR (2%)

GUSSET PLATES AND BRACING HAVE THE DEAD LOAD DETAIL FACTOR (5%)



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/29/08 BY RAM SHEET NO. 2 OF 2
CJM 2/3/08

REVISIONS TO POINT LOADS AT L1 AND L2

PER PLAN MEMBER L^{1/2} - W^{1/2}

$$\Delta L = (64.68 \text{ in}^2) (17\text{-}6") (490 \text{ PCF}) = 3852 \text{ LB} + 5\% \text{ DETAIL FACTOR}$$
$$= 4045 \text{ LB}$$

PER PLAN L¹ - W^{1/2}

$$\Delta L = (39.25 \text{ in}^2) (23\text{-}5") (490 \text{ PCF}) = 3128 \text{ LB} + 5\% \text{ DETAIL FACTOR}$$
$$= 3285 \text{ LB}$$

TOTAL = 7330 LB

= 3665 LB TO L1 AND
3665 LB TO L2

FROM SHEET 1

$$L_1 = 89.6 \text{ K} + 3.665 \text{ K} = 93.3 \text{ K}$$

$$L_2 = 164.5 \text{ K} + 3.665 \text{ K} = 168.2 \text{ K}$$

NOTE: DEAD LOAD COMPUTATIONS WERE INDEPENDENTLY VERIFIED
BY MEANS OF COMPARISON OF DEAD LOAD MEMBER
LOADS TO THOSE SHOWN IN ORIGINAL DESIGN
DRAWINGS. JWS 2-14-08



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 1 OF 6
CJM 2/13/08

FLOOR SYSTEM DEAD LOADS (AT FLOORBEAM L1)

STRINGERS

$$= (99 \text{ LB/FT}) (8) (31'-0")^{1/2} = 12,276 \text{ LB}$$

NOTE NUMBERS MATCH
ORIGINAL PLAN USED
RAM DEAD LOADS IN
TRUSS ANALYSIS.

FLOORBEAM

$$\text{WEB} = (66") (7\frac{1}{16}") (67'-4\frac{5}{8}") (490 \text{ PCF}) = 6621 \text{ LB}$$

$$\text{FLANGES} = 2 (1'-10") (1") (17'-3\frac{3}{8}") (490 \text{ PCF}) = 2587.4 \text{ LB}$$

$$\text{FLANGES} = 2 (1'-10") (1\frac{3}{4}") (50-0") (490 \text{ PCF}) = 13,100.7 \text{ LB}$$

$$\text{STIFFENERS} = (66") (5") (\frac{3}{8}") (490 \text{ PCF}) (17) = 596.5 \text{ LB}$$

$$\text{END STIFFENER} = 2 (66" \times 1'-0") (\frac{5}{8}") (490 \text{ PCF}) = 280.7 \text{ LB}$$

$$\text{CONNECTION ANGLE} = (8.5 \text{ LB/FT}) (1'-8") (8) = 113.3 \text{ LB}$$

DIAPHRAGMS

$$= (33.9 \text{ LB/FT}) (5\frac{1}{2}") (6)^{1/2} = 813.6 \text{ LB}$$

$$\text{STIFFENERS} = (9.8 \text{ LB/FT}) (1'-8") (12)^{1/2} = 98 \text{ LB}$$

DECK (FROM AUTOCAD DRAWING)

$$= 2 (27.661 \text{ FT}^2) (31'-0") (150 \text{ PCF})^{1/2} = 128,623.7 \text{ LB}$$

RAILING (ASSUMED)

$$= (1'-6") (1'-0") (150 \text{ PCF}) + 25 \text{ PLF} = (250 \text{ LB/FT}) (31'-0") 2 (1/2) = 7,750 \text{ LB}$$



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/10/08 BY RAM SHEET NO. 2 OF 6

CJM 2/13/08

FLOOR SYSTEM DEAD LOADS (FOR TYPICAL BAY)

STRINGERS

$$= (99 \text{ LB/FT})(8 \text{ STRINGERS})(31'-0") = 24,552 \text{ LB}$$

FLOOR BEAM

$$\text{WEB} = (6\frac{1}{2}")(7\frac{1}{2}")(67' - 4\frac{5}{8}")(490 \text{ PCF}) = 6621 \text{ LB}$$

$$\text{FLANGES} = 2(1'-9") (1") (21' - 3\frac{3}{8}") (490 \text{ PCF}) = 3041.4 \text{ LB}$$

$$\text{STIFFENERS} = (66") (5") (\frac{3}{8}") (490 \text{ PCF}) (34) = 193.1 \text{ LB}$$

$$\text{FLANGES} = 2(1'-9") (1\frac{1}{2}") (46'-0") (490 \text{ PCF}) = 9861.3 \text{ LB}$$

$$\text{CONNECTION ANGLES} = (12.3 \text{ LB/FT}) (1'-8") (8)(2) = 328 \text{ LB}$$

$$\text{END STIFFENERS} = 2(66") (1'-0") (\frac{5}{8}") (490 \text{ PCF}) = 280.7 \text{ LB}$$

DIAPHRAGMS

$$= (33.9 \text{ LB/FT})(8'-0") (6) = 1627.2 \text{ LB}$$

$$\text{STIFFENERS} = (9.9 \text{ LB/FT}) (1'-8") (12) = 196 \text{ LB}$$

DECK (FROM AUTOCAD DRAWING)

$$= 2(27.662 \text{ FT}^2)(31'-0") (150 \text{ PCF}) = 257,247.3 \text{ LB}$$

RAILING (ASSUMED)

$$= (1'-6") (1'-0") (150 \text{ PCF}) + 25 \text{ PLF} = (250 \text{ LB/FT}) (31'-0") 2 = 15,500 \text{ LB}$$



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 3 OF 6

CJm 2/13/08

FLOOR SYSTEM DEAD LOADS (AT FLOORBEAM L11)

STRINGERS

$$= (99 \text{ LB/FT})(8)(31'-0")^{1/2} = 12,276 \text{ LB}$$

FLOORBEAM

$$\text{WEB} = (66") (7\frac{1}{16}") (67'-4\frac{5}{8}") (490 \text{ PCF}) = 6621 \text{ LB}$$

$$\text{FLANGES} = 2(1\cdot 9") (1") (21 - 3\frac{3}{8}") (490 \text{ PCF}) = 3041.4 \text{ LB}$$

$$\text{FLANGES} = 2(1\cdot 9") (1\frac{1}{2}") (46'-0") (490 \text{ PCF}) = 9361.3 \text{ LB}$$

$$\text{STIFFENERS} = (66") (5") (3\frac{1}{2}) (490 \text{ PCF}) (34) = 1193.1 \text{ LB}$$

$$\text{END STIFFENER} = 2(66") (1\cdot 0") (5\frac{1}{3}") (490 \text{ PCF}) = 280.7 \text{ LB}$$

$$\text{CONNECTION ANGLE} = (8.5 \text{ LB/FT}) (1\cdot 8") (8) = 113.3 \text{ LB}$$

DIAPHRAGMS

$$= (33.9 \text{ LB/FT}) (8\cdot 0") (6)^{1/2} = 813.6 \text{ LB}$$

$$\text{STIFFENERS} = (9.8 \text{ LB/FT}) (1\cdot 8") (12)^{1/2} = 98 \text{ LB}$$

DECK (FROM AUTOCAD DRAWING)

$$= 2(27.661 \text{ FT}^2) (31'-0") (150 \text{ PCF})^{1/2} = 128,623.7 \text{ LB}$$

RAILING

$$= (1\cdot 6") (1\cdot 0") (150 \text{ PCF}) + 25 \text{ PLF} = (250 \text{ LB/FT}) (31'-0") (2)^{1/2} = 7,750 \text{ LB}$$



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 4 OF 6

CJM 2/13/08

TRUSS DEAD LOADS

BOTTOM LATERALS (TYPICAL PANEL)

$$= (32.5 \text{ LB/FT})(35.48')(4) = 4612.4 \text{ LB}$$

BOTTOM LATERALS (CENTER PANEL)

$$= (32.5 \text{ LB/FT})(46.38')(4) = 6029.4 \text{ LB}$$

TOP LATERALS

$$\text{PANEL 2} = (53 \text{ LB/FT})(36.44')(4) = 7725.3 \text{ LB} \quad (\text{PANEL 8})$$

$$\text{PANEL 3} = (53 \text{ LB/FT})(35.83')(4) = 7596 \text{ LB} \quad (\text{PANEL 7})$$

$$\text{PANEL 4} = (53 \text{ LB/FT})(35.52')(4) = 7530.2 \text{ LB} \quad (\text{PANEL 6})$$

$$\text{PANEL 5} = (53 \text{ LB/FT})(46.38')(4) = 9832.6 \text{ LB}$$

VERTICAL BRACING (AT U6 AND U7)

$$\text{DIAGONALS} = (53 \text{ LB/FT})(29.88')(4) = 6334.6 \text{ LB}$$

TOP HORIZONTAL

$$= 2(42.7 \text{ LB/FT})(69'-0") = 5892.6 \text{ LB}$$

$$\text{BOT. PLATE} = (1'-0") \times (3/8") (69'-0") (490 \text{ PCF}) = 1056.6 \text{ LB}$$

$$(\text{ASSUMED}) \quad \text{TOP PLATE} = (1'-0") (3/8") (69'-0" - 6'-11" \times 2) (490 \text{ PCF}) = 844.7 \text{ LB}$$



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 5 OF 6
CJM 2/13/08

BOTTOM HORIZONTAL

$$= 2(20.7 \text{ LB/FT})(69'-0") = 2856.6 \text{ LB}$$

$$\text{BOT. PLATE} = (1'-2")(\frac{3}{8}")(69'-0") (490 \text{ PCF}) = 1232.7 \text{ LB}$$

$$\text{TOP PLATE} = (1'-2")(\frac{3}{8}")(44\frac{1}{2}") (490 \text{ PCF}) = 787.5 \text{ LB}$$

VERTICAL BRACING (AT U5 AND U8)

$$\text{DIAGONALS} = (53 \text{ LB/FT})(28.19')(4) = 5976.3 \text{ LB}$$

$$\text{BOTTOM HORIZONTAL} = 4876.8 \text{ LB}$$

TOP HORIZONTAL

$$= 2(42.7 \text{ LB/FT})(69'-0") = 5892.6 \text{ LB}$$

$$\text{TOP PLATE} = (1'-6")(\frac{3}{8}")(69'-0") (490 \text{ PCF}) = 1584.8 \text{ LB}$$

$$\text{BOTTOM PLATE} = (10")(\frac{3}{8}")(69'-0") (490 \text{ PCF}) = 880.5 \text{ LB}$$

VERTICAL BRACING (AT U4 AND U9)

$$\text{DIAGONALS} = (53 \text{ LB/FT})(24.42')(4) = 5177 \text{ LB}$$

$$\text{BOTTOM HORIZONTAL} = 4876.8 \text{ LB}$$

$$\text{TOP HORIZONTAL} = 8357.9 \text{ LB}$$



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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 6 OF 6
CJM 2/13/08

VERTICAL BRACING (AT LB AND L10)

$$\text{DIAGONALS} = (53 \text{ LB/FT})(19.44')(4) = 4121.3 \text{ LB}$$

$$\text{BOTTOM HORIZONTAL} = 4876.8 \text{ LB}$$

$$\text{TOP HORIZONTAL} = 8357.9 \text{ LB}$$

PORTAL BRACING

$$= (94 \text{ LB/FT})(69'-0") = 6486 \text{ LB}$$

$$= (45 \text{ LB/FT})(16.19')(6) = 4371.3 \text{ LB}$$



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PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-15-08 BY CJM SHEET NO. 1 OF 11

RAM 2-13-08

Dead load - Floor system @ L1

Stringer - 30 WF 99

$$8 \cdot 99 \text{ lb/ft} \cdot 31' \cdot \frac{1}{2} = 12276 \text{ lb}$$

Node Numbers match
original plan, used
RAM Dead Loads in
Truss Analysis

Floor beam

$$\text{Flange} - 2 \cdot 17' 3\frac{3}{8}'' \cdot 1' 10'' \cdot 1'' \cdot 490 \text{ lb/ft}^3 = 2587.38 \text{ lb}$$

$$\text{Flange} - 2 \cdot 50' - 1' 10'' \cdot 1\frac{3}{4}'' \cdot 490 \text{ lb/ft}^3 = 13100.69 \text{ lb}$$

$$\text{Web} - 66'' \cdot 67' 4\frac{5}{8}'' \cdot 7\frac{1}{16}'' \cdot 490 \text{ lb/ft}^3 = 6620.96 \text{ lb}$$

$$\text{Stiffeners} - 17 \cdot 66'' \cdot 5'' \cdot 3\frac{3}{8}'' \cdot 490 \text{ lb/ft}^3 = 5961.55 \text{ lb}$$

$$\text{End stiffener} - 2 \cdot 1' \cdot 5\frac{7}{8}'' \cdot 66'' \cdot 490 \text{ lb/ft}^3 = 280.73 \text{ lb}$$

$$\text{Connection plate } \approx 20'' \cdot 8.5 \text{ lb/ft} \cdot 8 = 113.33 \text{ lb}$$

$\hookrightarrow 3\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{8}$

Diaphragms - 15 U 33.9

$$6 \cdot 8' \cdot 33.9 \text{ lb/ft} = 1627.2 \text{ lb} \cdot \frac{1}{2} = 813.6 \text{ lb}$$

$$\text{Stiffeners} - 12 \cdot 9.8 \text{ lb/ft} \cdot 1' 8'' = 196 \text{ lb} \cdot \frac{1}{2} = 98 \text{ lb}$$

$$\hookrightarrow 1 \frac{1}{4} \times 4 \times 3\frac{1}{8}$$

Bridge Deck

$$2 \cdot 27.66 \text{ ft}^2 \cdot 150 \text{ lb/ft}^3 \cdot 31' \cdot \frac{1}{2} = 128,619 \text{ lb}$$

Railing (assumed)

$$1' 6'' \cdot 1' 0'' \cdot 150 \text{ pcf} + 25 \text{ plf} = 250 \text{ lb/ft} \cdot 31' \cdot 2 \cdot \frac{1}{2} \\ = 7,750 \text{ lb}$$



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PROJECT Bridge # 9090

PROJECT # 07074 S.30 DATE 1-15-07 BY CJM SHEET NO. 2 OF 11
RAM 2-13-08

Dead Load - Typical Floor beam

Stringer - 30 WF 99

$$8 \cdot 99 \text{ lb/ft} \cdot 31 \text{ ft} = 24552 \text{ lb}$$

Floor beam

$$\text{Flange} - 2 \cdot 21 \frac{3}{8}'' \cdot 119'' \cdot 1'' \cdot 490 \text{ lb/ft}^3 = 3041.45 \text{ lb}$$

$$\text{Flange} - 2 \cdot 46'' \cdot 119'' \cdot 1\frac{1}{2}'' \cdot 490 \text{ lb/ft}^3 = 9,861.25 \text{ lb}$$

$$\text{Web} - 66'' \cdot 67\frac{1}{4} \frac{5}{8}'' \cdot 7\frac{1}{16}'' \cdot 490 \text{ lb/ft}^3 = 6620.96 \text{ lb}$$

$$\text{Stiffeners} - 34 \cdot 5'' \cdot \frac{3}{8}'' \cdot 66'' \cdot 490 \text{ lb/ft}^3 = 1193.10 \text{ lb}$$

$$\text{End stiffeners} - 2 \cdot 5\frac{1}{8}'' \cdot 66'' \cdot 1'' \cdot 490 \text{ lb/ft}^3 = 280.73 \text{ lb}$$

$$\text{Connection plate} - 12.3 \text{ lb/ft} \cdot 20'' \cdot 8 = 164 \text{ lb} \cdot 2 \text{ sides} = 328 \text{ lb}$$

$$\hookrightarrow L 5 \times 5 \times \frac{3}{8}$$

Diaphragm - 15 U 33, 9

$$6 \cdot 8' \cdot 33.9 \text{ lb/ft} = 1627.2 \text{ lb}$$

$$\text{Stiffeners} - 12 \cdot 9.3 \text{ lb/ft} \cdot 1\frac{1}{8}'' = 196 \text{ lb}$$

$$\hookrightarrow L 4 \times 4 \times \frac{3}{8}$$

Bridge Deck

$$2 \cdot 27.66 \text{ ft}^2 \cdot 31'' \cdot 150 \text{ lb/ft}^3 = 257,238 \text{ lb}$$

Railing (assumed)

$$250 \text{ lb/ft} \cdot 31' \cdot 2 = 15,500 \text{ lb}$$



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PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-15-08 BY C Jm SHEET NO. 3 OF 11

RAM 2-B-08

Dead Load - Floor System @ L-11

Stringers - 30 WF 99

$$8 \cdot 99 \text{ lb/ft} \cdot 31' \cdot 1/2 = 12,276 \text{ lb}$$

Floor beam

$$\text{Flange} - 2 \cdot 21' 3\frac{1}{8}'' \cdot 1' 9'' \cdot 1'' \cdot 490 \text{ lb/ft}^3 = 3041.45 \text{ lb}$$

$$\text{Flange} - 2 \cdot 46 \cdot 1' 9'' \cdot 1\frac{1}{2}'' \cdot 490 \text{ lb/ft}^3 = 9861.25 \text{ lb}$$

$$\text{Web} - 66'' \cdot 67' 4\frac{5}{8}'' \cdot 7\frac{1}{16}'' \cdot 490 \text{ lb/ft}^3 = 6620.97 \text{ lb}$$

$$\text{Stiffeners} - 34 \cdot 5'' \cdot 3\frac{1}{8}'' \cdot 66'' \cdot 490 \text{ lb/ft}^3 = 1193.10 \text{ lb}$$

$$\text{End stiffeners} - 2 \cdot 66'' \cdot 1' 0\frac{5}{8}'' \cdot 490 \text{ lb/ft}^3 = 280.73 \text{ lb}$$

$$\text{Connection plate} - 8 \cdot 8.5 \text{ lb/ft} \cdot 20'' = 113.33 \text{ lb}$$

$$\hookrightarrow L 3\frac{1}{2} \times 3\frac{1}{2} \times 3\frac{1}{8}$$

Diaphragm - 15 U 33.9

$$6 \cdot 33.9 \text{ lb/ft} \cdot 8' = 1627.2 \text{ lb} \cdot 1/2 = 813.6 \text{ lb}$$

$$\text{Stiffeners} - 9.8 \text{ lb/ft} \cdot 20'' \cdot 12 = 196 \cdot 1/2 = 98 \text{ lb}$$

$$\hookrightarrow L 4 \times 4 \times 3\frac{1}{8}$$

Bridge deck

$$2 \text{ sides} \cdot 27.66 \text{ ft}^2/\text{side} \cdot 150 \text{ lb/ft}^3 \cdot 31' \cdot 1/2 = 128,619 \text{ lb}$$

Railing (assumed)

$$250 \text{ lb/ft} \cdot 31' \cdot 2 \cdot 1/2 = 7,750 \text{ lb}$$



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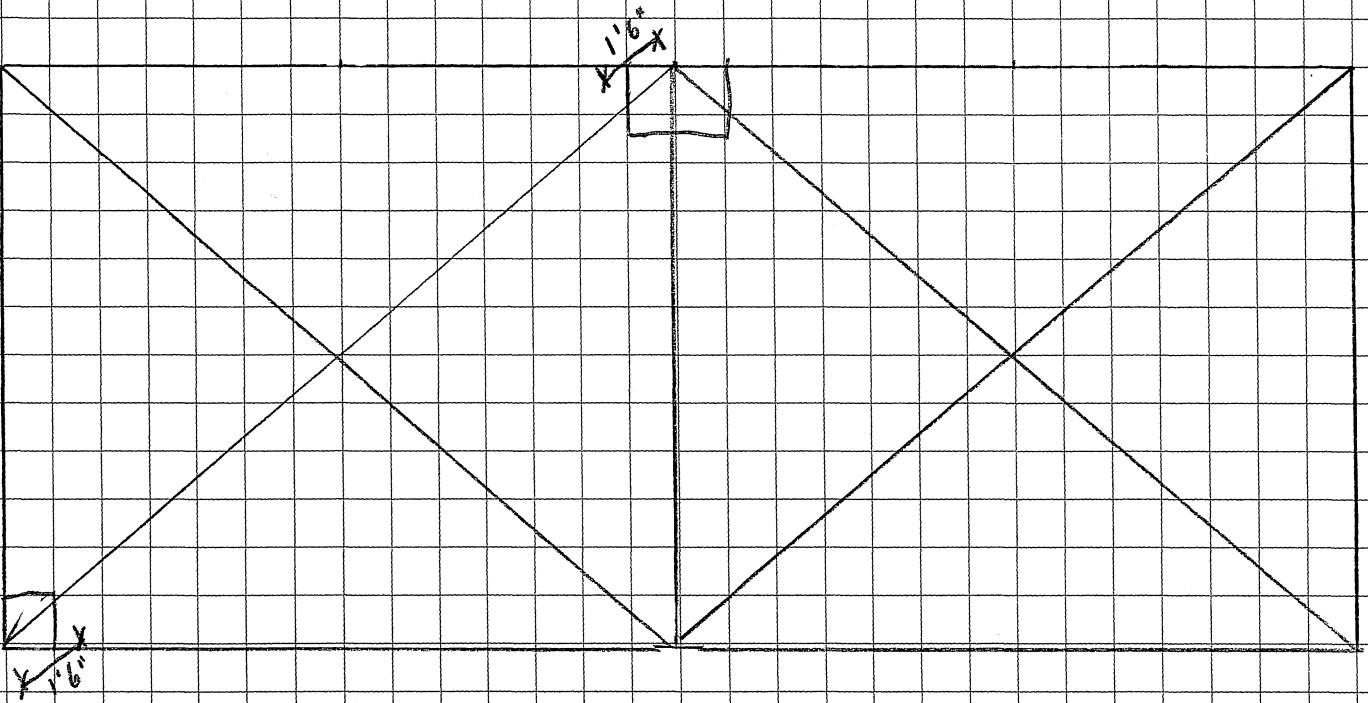
PROJECT Bridge # 90 90

PROJECT # 070745.30 DATE 1-15-08 BY C JM SHEET NO. 4 OF 11

RAM 2-13-08

Bottom Lateral

Center Bay - Node to Node - 46,38 ft - $Z(1'6") = \underline{43.38}$





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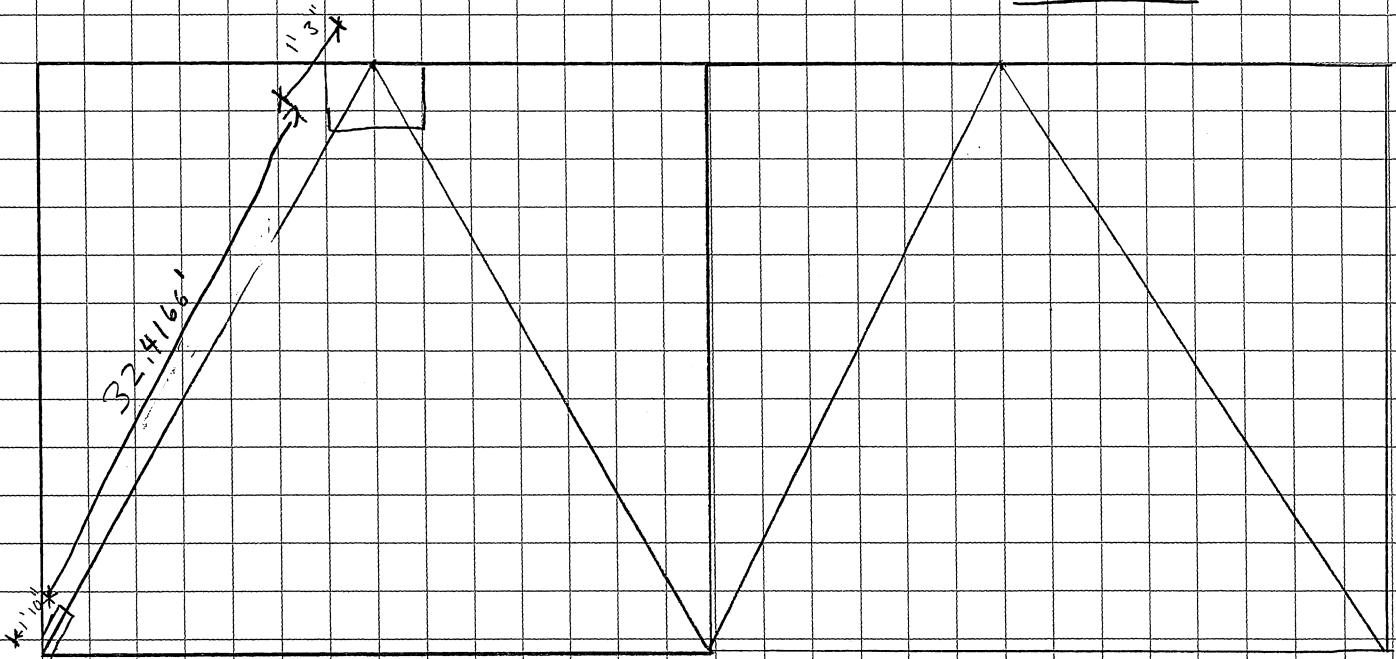
PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-15-08 BY CJM SHEET NO. 5 OF 11

RAM 2-13-08

Bottom Lateral

Typical Bay - Node to Node - 35.48 ft - $1,25^1 - 1\frac{6}{12}^1$
 $= 32,4 \text{ ft}$





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PROJECT Bridge # 9090

PROJECT # 070745.30 DATE 1-15-08 BY CJM SHEET NO. 6 OF 11

RAM 2-13-08

Truss dead load

Bottom Lateral (Typical panel)

$$32.5 \text{ lb/ft} \cdot 32.4 \text{ ft} \cdot 4 = 4212 \text{ lb}$$

Bottom Lateral (center panel)

$$32.5 \text{ lb/ft} \cdot 43.38 \text{ ft} \cdot 4 = 5622.05 \text{ lb}$$

Top Lateral - 12 BP 53

node to node length - 36.44' - Panel 2

length short - 2 @ 7'8"

2 @ 4'2"

$$\text{Panel 2 } (36.44 \cdot 4 - 2 \cdot 7'8" - 2 \cdot 4'2") \cdot 53 \text{ lb/ft} \\ = 6470.95 \text{ lb}$$

Panel 3 node to node - 35.83'

$$= (35.83 \cdot 4 - 2 \cdot 7'8" - 2 \cdot 4'2") \cdot 53 \text{ lb/ft} \\ = 6341.63 \text{ lb}$$

Panel 4 node to node - 35.52'

$$= (35.52 - 2 \cdot 7'8" - 2 \cdot 4'2") \cdot 53 \text{ lb/ft} \\ = 6275.91 \text{ lb}$$

Panel 5 node to node - 46.38'

$$= (46.38 \cdot 4 - 4 \cdot 2'10") \cdot 53 \text{ lb/ft} = 9231.89 \text{ lb}$$

Panel 6 = Panel 4 = 6275.91 lb

Panel 7 = Panel 3 = 6341.63 lb

Panel 8 = Panel 2 = 6470.95 lb



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Fax 612 338-2088

PROJECT Bridge # 9090

PROJECT # 070 745.30 DATE 1-15-08 BY C JM SHEET NO. 7 OF 11

RAM 2-13-08

Vertical Bracing (U6 + U7)

$$\text{Diagonals - Node to Node length} = 29.88' - 12 \text{ BP } 53 \\ = [4(29.88') - 2(2'6") - 2(19")] \cdot 53^{\text{Lb}/\text{ft}} = 5901.73 \text{ Lb}$$

Top Horizontal - 2.18 U 42.7 + 2 plates

$$2(42.7^{\text{Lb}/\text{ft}})(69') = 5892.6 \text{ Lb}$$

$$\text{Bottom plate} - (1')(3/8") (69') (490^{\text{Lb}/\text{ft}^3}) = 1056.56 \text{ Lb}$$

$$\text{Top plate} - (1')(3/8") (69' - 2.1') (490^{\text{Lb}/\text{ft}^3}) = 934.06 \text{ Lb}$$

$$\text{Total} = \underline{7883.22 \text{ Lb}}$$

Bottom Horizontal - 2-12 U 20.7 + 2 plates

$$2(20.7^{\text{Lb}/\text{ft}})(69') = 2856.6 \text{ Lb}$$

$$\text{Bottom plate} - (1'2") (69') (3/8") (490^{\text{Lb}/\text{ft}^3}) = 1232.66 \text{ Lb}$$

$$\text{Top plate} - (1'2") (3/8") (69' - 2.1' - 3') (490^{\text{Lb}/\text{ft}^3}) = 1143.33 \text{ Lb}$$

$$\text{Total} = \underline{5232.59 \text{ Lb}}$$

Vertical Bracing (U5 + U8)

$$\text{Diagonals - Node to Node length} - 28.19' \\ = [4(28.19') - 2(2'6") - 2(19")] \cdot 53^{\text{Lb}/\text{ft}} = 5543.45 \text{ Lb}$$

$$\text{Top Horizontals} = 7883.22 \text{ Lb}$$

$$\text{Bottom Horizontals} = 5232.59 \text{ Lb}$$

Vertical Bracing (U4 + U9)

$$\text{Diagonal - Node to Node length} - 24.43' \\ = [4(24.43) - 2(2'6") - 2(19")] \cdot 53^{\text{Lb}/\text{ft}} = 4746.33 \text{ Lb}$$

$$\text{Top Horizontal} = 7883.22 \text{ Lb}$$

$$\text{Bottom Horizontal} = 5232.59$$



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PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-15-08 BY CJM SHEET NO. 8 OF 11

RAM 2-13-08

Vertical Bracing (U3 + U10)

$$\text{Diagonal - Node to Node Length} = 19.44' \\ = [4(19.44') - 2(2'6") - 2(19'')] \cdot 53^{\text{lb}}/\text{ft} = 3688.45 \text{ lb}$$

$$\text{Top Horizontal} = 7883.22 \text{ lb}$$

$$\text{Bottom Horizontal} = 5232.59 \text{ lb}$$

Portal Bracing

$$\text{Diagonal - 6 - 18 WF 45 - Node to Node length} = 16.19' \\ = [6(16.19') - 2(5'9") - 4(3'2"')] \cdot 45^{\text{lb}}/\text{ft} = 3283.8 \text{ lb}$$

$$\text{Horizontal} - 24 \text{ WF 94}$$

$$69' \cdot 94^{\text{lb}}/\text{ft} = 6486 \text{ lb}$$



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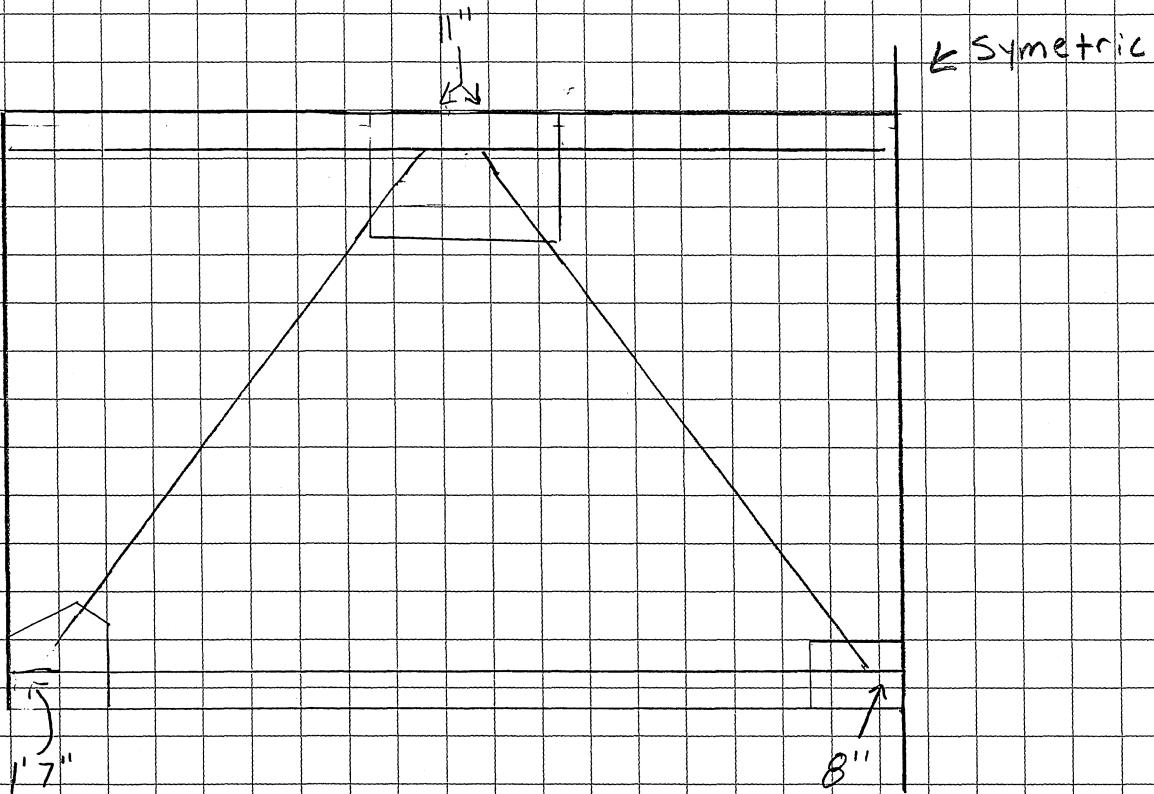
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PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-16-08 BY C J W SHEET NO. 9 OF 11

RAM 2-13-08

Sway Bracing Subtractions - scaled from drawings





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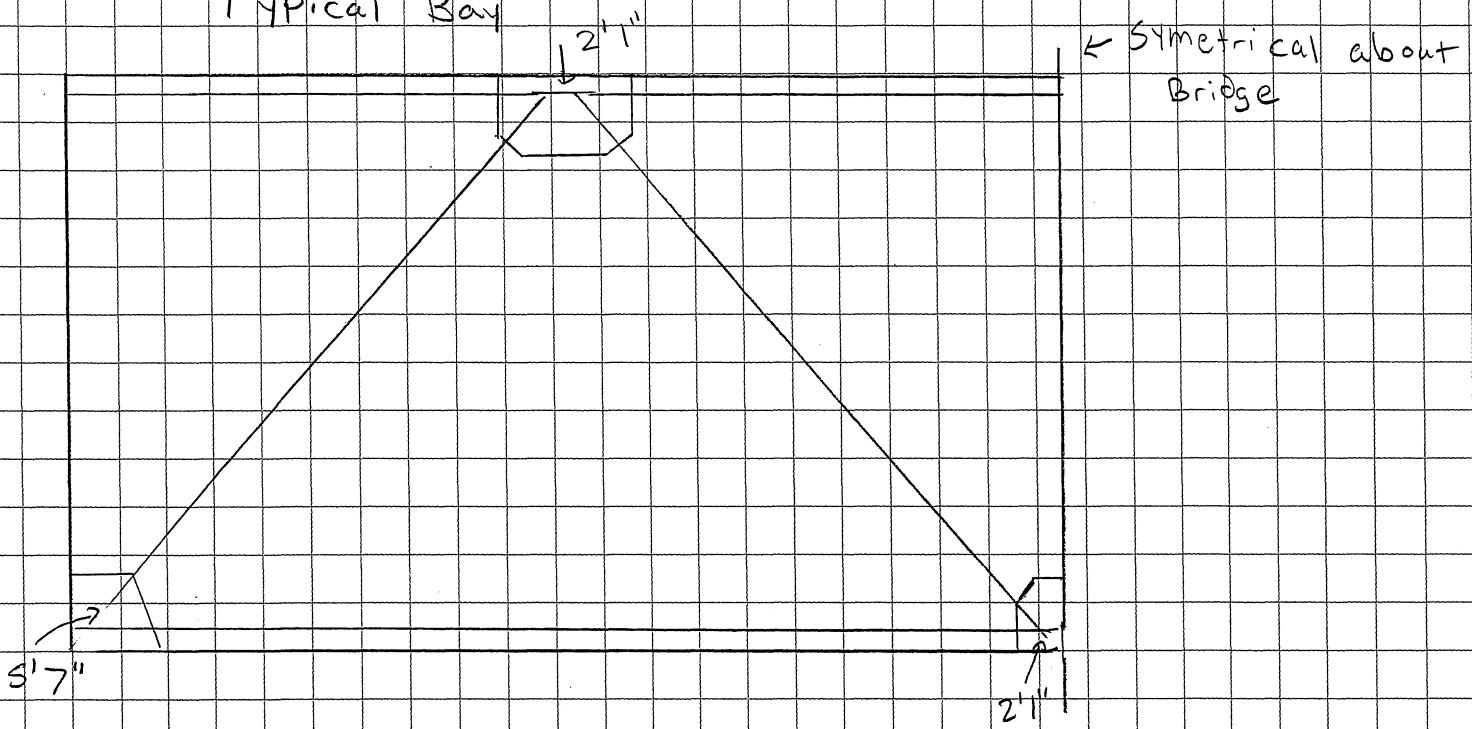
PROJECT Bridge #9090

PROJECT # 070745.30 DATE 1-16-08 BY CJM SHEET NO. 10 OF 11

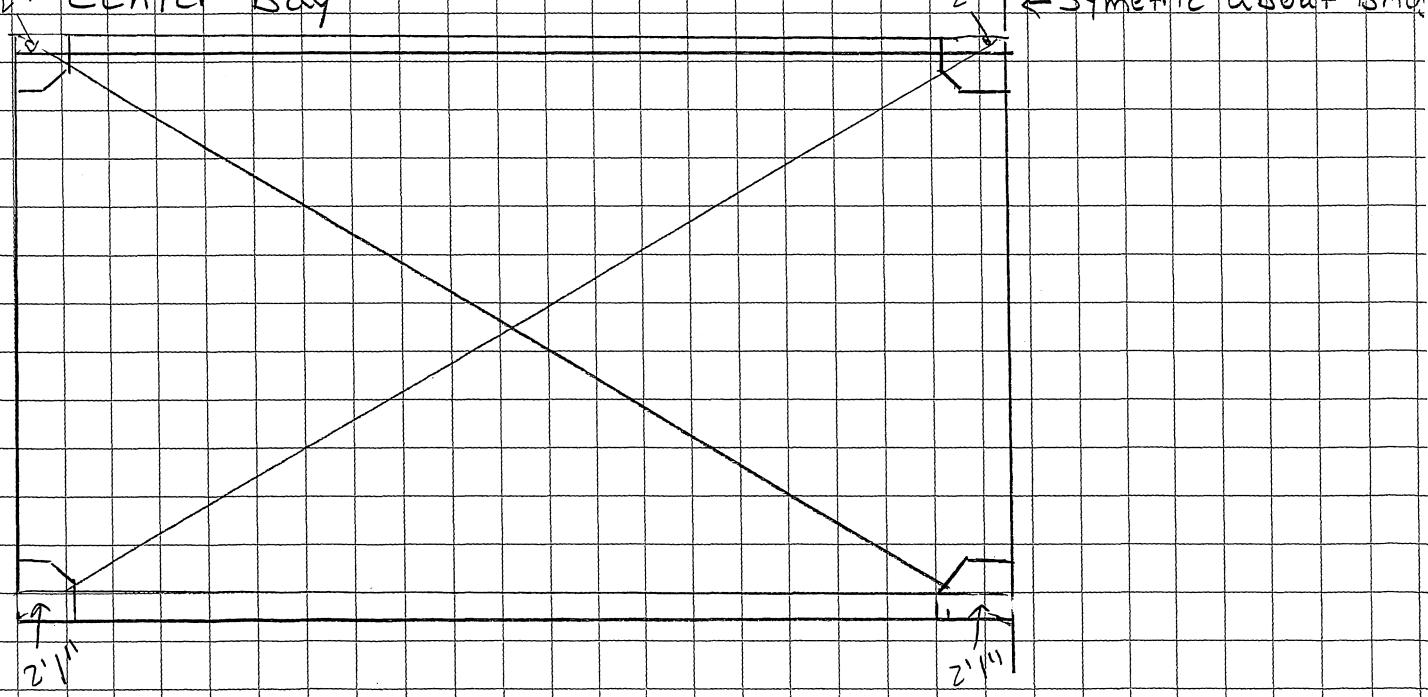
RAM 2-13-08

Top Lateral Subtractions - Scaled from drawings

Typical Bay



2' 1" Center Bay





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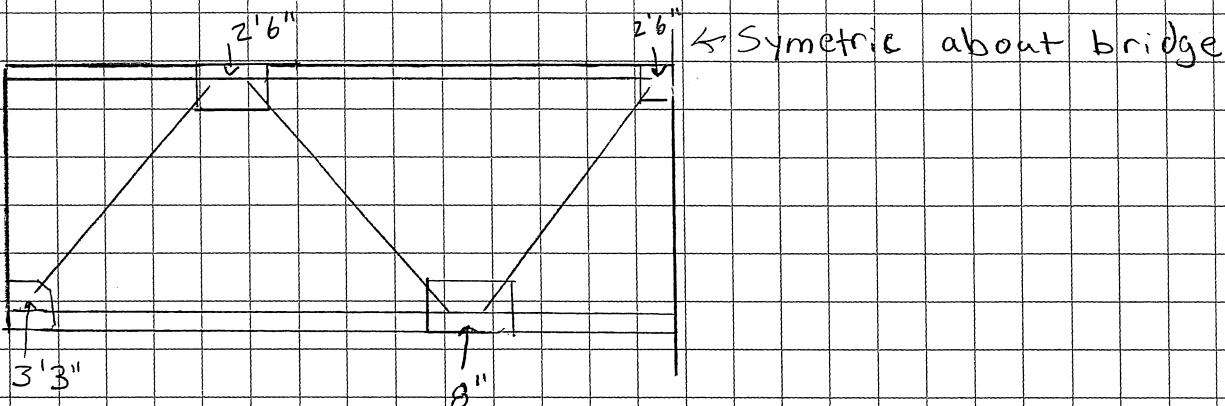
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PROJECT Bridge # 9090

PROJECT # 070745.30 DATE 1-16-08 BY CJM SHEET NO. 11 OF 11

RAM 2-13-08

Portal Subtractions - Scaled from drawings





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PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 2/13/08 BY RAM SHEET NO. 1 OF 1

✓ JWS 2-13-08

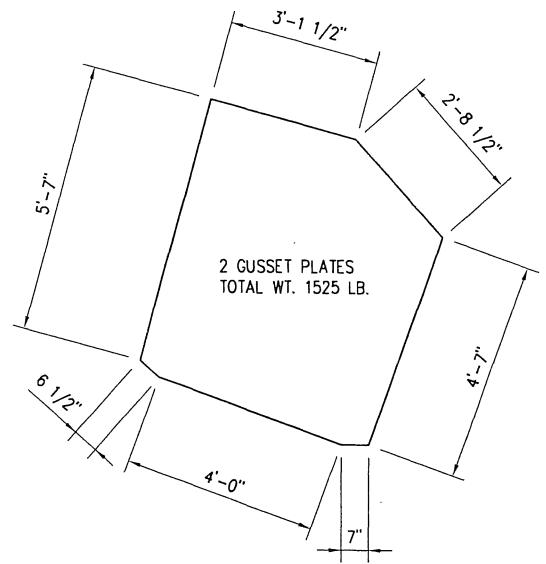
DETERMINE YIELD STRENGTH OF STEEL

BOTTOM CHORD $\Rightarrow .55(\text{AREA})F_y$ = ALLOWABLE STRESS PER EXISTING PLAN

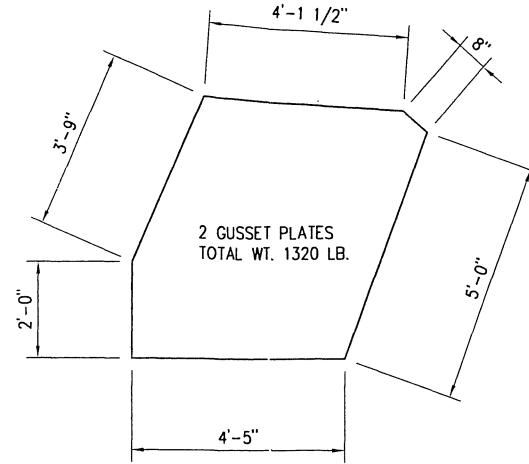
$$\text{TOP CHORD} = F_y \left[1 - \frac{(KL/r)^2}{4T^2 E} F_y \right] = \text{ALLOWABLE STRESS PER EXISTING PLAN}$$

VERTICAL AND DIAGONALS IN TENSION = $.55(A_g)F_y$ = ALLOWABLE STRESS
PER EXISTING PLAN

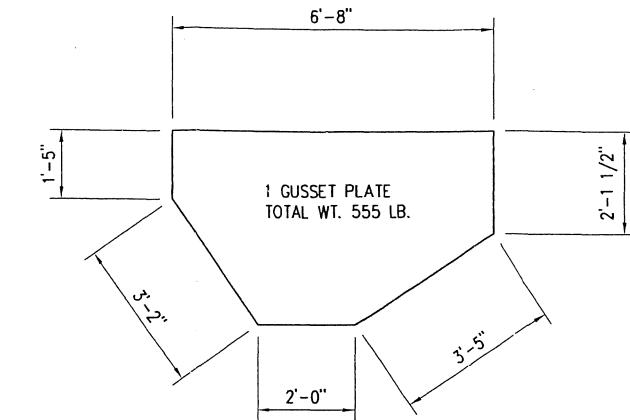
VERTICAL AND DIAGONALS IN COMPRESSION SAME FORMULA AS TOP CHORD



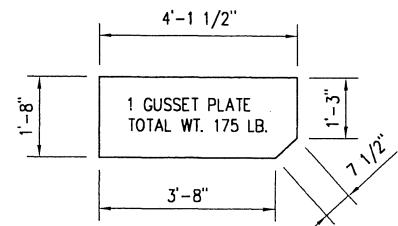
VERTICAL GUSSET PLATE AT U3 & U10



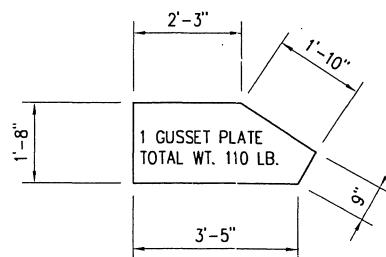
VERTICAL GUSSET PLATE AT L4 & L9



HORIZONTAL GUSSET PLATE AT U3 & U10



HORIZONTAL GUSSET PLATE AT L1 - L11



HORIZONTAL GUSSET PLATE AT L2 - L10

Original Plans

MINNESOTA DEPARTMENT OF TRANSPORTATION

CONSTRUCTION PLAN FOR DECK REPAIR AND OVERLAY, BRIDGE 9090 (MN) BRIDGE 2-358.22 (N.D.)

LOCATED ON T.H. 2 OVER RED RIVER OF THE NORTH BETWEEN EAST GRAND FORKS AND GRAND FORKS

STATE PROJ. NO. 6018-9090

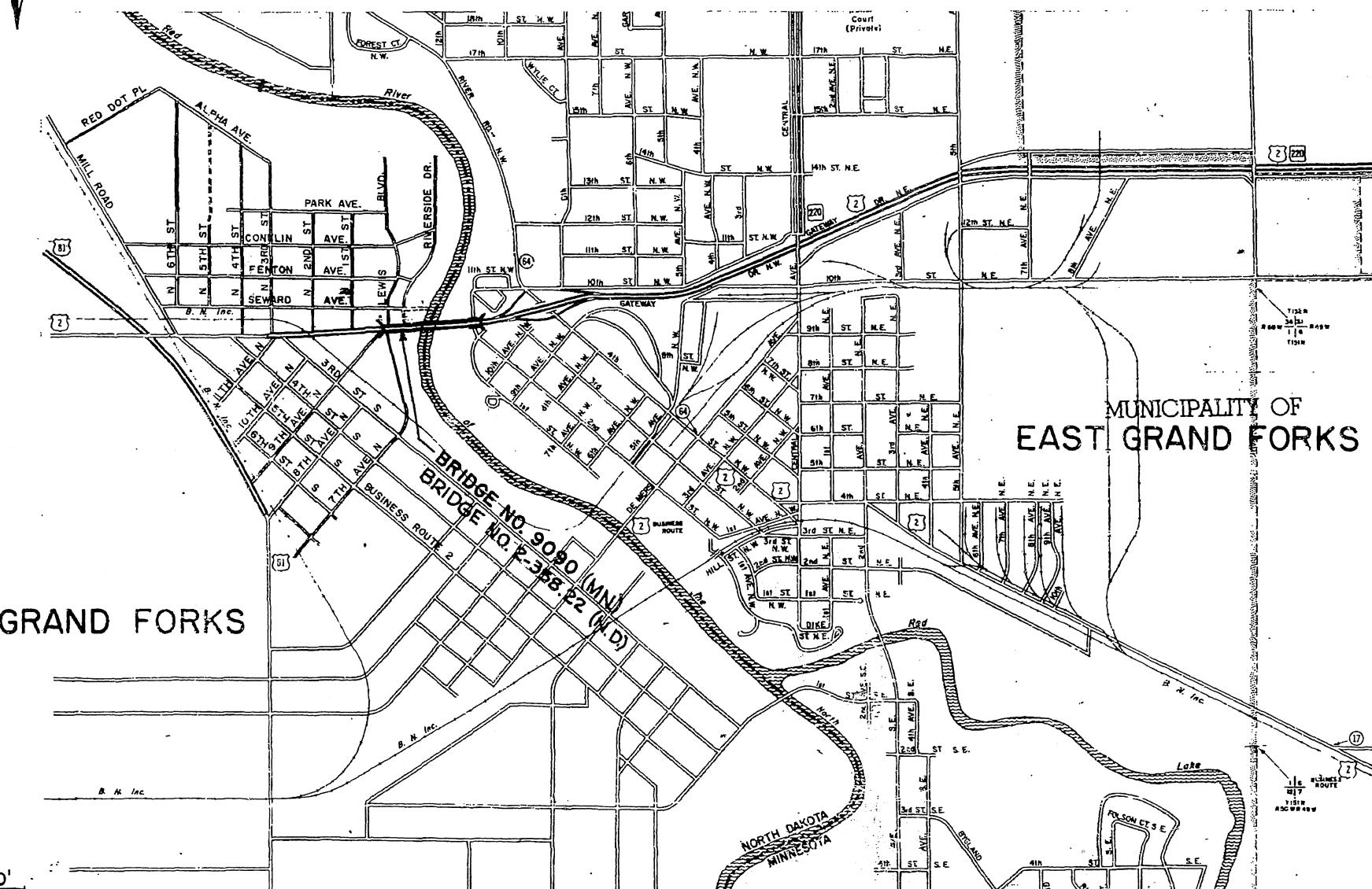
MINN. PROJ. NO.

GROSS LENGTH 1436.0 FEET MILES
BRIDGES-LENGTH 1261.0 FEET MILES
EXCEPTIONS-LENGTH 0 FEET MILES
NET LENGTH FEET MILES
MILE POINT TO MILE POINT

STATE PROJ. NO.

MINN. PROJ. NO.

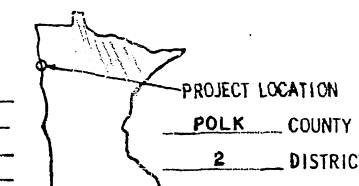
GROSS LENGTH FEET MILES
BRIDGES-LENGTH FEET MILES
EXCEPTIONS-LENGTH FEET MILES
NET LENGTH FEET MILES
MILE POINT TO MILE POINT



SCALES
PLAN 100'
PROFILE 10'v.100'
INDEX MAP 800'
GENERAL LAYOUT ±50'

PLAN REVISIONS		
DATE	SHEET NO.	APPROVED BY

DESIGN DESIGNATION
ADT (Current Year) 1982 = 15,800 Design Speed MPH
ADT (Future Year) = Based on Sight Distance
DHV (Design Hr. Vol.) = Height of eye Height of object
D (Directional Distr.) = % Design Speed not achieved at:
T (Heavy Commercial) = % STA. TO STA. MPH
STA. TO STA. MPH



STATE PROJ. NO. 6018-9090 (T.H. 2-307) SHEET NO. 1 OF 16 SHEETS

FED. PROJ. NO. F-6-002 (25) 358 NORTH DAKOTA
FED. PROJ. NO. F008-1 (62) MINNESOTA

GOVERNING SPECIFICATIONS

THE 1983 EDITION OF THE MINNESOTA DEPARTMENT OF TRANSPORTATION "STANDARD SPECIFICATIONS FOR CONSTRUCTION" SHALL GOVERN.

INDEX

SHEET NO.	DESCRIPTION
1	TITLE SHEET
2	ESTIMATE SHEET
3	GENERAL PLAN AND ELEVATION
4	REMOVAL & RECONSTRUCT SLAB JOINTS-TYPES OF REMOVAL-DRAIN DIAGRAM
5	RECONSTRUCT SLAB JOINT AT SWIVEL END OF TRUSS ONLY
6	RECONSTRUCT SLAB JOINT AT SWIVEL APPROACH SPANS
7	RECONSTRUCT SLAB JOINT AT SWIVEL AT PIER NO. 7
8	RAISE EXPANSION DEVICE
9	DETAILS OF NEW MEDIAN JOINT-5' 6" REMOVABLE END SPANS-DETAILS ON APPROACH MEDIAN
10 & 11	APPROACHES
12	APPROACH DRAINAGE SYSTEM
13	SLOPE PAVING
14	BRIDGE APPROACH PANEL
15	WATERPROOF EXPANSION DEVICE
16	TRAFFIC CONTROL

THIS PLAN CONTAINS 16 SHEETS

I HEREBY CERTIFY THAT THIS PLAN WAS PREPARED BY ME OR UNDER MY DIRECT SUPERVISION AND THAT I AM A DULY REGISTERED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF MINNESOTA.

DATE Jan 18, 1984 REG. NO. 7176 ENGR. Roger Bachmann
DESIGN SQUAD Roger Bachmann with B.P.S. and K.W.P.

Right of Way Approval 1-26-1984
DIRECTOR, RIGHT OF WAY OPERATIONS

Recommended for Approval 19
DISTRICT ENGINEER

Recommended for Approval 19
TRANSPORTATION PLANS ENGINEER

Recommended for Approval 19
DESIGN SERVICES DIRECTOR

Recommended for Approval 1-26-1984
for BRIDGE ENGINEER

Approved 1/26/1984 Ed J. Smith
ASSISTANT DIVISION DIRECTOR

DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION	
APPROVED	DATE
DIVISION ADMINISTRATOR	DATE

I HEREBY CERTIFY THAT THE FINAL FIELD REVISIONS, IF ANY, OF THIS PLAN WERE MADE BY ME OR UNDER MY DIRECT SUPERVISION AND THAT I AM A DULY REGISTERED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF MINNESOTA.

DATE REG. NO.

THE FOLLOWING STANDARD PLATES, APPROVED BY THE FEDERAL HIGHWAY ADMINISTRATION, SHALL APPLY ON THIS PROJECT.	
PLATE NO.	DESCRIPTION
D004A	SPECIFICATION REFERENCE TO STANDARD PLATES
I016G	CONCRETE PAVEMENT NON-REINFORCED
I018B	CONCRETE PAVEMENT WITH STEEL FABRIC REINFORCEMENT
I100N	EXPANSION JOINTS
I103I	TYPICAL DOWEL BAR ASSEMBLY
I120R	CONTRACTION JOINTS
I140R	LONGITUDINAL JOINTS
I141C	PAVEMENT KEYWAY
3142A	OUTLET SCREEN FOR C.M. PIPE
4010F	CONCRETE ADJUSTING RING
7020J	CONCRETE CURB
7035J	CONCRETE WALK
7100F	CONCRETE CURB & GUTTER
8000H	STANDARD BARRICADES
8333A	TEMPORARY PORTABLE PRECAST CONCRETE BARRIER, DESIGN 8333A

CONSTRUCTION NOTES:

IMMEDIATELY PRIOR TO PLACING NEW CONCRETE AGAINST ANY ORIGINAL CONCRETE A BONDING GROUT SHALL BE APPLIED TO THE VERTICAL CONTACT SURFACES OF THE INPLACE CONCRETE.

NO CUTTING WILL BE PERMITTED UNTIL THE CUTTING LIMITS HAVE BEEN OUTLINED BY THE CONTRACTOR AND APPROVED BY THE ENGINEER. REMOVAL AND RECONSTRUCTION SHALL CONFORM TO M.N.D.O.T. 2433.

PREFORMED JOINT FILLER MATERIALS ARE INCIDENTAL. PAYMENT TO BE INCLUDED IN PRICE BID FOR OTHER ITEMS.

PROVIDE SAW CUT IN CONCRETE WEARING COURSE OVER ALL CONSTRUCTION JOINTS IN EXISTING SLAB AND SEAL WITH CONCRETE JOINT SEALER PER SPEC. 3723.

CONTRACTOR SHALL MAKE FIELD MEASUREMENTS AS NECESSARY, PRIOR TO FABRICATION OF THE WATERPROOF EXPANSION JOINT DEVICES AND CURB PLATES, TO ASSURE PROPER FIT IN THE FINAL WORK.

THE FIRST DIGIT OF THE FIRST TWO DIGITS OF EACH BAR MARK INDICATES BAR SIZE.

BARS MARKED WITH THE SUFFIX "E" SHALL BE EPOXY COATED.

FIELD CUTTING OF NO. 4 REINFORCEMENT BARS WILL BE REQUIRED IN ORDER TO MEET MINIMUM 1'-0" LAP REQUIREMENTS FOR LONGITUDINAL DECK REBAR EXTENSIONS IN FIXED JOINT RECONSTRUCTIONS.

PLANS OF THE INPLACE BRIDGE NO. 9090 ARE AVAILABLE AT THE MINNESOTA DEPARTMENT OF TRANSPORTATION, BEMIDJI AND ST. PAUL. THEY ARE ALSO AVAILABLE AT THE NORTH DAKOTA STATE HIGHWAY DEPARTMENT IN GRAND FORKS AND BISMARCK.

9

STATEMENT OF ESTIMATED QUANTITIES				
ITEM NO.	ITEMS WITHOUT ALTERNATES	UNIT	ESTIMATED QUANTITIES	FINAL QUANTITIES
2021.501	MOBILIZATION	LUMP SUM	1	
2031.503	FIELD LABORATORY, TYPE DX	EACH	1	
2104.501	REMOVE CURB AND GUTTER	LIN. FT.	640	
2104.503	REMOVE SIDEWALK	SQ. FT.	104	
2104.505	REMOVE CONCRETE PAVEMENT	SQ. YD.	416	
2104.505	REMOVE BITUMINOUS PAVEMENT	SQ. YD.	94	
211.1505	REMOVE CONCRETE APPROACH PANELS	SQ. YD.	200	
2105.501	COMMON EXCAVATION	CU. YD.	346 (P)	
(7) 2211.501	AGGREGATE BASE, CLASS 3 (MOD)	TON	351	
2211.501	AGGREGATE BASE, CLASS 5	TON	241	
2301.501	CONCRETE PAVEMENT	SQ. YD.	494	
2301.511	STRUCTURAL CONCRETE	CU. YD.	132	
2301.521	PAVEMENT REINF. TYPE 612-D4.9 XD4.0	SQ. YD.	403	
2301.551	BRIDGE APPROACH PANEL, DESIGN C	EACH	2	
301.604	CLEAN & SEAL CONCRETE JOINTS	LIN. FT.	314	
2331.504	BITUMINOUS MATERIAL FOR MIXTURE	TON	4.5	
2331.508	WEARING COURSE MIXTURE	TON	49	
2401.511	STRUCTURE CONCRETE (3X33)	SQ. FT.	600	
2401.512	BRIDGE SLAB CONCRETE (3X33)	SQ. FT.	616	
2401.541	REINFORCEMENT BARS	POUND	22185 (P)	
2401.541	REINFORCEMENT BARS (EPOXY COATED)	POUND	2205 (P)	
401.612	SILICONE RAIL TREATMENT	SQ. FT.	17969 (P)	
2402.591	EXPANSION JOINT DEVICE, TYPE 3.0	LIN. FT.	642	
402.601	DRAINAGE SYSTEM	LUMP SUM	1	
(1) (2) ALTERNATE 1-1	404.602 CONCRETE OVERLAY 3UITA	CU. YD.	532	
(1) (2) ALTERNATE 1-2	404.602 CONCRETE OVERLAY LATEX	CU. YD.	416	
(3) 2433.505	REMOVE SLAB, TYPE 1	SQ. FT.	2400	
(3) 2433.505	REMOVE SLAB, TYPE 3	SQ. FT.	600	
(4) 2433.505	REMOVE CONCRETE BRIDGE DECK	SQ. FT.	616 (P)	
2433.507	REMOVE DEBRIS	LUMP SUM	1	
433.601	SCARIFY BRIDGE DECK	SQ. FT.	70000	
433.601	SCARIFY CONCRETE APPROACHES	SQ. FT.	4480	
433.607	RECONSTRUCT FIXED JOINT, TYPE D	LIN. FT.	470	
433.607	RECONSTRUCT FIXED JOINT, TYPE E	LIN. FT.	134	
433.607	RECONSTRUCT FIXED JOINT, TYPE F	LIN. FT.	67	
433.607	RAISE EXPANSION JOINT DEVICE	LIN. FT.	134	
433.607	RECONSTRUCT MEDIAN JOINT (TYPE I)	LIN. FT.	1261	
(5) 2476.502	CLEAN STRUCTURAL STEEL	SQ. FT.	36100	
(5) 2476.502	PRIME COAT STRUCTURAL STEEL	SQ. FT.	36100	
(5) 2476.502	FINISH COAT STRUCTURAL STEEL	SQ. FT.	18000	
404.603	WEARING COURSE FINISH	SQ. FT.	75485	
2506.522	ADJUST FRAME & RING CASTING	EACH	1	
2514.501	CONCRETE SLOPE PAVING	SQ. YD.	333	
2521.501	4" CONCRETE WALK	SQ. FT.	504	
2531.501	CONCRETE CURB & GUTTER, DESIGN B924	LIN. FT.	536	
2531.502	CONCRETE CURB, DESIGN BR 6-10	LIN. FT.	136	
554.603	CONCRETE MED. BARRIER DESIGN 8333A	LIN. FT.	2150	
583.601	TRAFFIC CONTROL	LUMP SUM	1	

(1) SEE TABULATION ON SHEET 4 FOR ESTIMATED QUANTITIES OF LOW SLUMP AND LATEX OPTIONS.

(2) SEE TABULATION ON SHEET 10 FOR ESTIMATED QUANTITIES OF LOW SLUMP AND LATEX.

(3) 5' - 6" REMOVABLE SLABS AT EACH ABUTMENT, INCLUDES CURBS.

(4) SEE SPECIAL PROVISIONS.

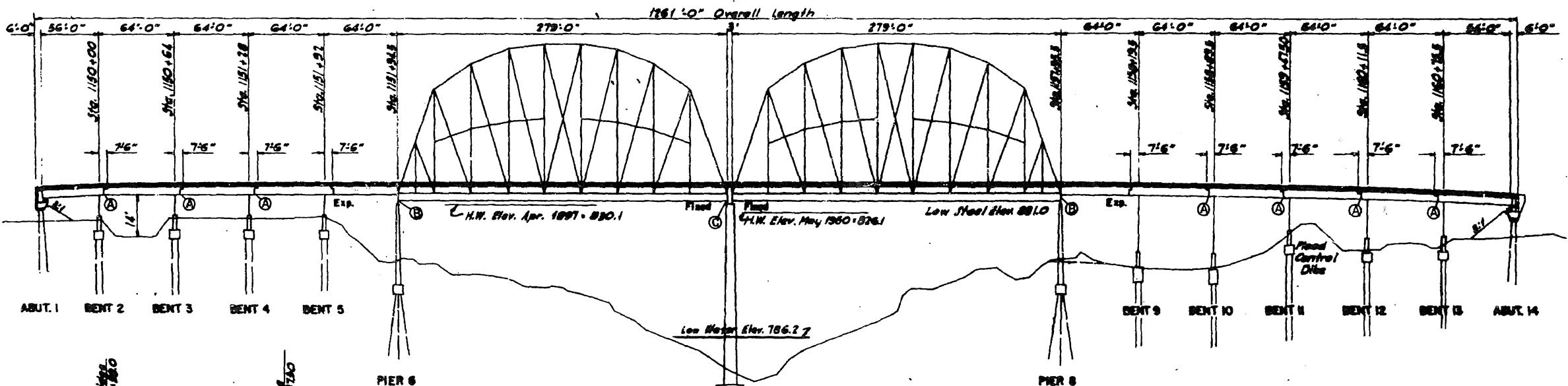
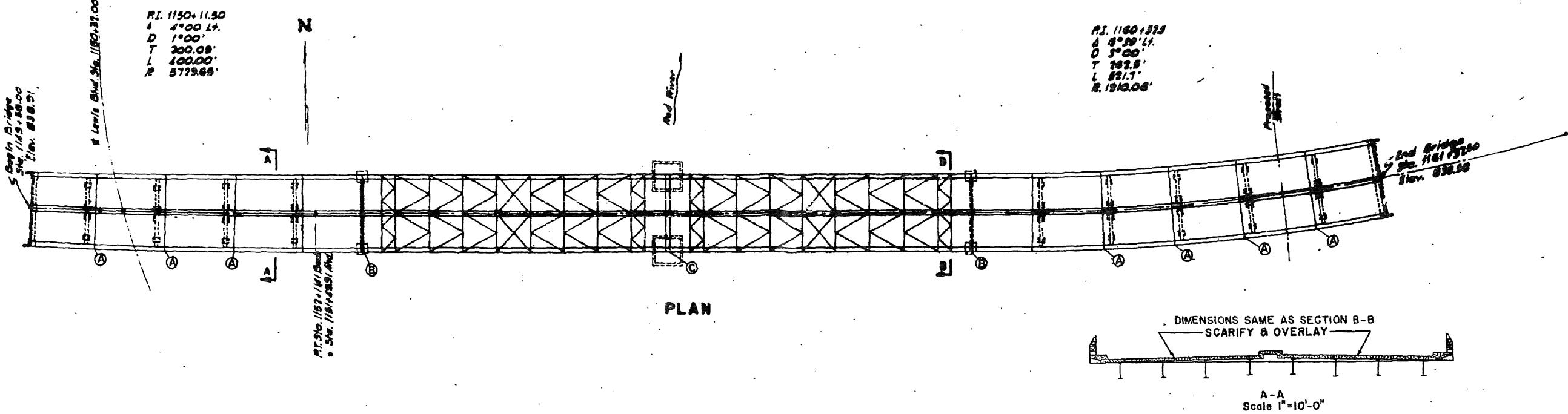
(5) CONFINED TO STEEL MEMBERS BELOW AND WITHIN CONCRETE REMOVAL LIMITS.

(6) INCLUDES APPROXIMATELY 400 SQ. FT. OF SPLASH PADS UNDER EXPANSION JOINT TROUGHS.

(7) INCLUDES 39 TONS FOR SLOPE PAVING FOUNDATION PREPARATION.

TITLE: ESTIMATED QUANTITIES	DES: _____	DR: _____	APPROVED: _____	Bridge No. _____
	CNK: _____	CNK: _____	1-26-87	9090

Sheet No. 2 of 16 Sheets

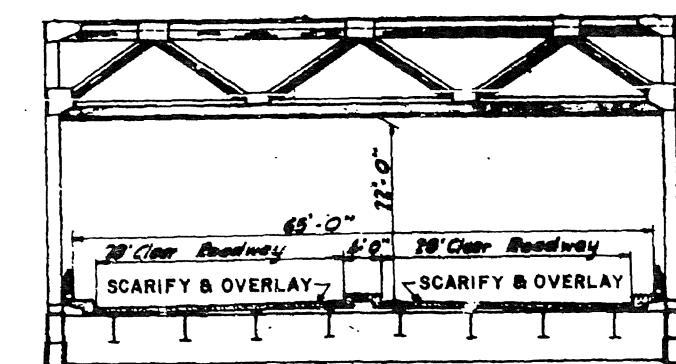


- ④ REMOVE INPLACE EXPANSION JOINT TYPE "D", INSTALL NEW TYPE 3.0 WATERPROOF JOINT
- ⑤ REMOVE INPLACE EXPANSION JOINT TYPE "E", INSTALL NEW TYPE 3.0 WATERPROOF JOINT
- ⑥ REMOVE INPLACE EXPANSION JOINT TYPE "F", INSTALL NEW TYPE 3.0 WATERPROOF JOINT

P.J. 1146+38 Elev. 827.80
H.W. 1146+40 Elev. 829.00
K.C. 200' V.C. 186' K.C. 200'

VERTICAL CURVE DATA
Elevations are to top of finished roadway beside Median Curb

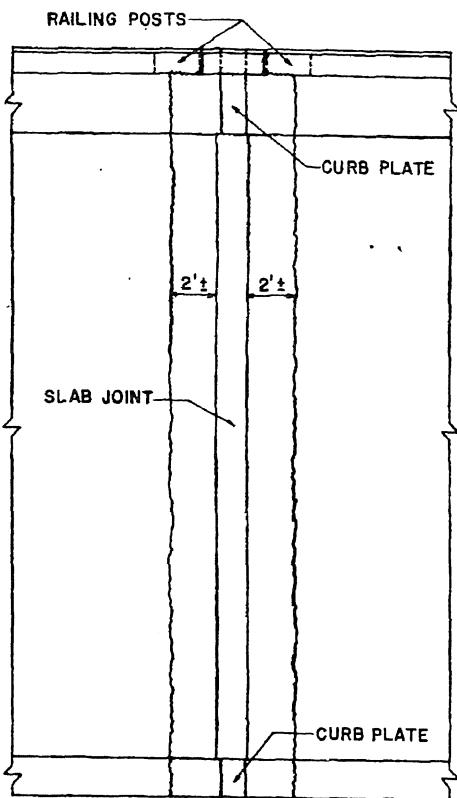
B.M. ELEV. 833.527 (6019 A)
M.H.D. DISK LOCATED ON THE SOUTHEAST WINGWALL OF BRIDGE 60001
ON T.H. 2, MILEPOST 0.24 (1965)



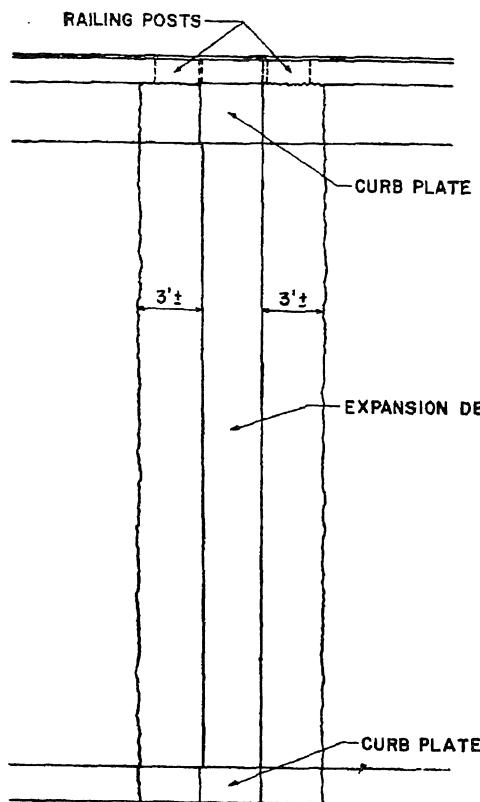
B-8
Scale 1"=10'-0"

TITLE: GENERAL PLAN & ELEVATION	DES:	DR:	APPROVED:
CNR:	CNR:		1-26-84
Sheet No. 3 of 16 Sheets			Bridge No. 9090

**REMOVAL AT INPLACE SLAB JOINTS
(7 SWIVEL APPROACH SPANS) (PIER NO. 7)
(ENDS OF HIGH TRUSS)**

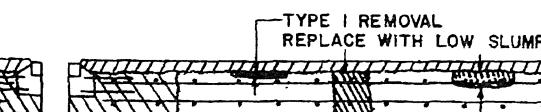
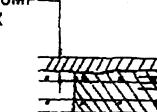


REMOVAL AT INPLACE EXPANSION DEVICES



TYPES OF REMOVAL

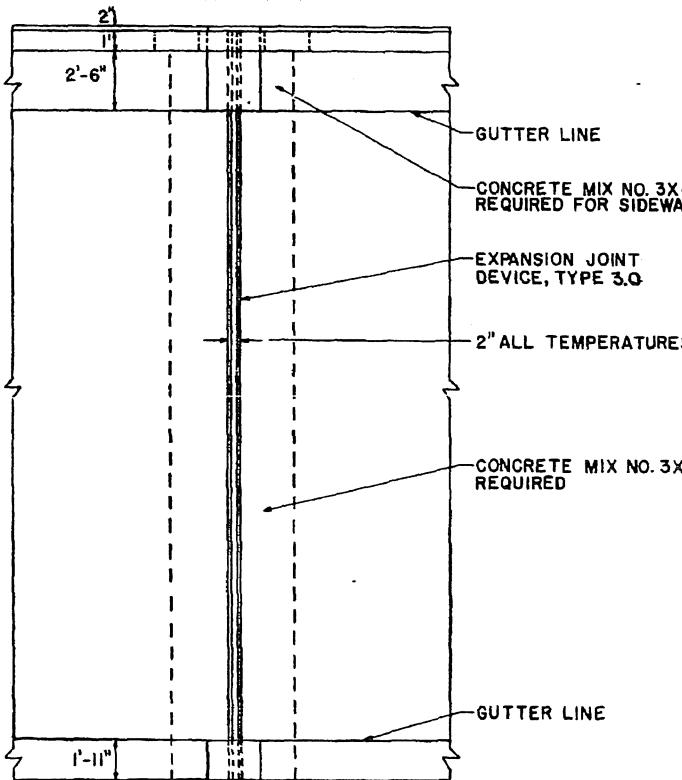
2" MINIMUM LOW SLUMP
1 1/2" MINIMUM LATEX



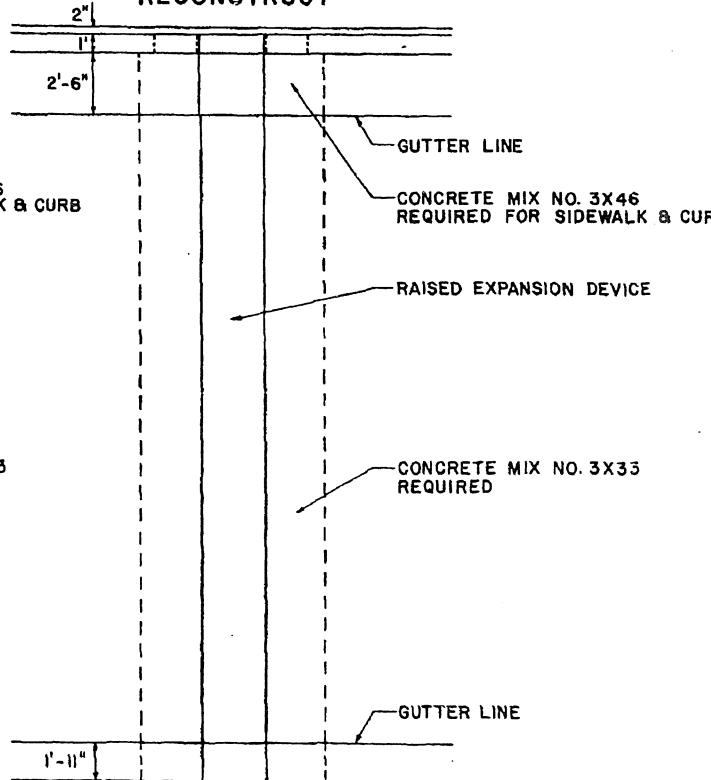
TYPE I REMOVAL
REPLACE WITH LOW SLUMP OR LATEX CONCRETE
PARTIAL DEPTH TYPE 3 REMOVAL
REPLACE WITH CONCRETE MIX NO. 3X33 OR 3X37.

PARTIAL DEPTH TYPE 3 REMOVAL
REPLACE WITH CONCRETE MIX NO. 3X37

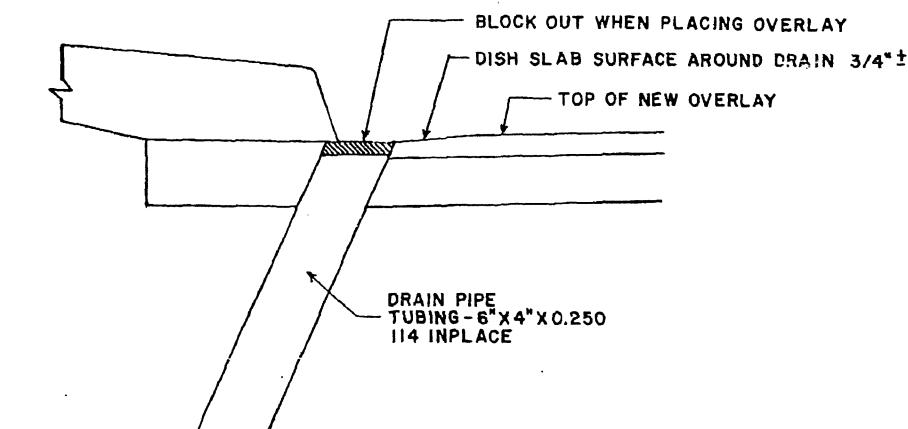
RECONSTRUCT



RECONSTRUCT



SECTION AT DRAINS



NOTE: WORK REQUIRED AT DRAINS WILL BE INCIDENTAL
TO THE PLACEMENT OF THE CONCRETE OVERLAY
APPROXIMATELY 490 CU.YDS. OF CONCRETE MIX NO. 3U17A (LOW SLUMP) WILL BE
REQUIRED FOR THE BRIDGE DECK OR 381 CU.YDS. OF LATEX OVERLAY.
LOW SLUMP COMPUTED AT 2 1/4" THICK
LATEX COMPUTED AT 1 3/4" THICK

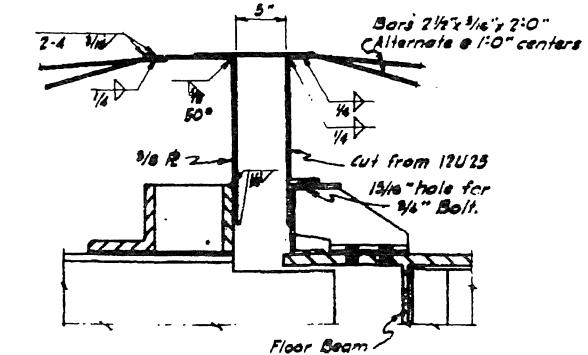
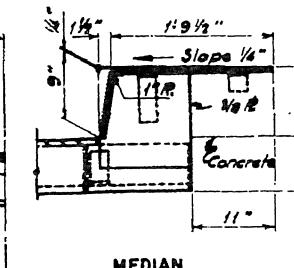
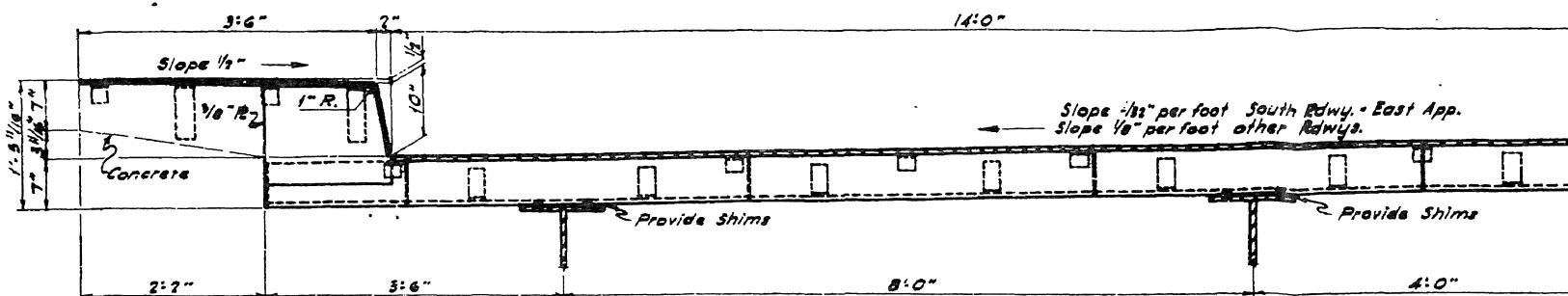
REMOVAL & RECONSTRUCT AT
SLAB JOINTS - TYPES OF
REMOVAL - DRAIN DIAGRAM

DES:	DR:	APPROVED:
CHM:	CHM:	1-26-84

Bridge No.
Sheet No. 4 of 16 Sheets

9090

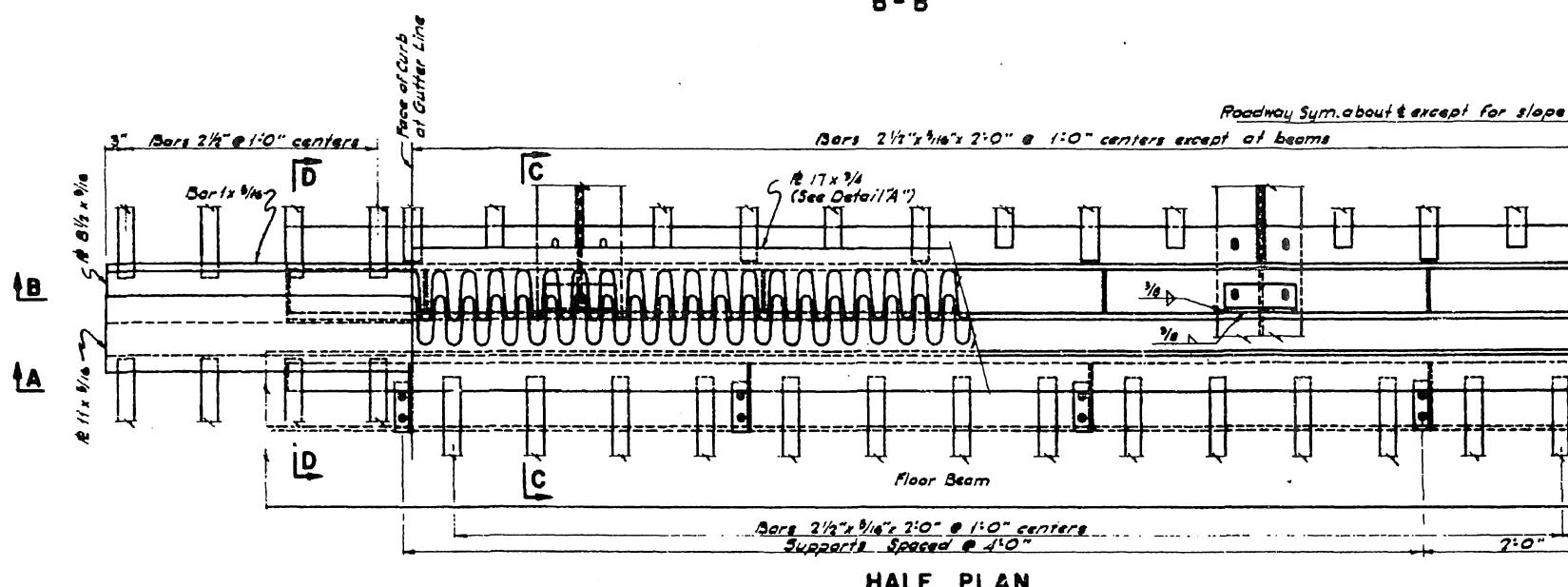
INPLACE SLAB JOINTS AT
SWIVEL END OF TRUSS (2)
TYPE "E"



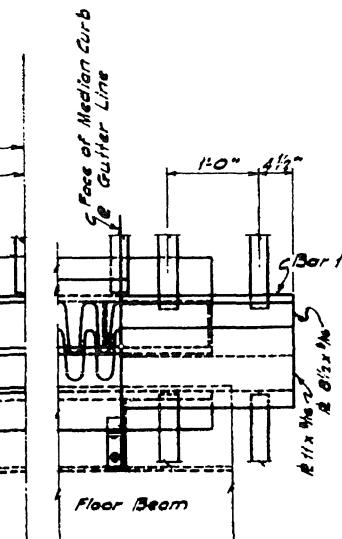
B-B

MEDIAN

D-D



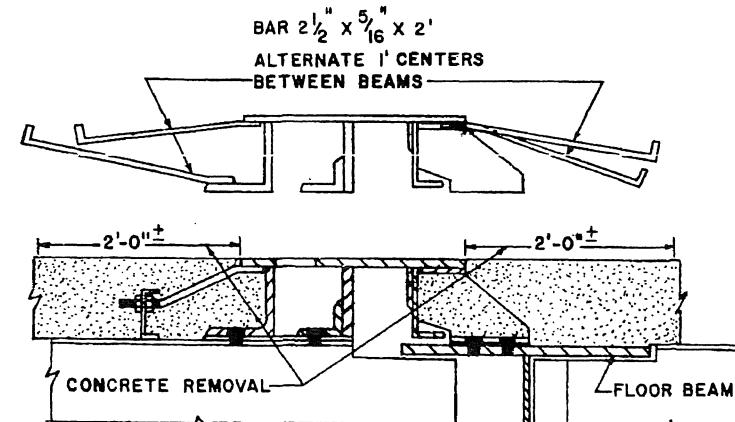
HALF PLAN



MEDIAN

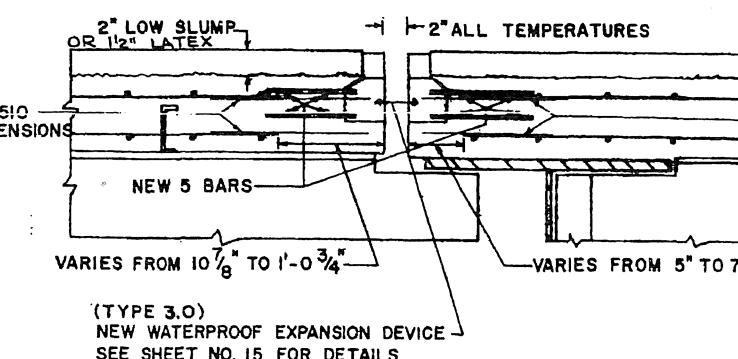
CONSTRUCTION NOTE: FIELD CUTTING OF NO. 408 & 510 REBARS WILL BE REQUIRED IN ORDER TO MEET MINIMUM 1'-0" LAP FOR LONGITUDINAL DECK REBAR EXTENSIONS.

C-C REMOVAL



NEW NO. 408 BARS TOP, 510 BARS BOTTOM FOR EXTENSIONS ON LONGITUDINAL DECK REBARS (2' LONG)

CONSTRUCT



(TYPE 3.0)
NEW WATERPROOF EXPANSION DEVICE
SEE SHEET NO. 15 FOR DETAILS

NEW NO. 408 BARS TOP, NO. 510 BARS BOTTOM FOR EXTENSIONS ON LONGITUDINAL DECK REBARS (2' LONG)

EXISTING LONGITUDINAL REBARS TO REMAIN INPLACE

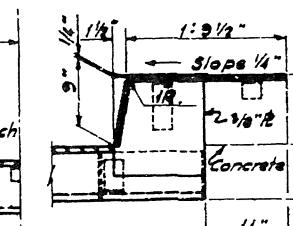
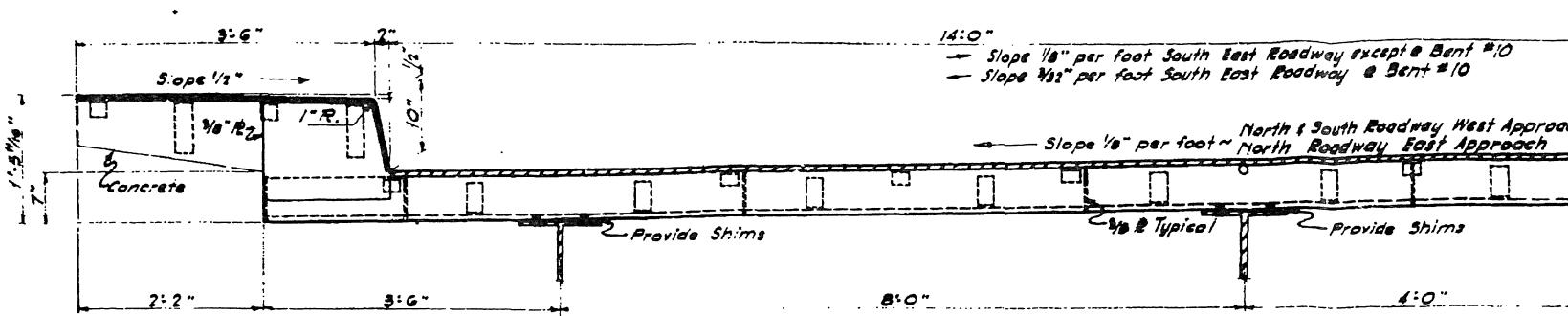
TITLE: RECONSTRUCT SLAB JOINT AT SWIVEL (END OF TRUSS ONLY)

DES:	DR: R.L.B.	APPROVED:
CHK:	CHK:	1-26-87

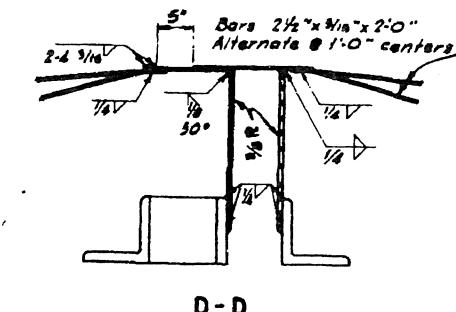
Bridge No.
9090

Sheet No. 5 of 16 Sheets

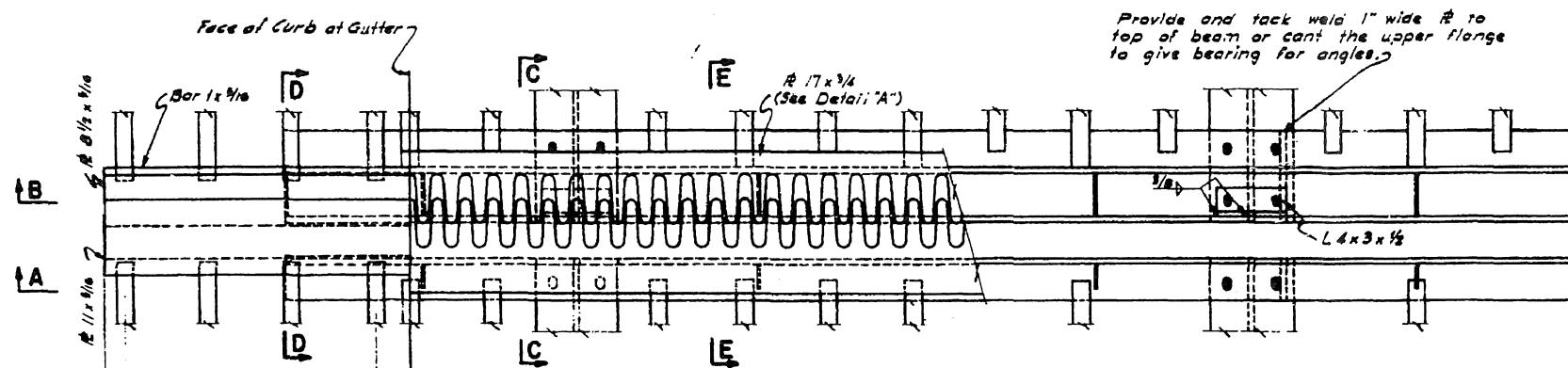
INPLACE SLAB JOINTS AT
SWIVEL APPROACH SPANS (7)
TYPE "D"



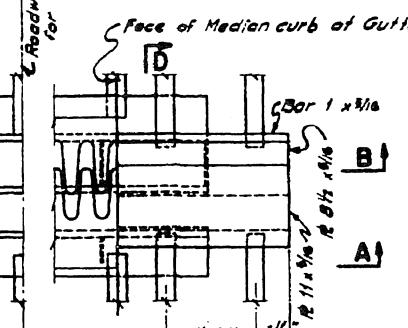
MEDIAN



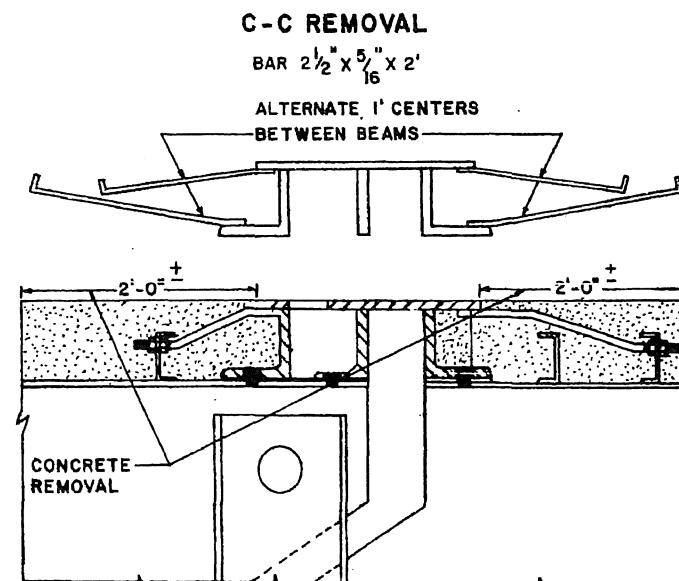
D-D



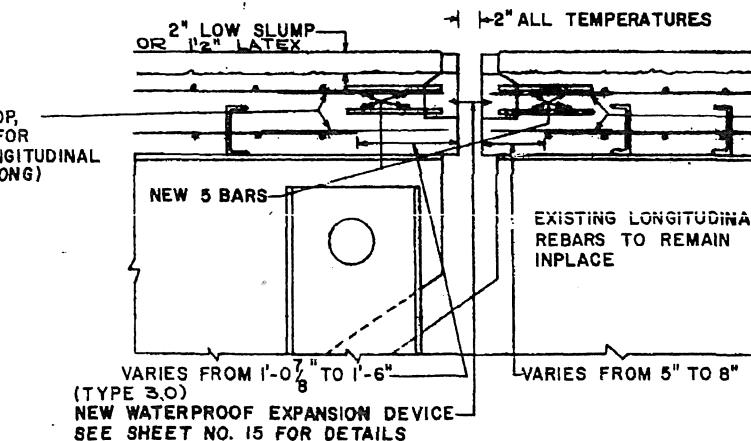
HALF PLAN



MEDIAN



NEW NO. 408 BARS TOP,
510 BARS BOTTOM FOR
EXTENSIONS ON LONGITUDINAL
DECK REBARS (2'-± LONG)



NEW NO. 408 BARS TOP, 510 BARS
BOTTOM FOR EXTENSIONS ON
LONGITUDINAL DECK REBARS (2'-± LONG)

CONSTRUCTION NOTE: FIELD CUTTING OF NO. 408
8 510 REBARS WILL BE
REQUIRED IN ORDER TO
MEET MINIMUM 1'-0" LAP
FOR LONGITUDINAL DECK
REBAR EXTENSIONS.

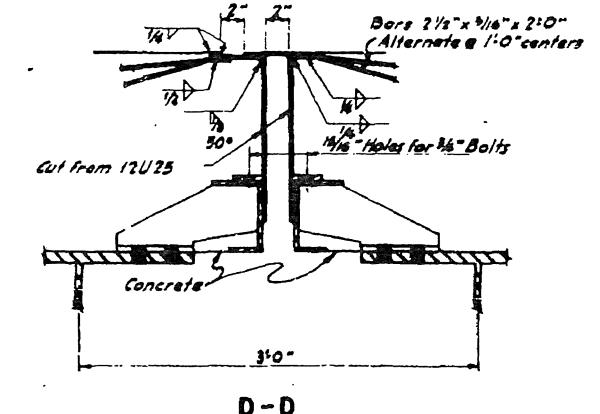
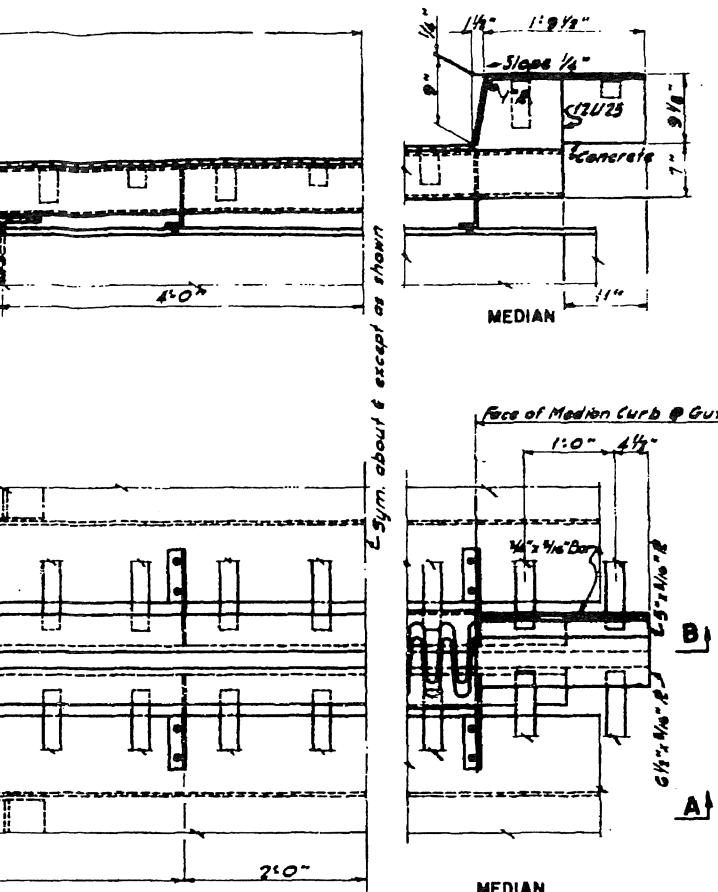
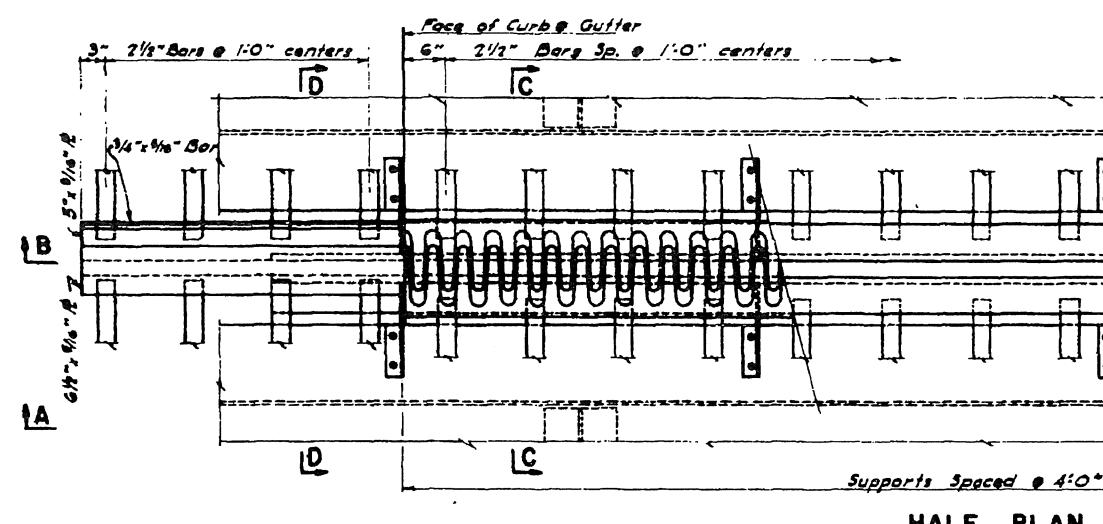
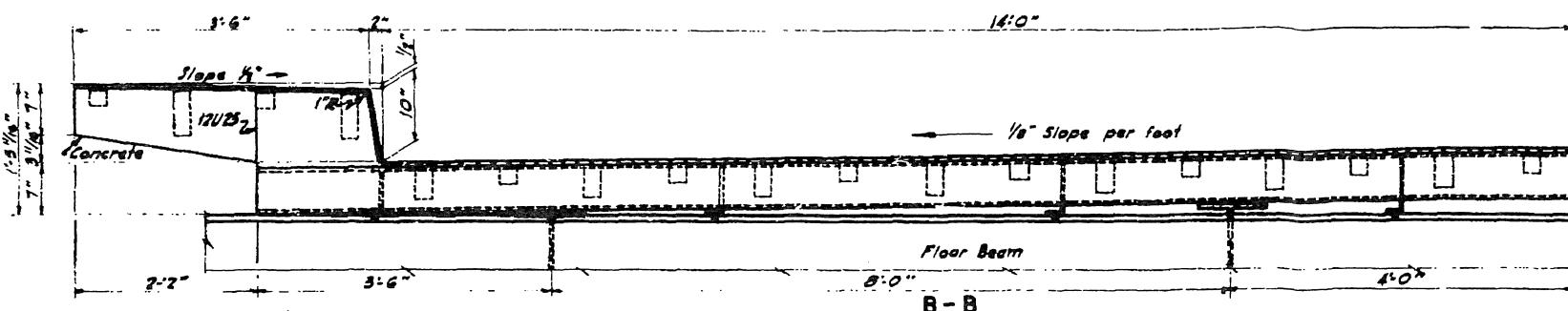
TITLE: RECONSTRUCT SLAB JOINT AT SWIVEL (APPROACH SPANS)

DES:	DR: R.L.B	APPROVED:
CHK:	CHK:	1-26-84

Bridge No.
9090

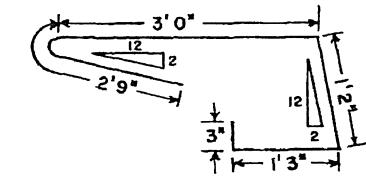
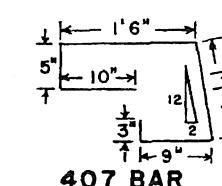
Sheet No. 6 of 16 Sheets

INPLACE SLAB JOINT AT
PIER NUMBER 7 (1)
TYPE "F"

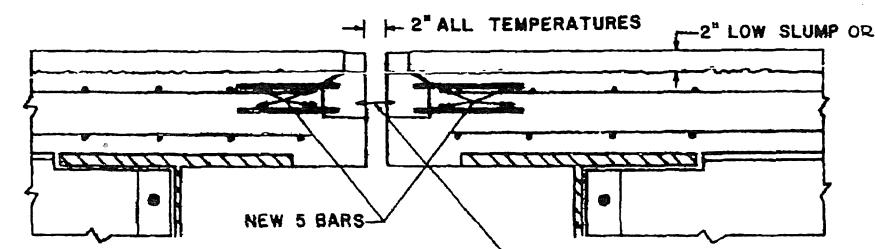


BILL OF REINFORCEMENT				
BAR NO.	LENGTH	SHAPE	LOCATION	
505	524	30.17	STR.	SLAB TRANSVERSE
506	94	8.00	BENT	SIDEWALK
407	94	4.83	BENT	MEDIAN CURB
408	85	20.00	STR.	SLAB, MED. CURB & S.W. LONG.
609	6	20.00	STR.	MED. CURB & S.W. LONG.
510	75	20.00	STR.	SLAB LONG.

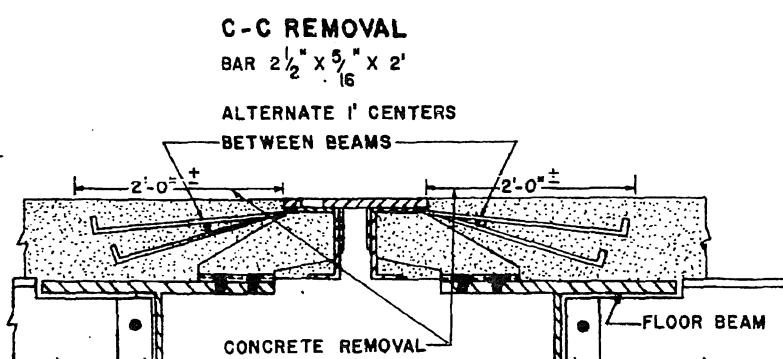
NOTE:
1) 506 AND 407 REBARS SHALL BE USED IN MEDIAN CURB AND SIDEWALK AS REQUIRED.
2) 408, 609 AND 510 REBARS SHALL BE CUT IN THE FIELD.



CONSTRUCT



→ 2" ALL TEMPERATURES
→ 2" LOW SLUMP OR 1 1/2" LATEX
EXISTING LONGITUDINAL REBARS TO REMAIN INPLACE
(TYPE 3.0)
NEW WATERPROOF EXPANSION DEVICE
SEE SHEET NO. 15 FOR DETAILS



TITLE: RECONSTRUCT SLAB JOINT
AT PIER NO. 7

DES:

DR: R.L.B.

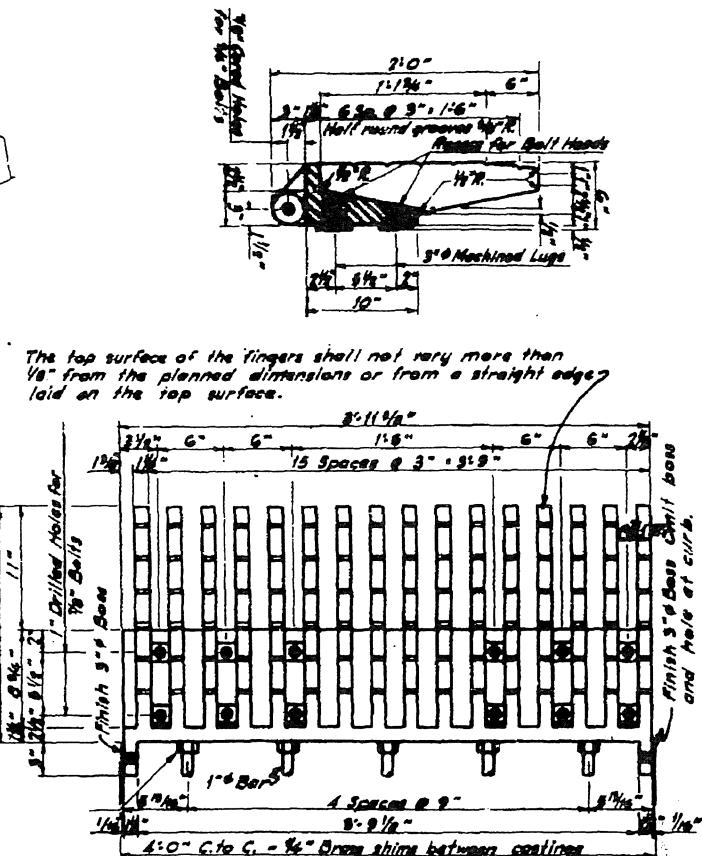
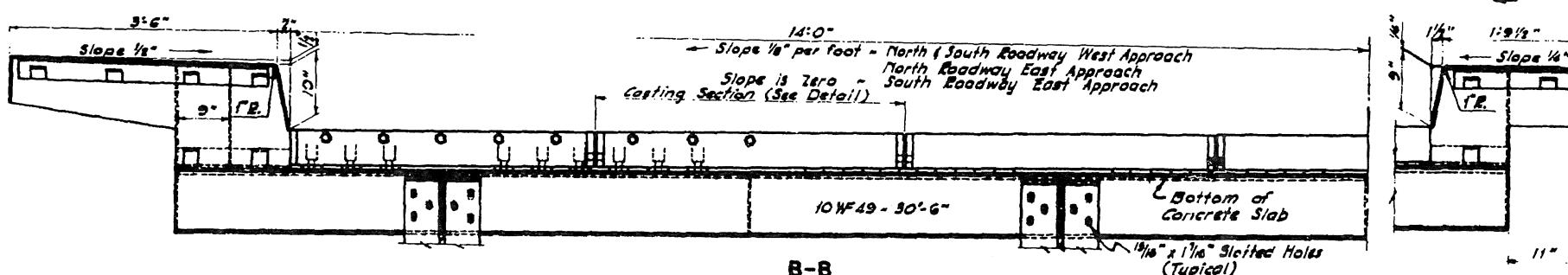
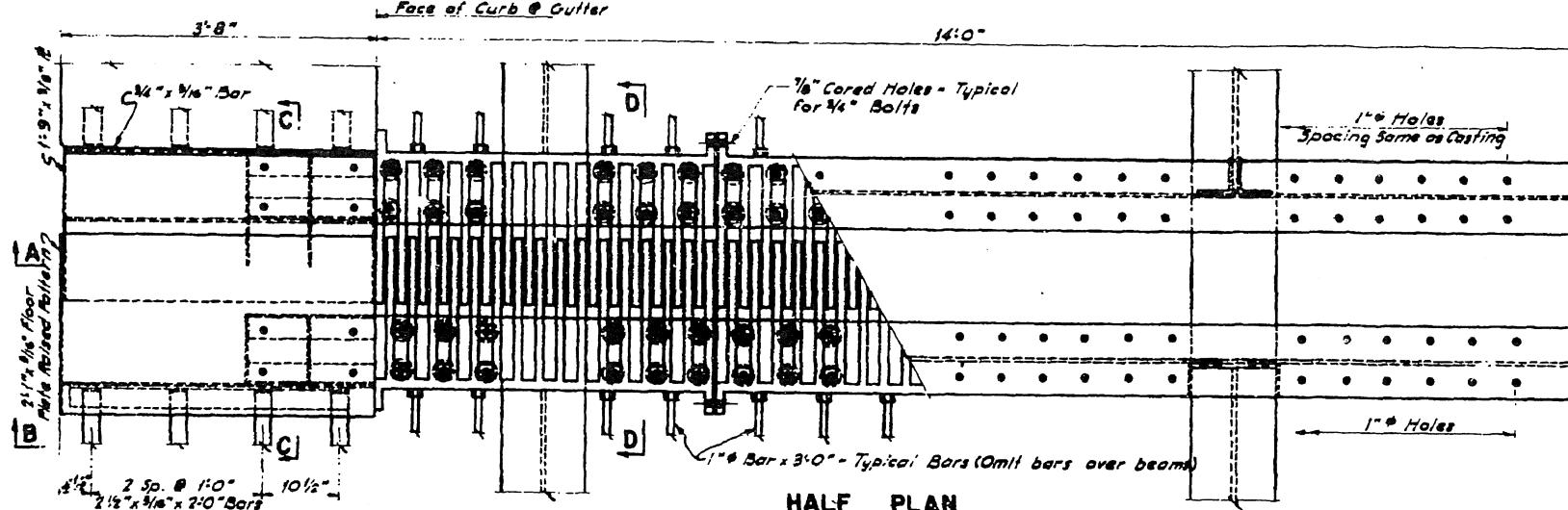
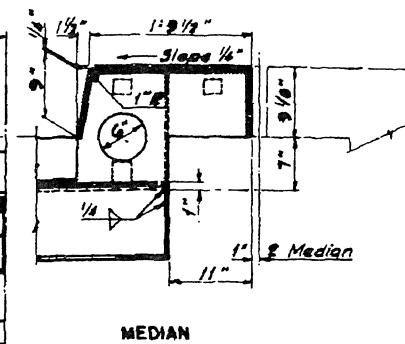
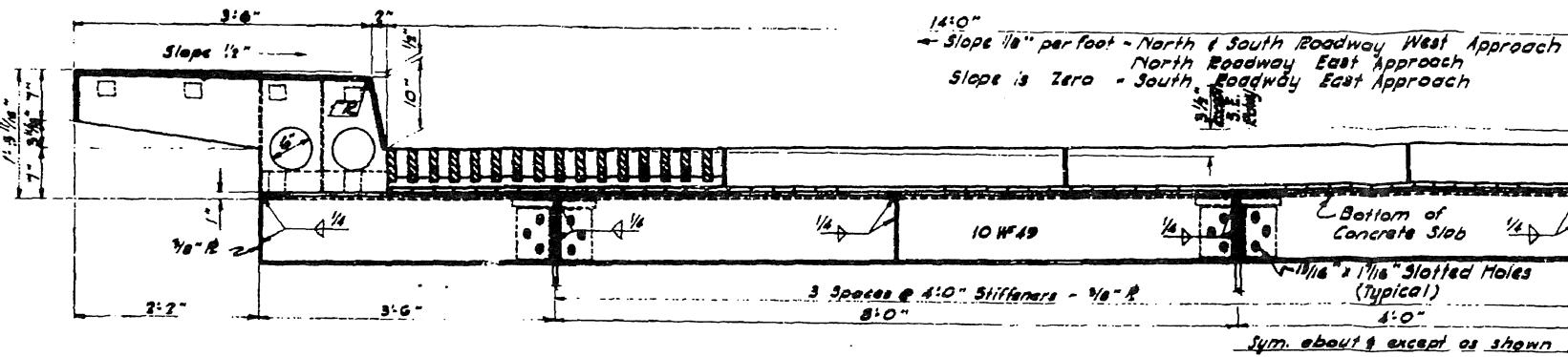
APPROVED:

1-26-84

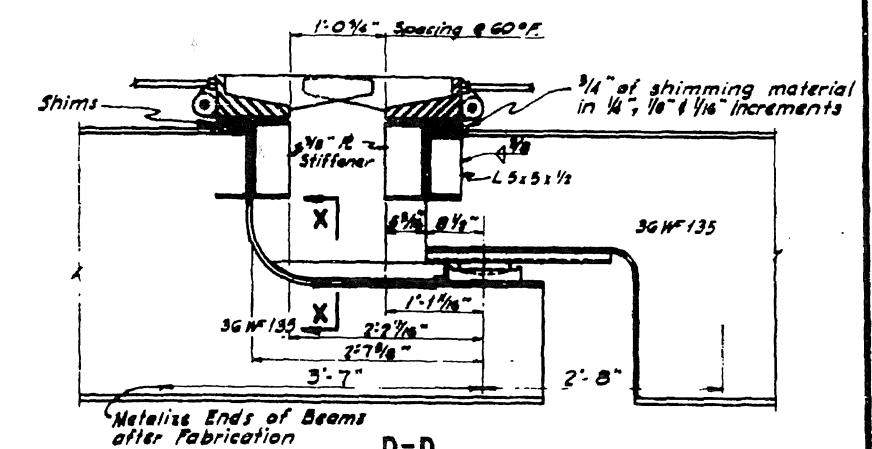
Bridge No.
9090

CHK: Sheet No. 7 of 16 Sheets

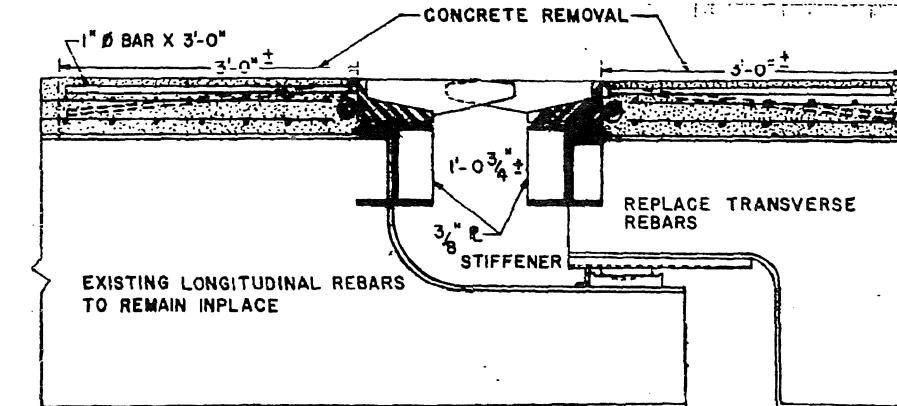
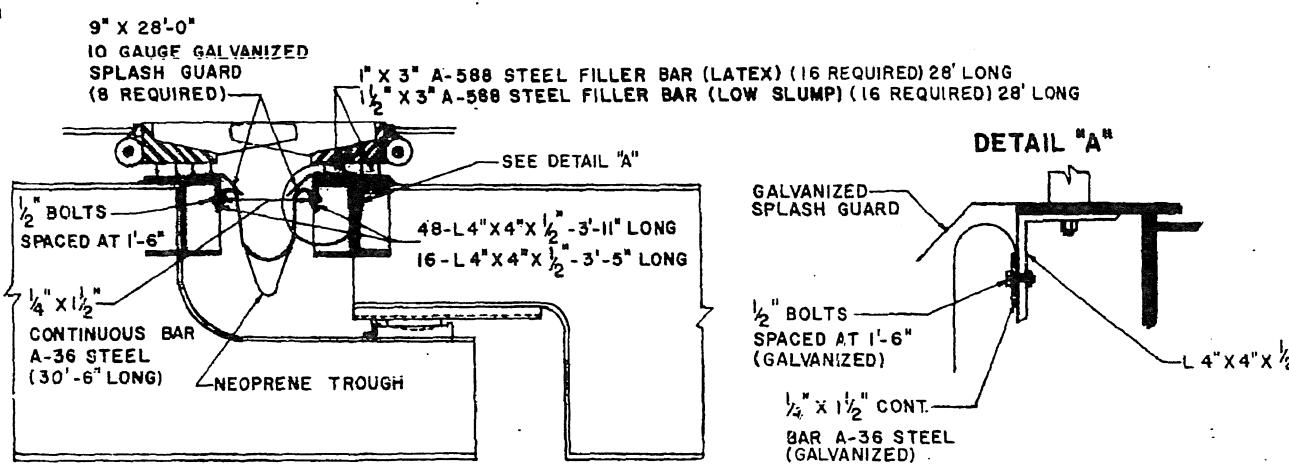
INPLACE EXPANSION DEVICE



DETAIL OF STEEL CASTING



RAISED EXPANSION DEVICE



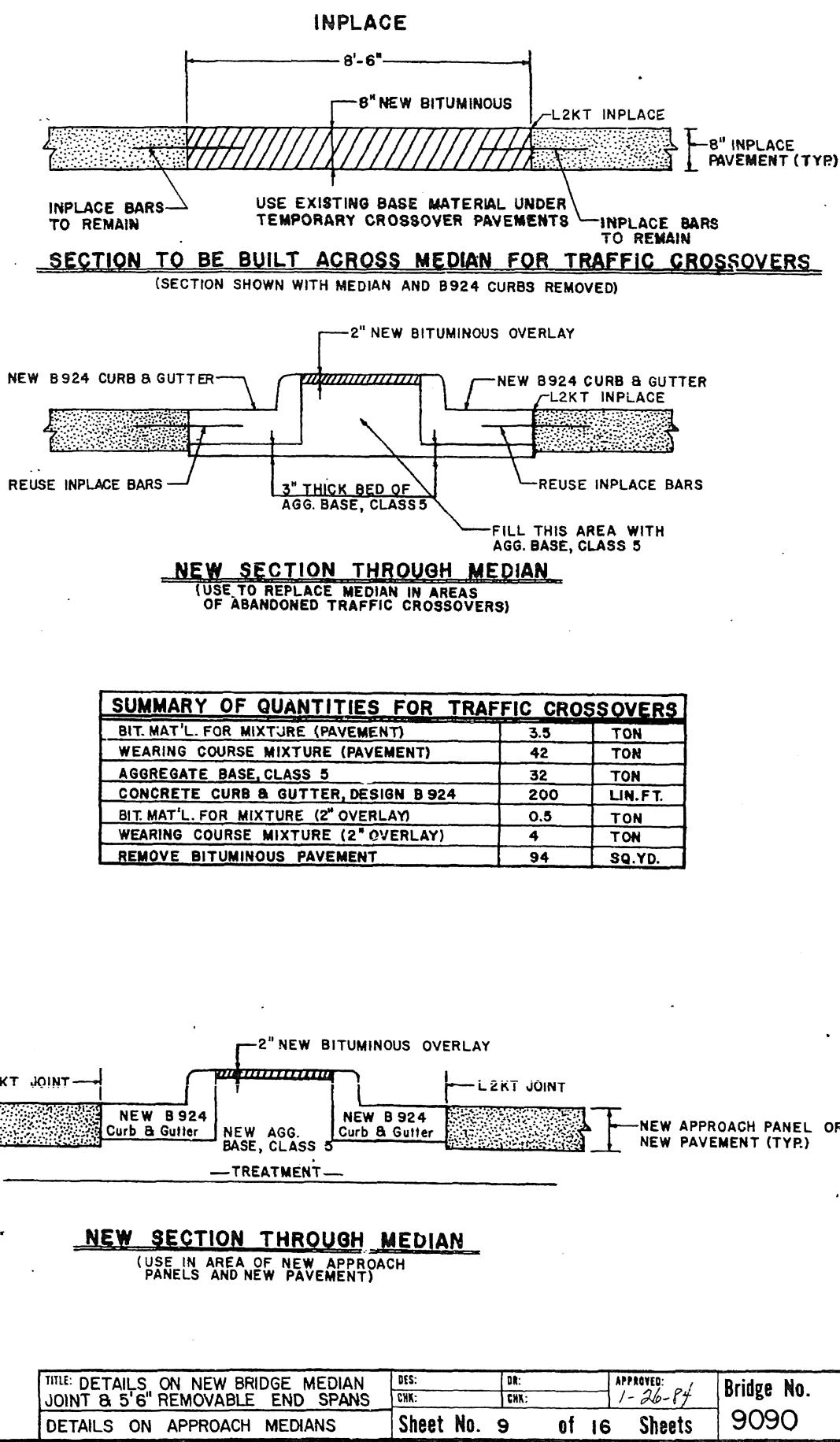
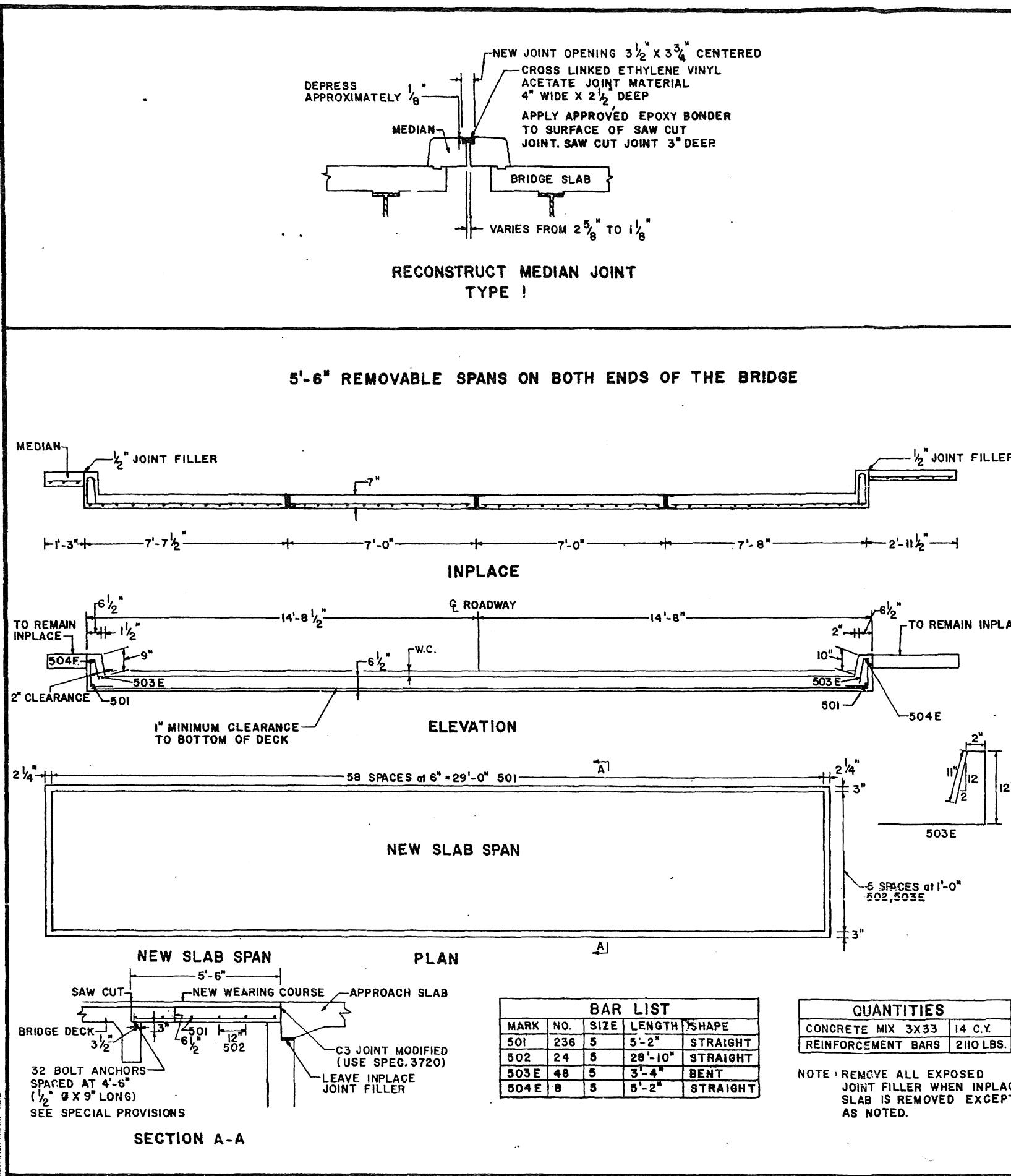
CONSTRUCTION NOTES

- COVER PLATES ON SIDEWALK & CURB FOR EXPANSION DEVICES WILL BE CUT OFF NECESSARY TO RAISE EXPANSION DEVICE AND REWELDED AND GALVANIZED.

TITLE:
RAISE EXPANSION DEVICE

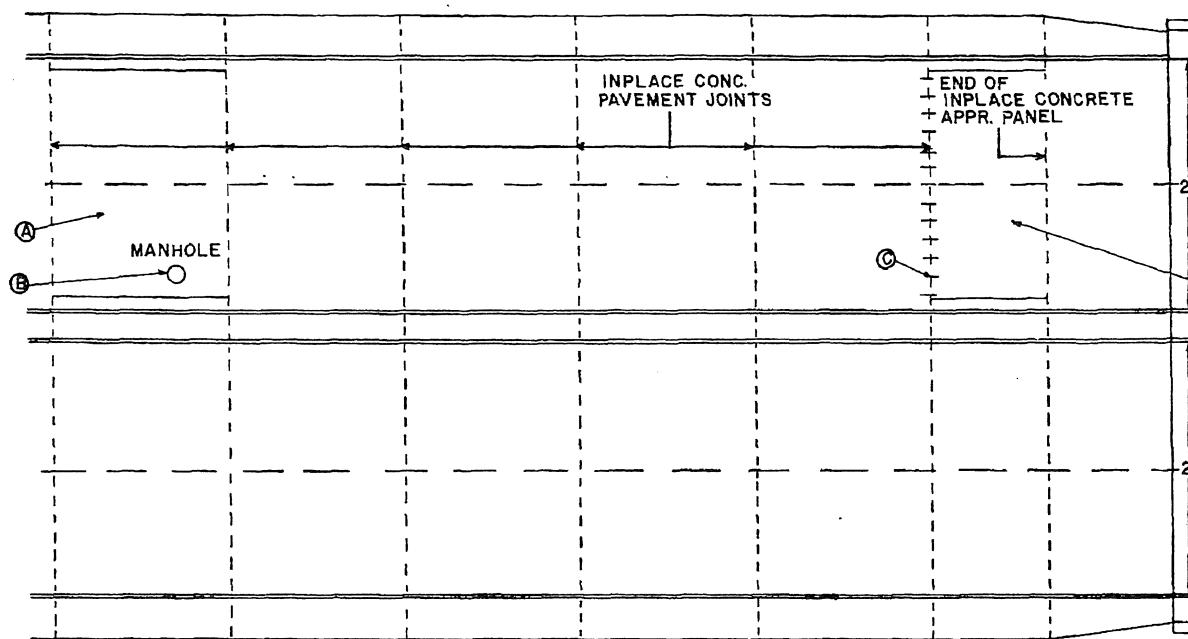
DES:	DR: R.L.B.	APPROVED:	1-26-84
CHK:	CHK:		

Bridge No.
9090

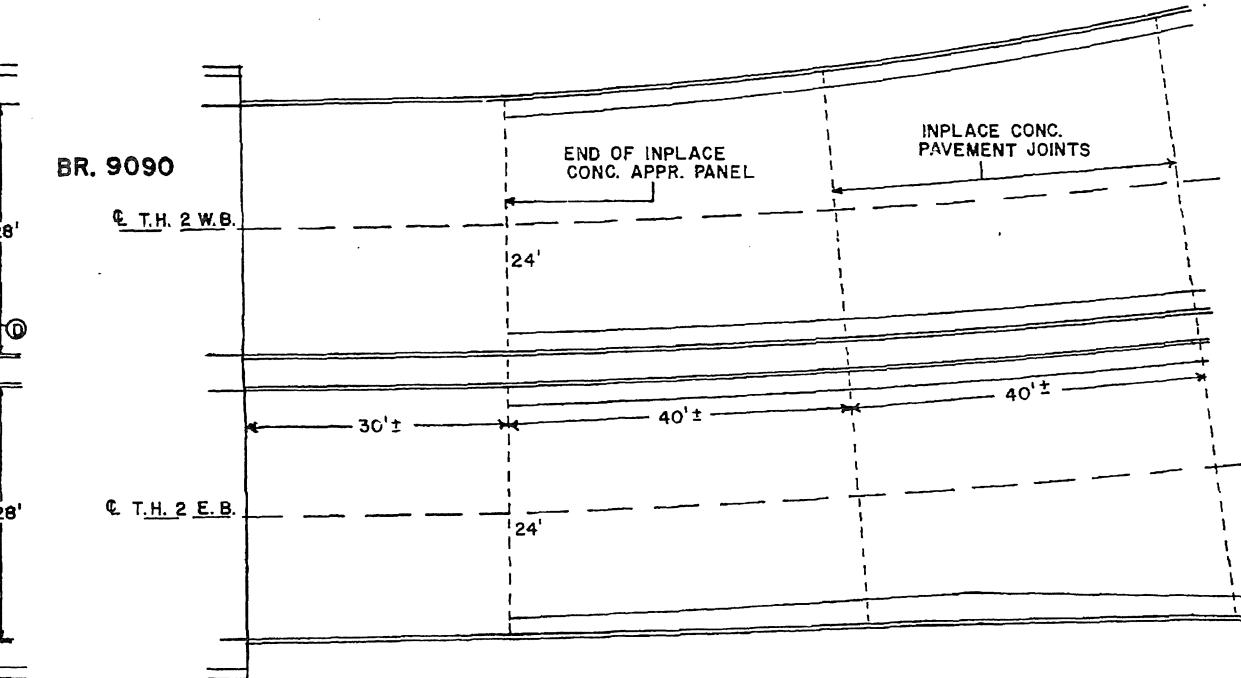


INPLACE

WEST APPROACH

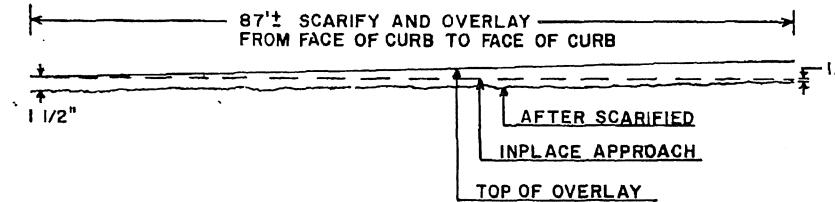


EAST APPROACH



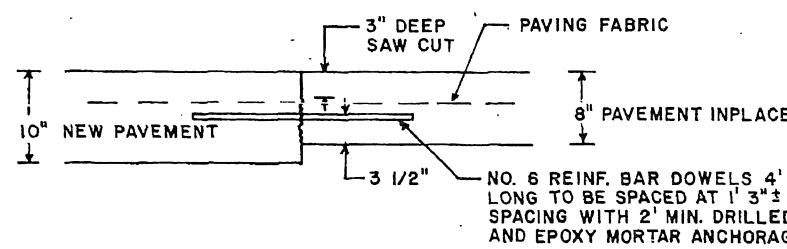
CONSTRUCT

- (A) REMOVE PAVEMENT PANEL AND REPLACE, SEE SHEET NO. II FOR DETAILS. CURB & GUTTER TO REMAIN INPLACE.
- (B) ADJUST MANHOLE TO PROPER ELEVATION. DETERMINED BY ENGINEER IN FIELD.
- (C) EXPANSION JOINT DOWEL ASSEMBLY TO REMAIN INPLACE.
- (D) REMOVE PAVEMENT PANEL AND REPLACE, SEE SHEET NO. II FOR DETAILS. CURB & GUTTER TO REMAIN INPLACE.

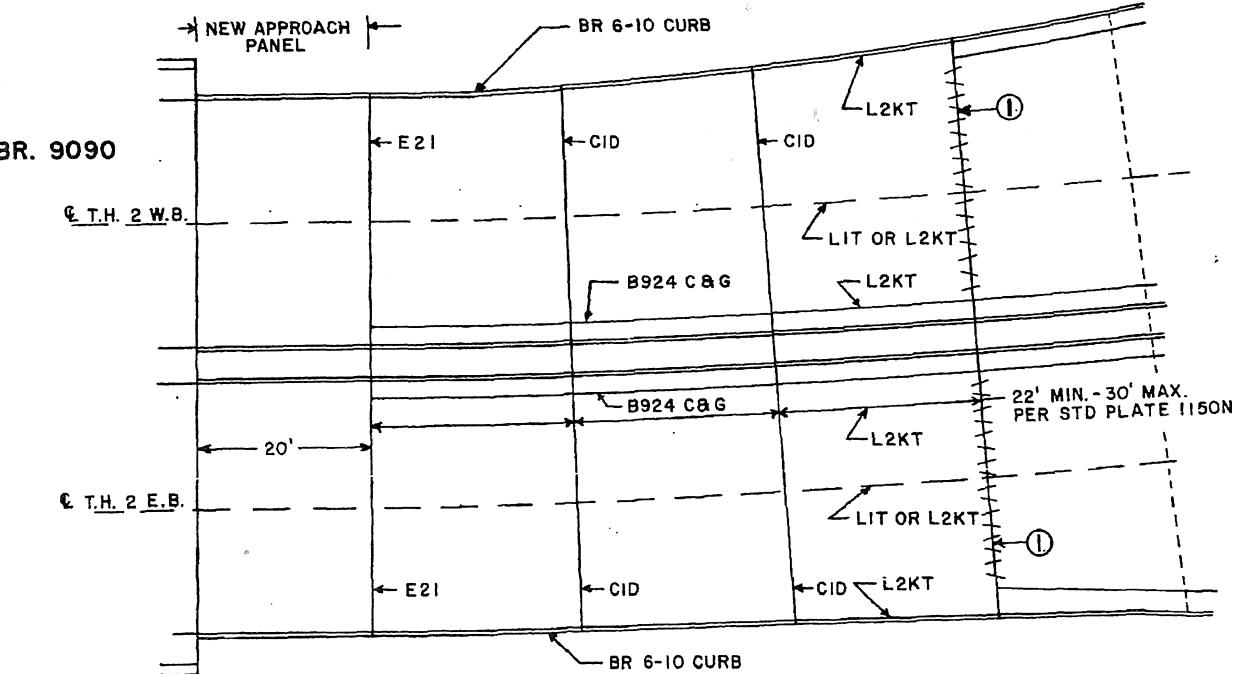


NOTE: APPROXIMATELY 42 CU. YDS. CONC. MIX 3U17A REQ'D FOR BOTH ROADWAYS
SAW CUT AND SEAL (SPEC. 3723) OVERLAY OVER EXISTING JOINTS
APPROXIMATELY 35 CU.YDS. LATEX IF LATEX OPTION IS USED

① RECONSTRUCT PAVEMENT JOINT



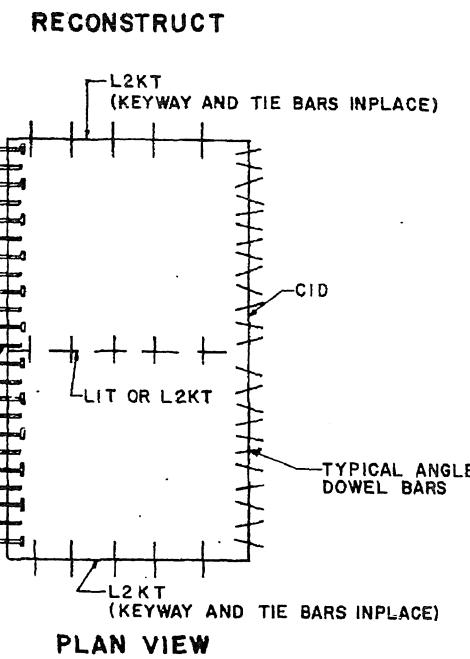
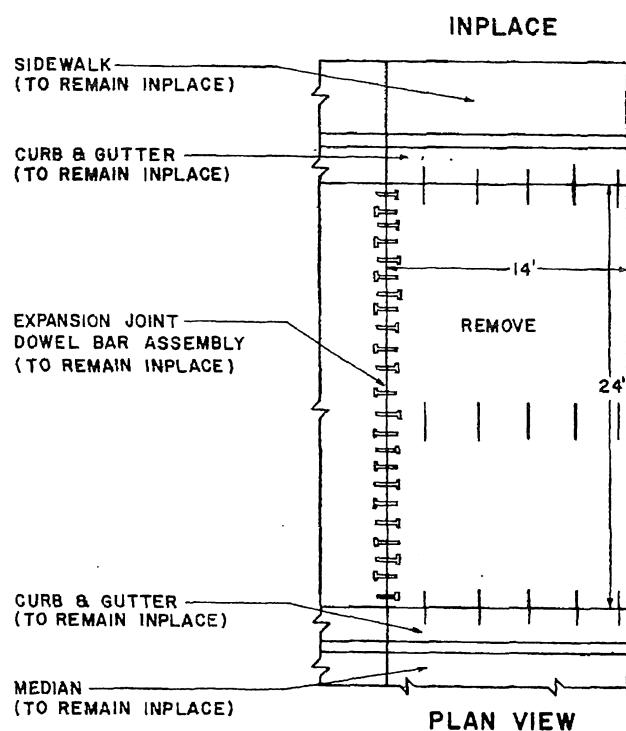
NOTE: RECONSTRUCT PAVEMENT JOINT INCLUDES THE FOLLOWING ITEMS (EXACT LOCATION TO BE DETERMINED BY ENGINEER IN THE FIELD)
 1. SAW CUT-PARTIAL DEPTH
 2. DRILLED AND GROUTED NO. 6 BARS, 4' LONG
 3. APPROVED EPOXY GROUT MIXTURE
 4. 1' MAXIMUM Ø HOLES DRILLED FOR NO. 6 DOWEL BARS
 5. DOWEL BARS ANGLED 20°± FROM NORMAL



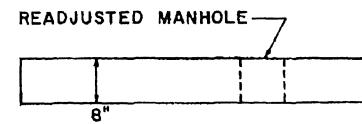
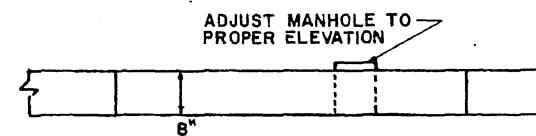
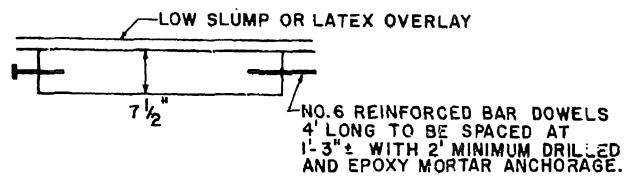
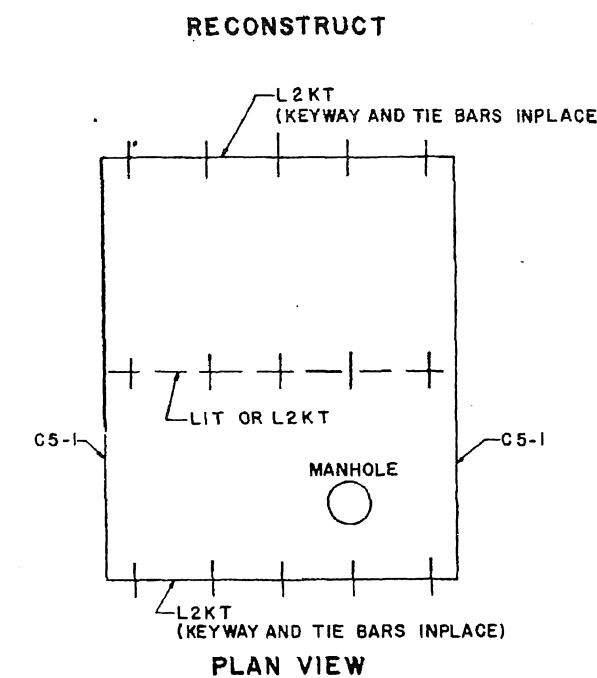
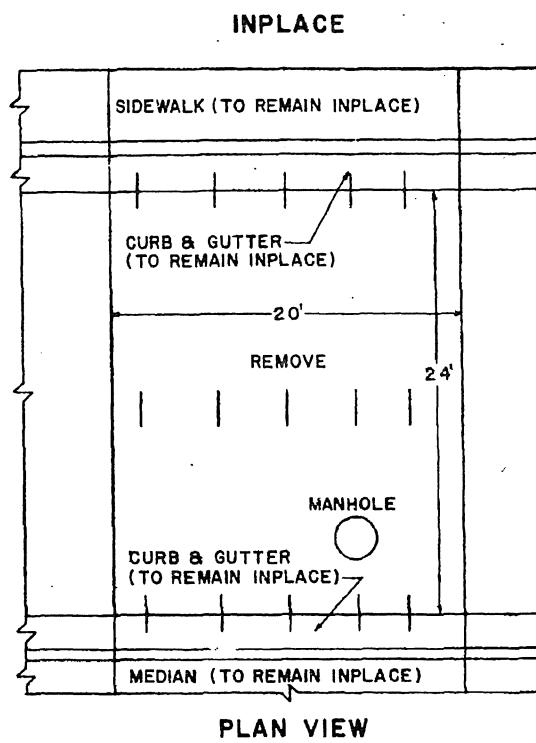
NOTE: THE FOLLOWING PAVEMENT CONSTRUCTION JOINTS AND ITEMS ARE INCIDENTAL TO CONCRETE PAVEMENT:
 1. ① RECONSTRUCT PAVEMENT JOINT
 2. LIT
 3. L2KT
 4. CID
 5. ALL PAVEMENT SECTIONS TO BE 10" THICK
 6. E41
 7. L3
 8. C4

TITLE: APPROACHES	DES:	DR:	APPROVED:	1-26-84	Bridge No.
	CHK:	CHK:			9090

PAVEMENT PANEL NEXT TO BRIDGE APPROACH PANEL
WEST BOUND ROADWAY, WEST END OF BRIDGE



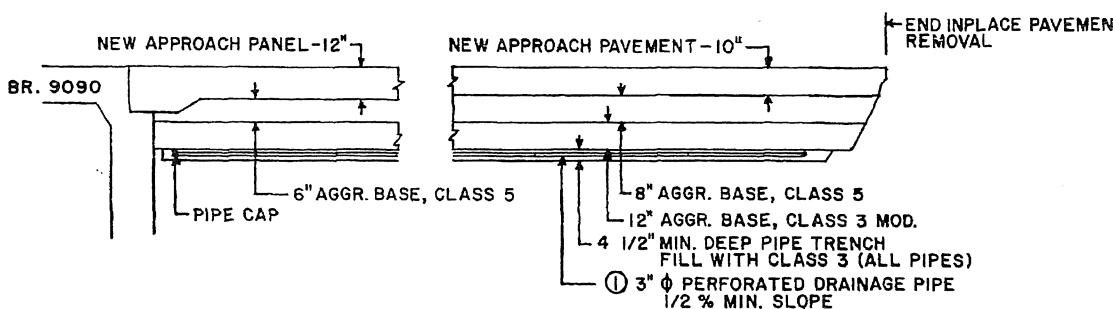
6TH PAVEMENT PANEL FROM THE BRIDGE APPROACH PANEL
WEST BOUND ROADWAY, WEST END OF BRIDGE



NOTE: THE FOLLOWING PAVEMENT CONSTRUCTION JOINTS AND ITEMS ARE INCIDENTAL TO CONCRETE PAVEMENT:
 1. LIT
 2. L2KT
 3. CID
 4. ALL PAVEMENT SECTIONS TO BE 8" THICK
 5. RECONSTRUCT EXPANSION JOINT E2D-1

- CONSTRUCTION NOTES:**
- ① DOWEL BARS TIEING CURB AND GUTTER TO PAVEMENT TO REMAIN INPLACE.
 - ② FREE ENDS ON DOWEL BAR ASSEMBLIES WILL REQUIRE TO BE COVERED WITH GREASE.
 - ③ 1" MAXIMUM Ø HOLES DRILLED FOR NO. 6 BARS.
 - ④ NO. 6 DOWEL BARS ARE TO BE ANGLED 20°± FROM NORMAL.
 - ⑤ APPROXIMATELY 20 CU.YDS. OF CONCRETE MIX 3A4I IS REQUIRED.

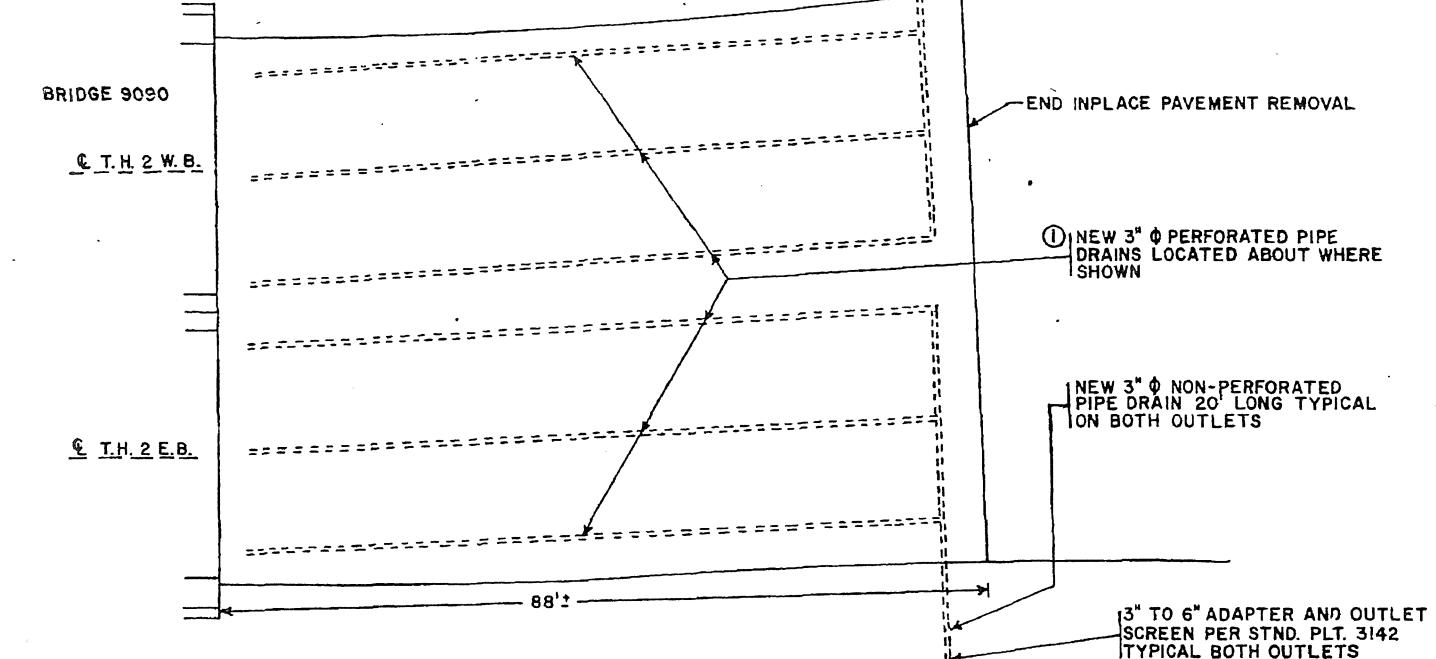
LONGITUDINAL SECTION OF EAST APPROACH
DRAINAGE SYSTEM



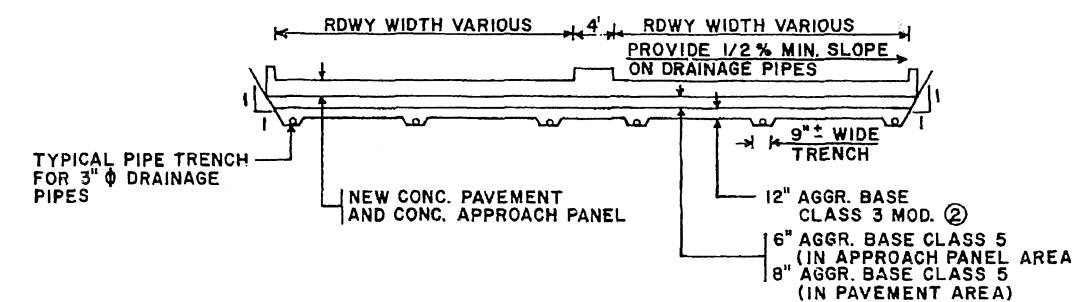
(3) SUMMARY OF QUANTITIES FOR DRAINAGE SYSTEM	
3" Ø PERFORATED PIPE DRAIN (WRAPPED)	540 LIN. FT.
3" Ø NON-PERFORATED PIPE DRAIN	40 LIN. FT.
3" PIPE ELBOWS	2 REQ'D
3" PIPE TEES	4 REQ'D
3" PIPE CAPS	6 REQ'D
6" OUTLET SCREENS	2 REQ'D
3" TO 6" ADAPTER	2 REQ'D

② THE SUMMARY OF QUANTITIES FOR THE "DRAINAGE SYSTEM" IS AS SHOWN. ANY ADDITIONAL MINOR ITEMS AND SLIGHT CHANGES OF QUANTITIES REQUIRED SHALL BE FURNISHED BY THE CONTRACTOR WITH NO ADDITIONAL COMPENSATION.

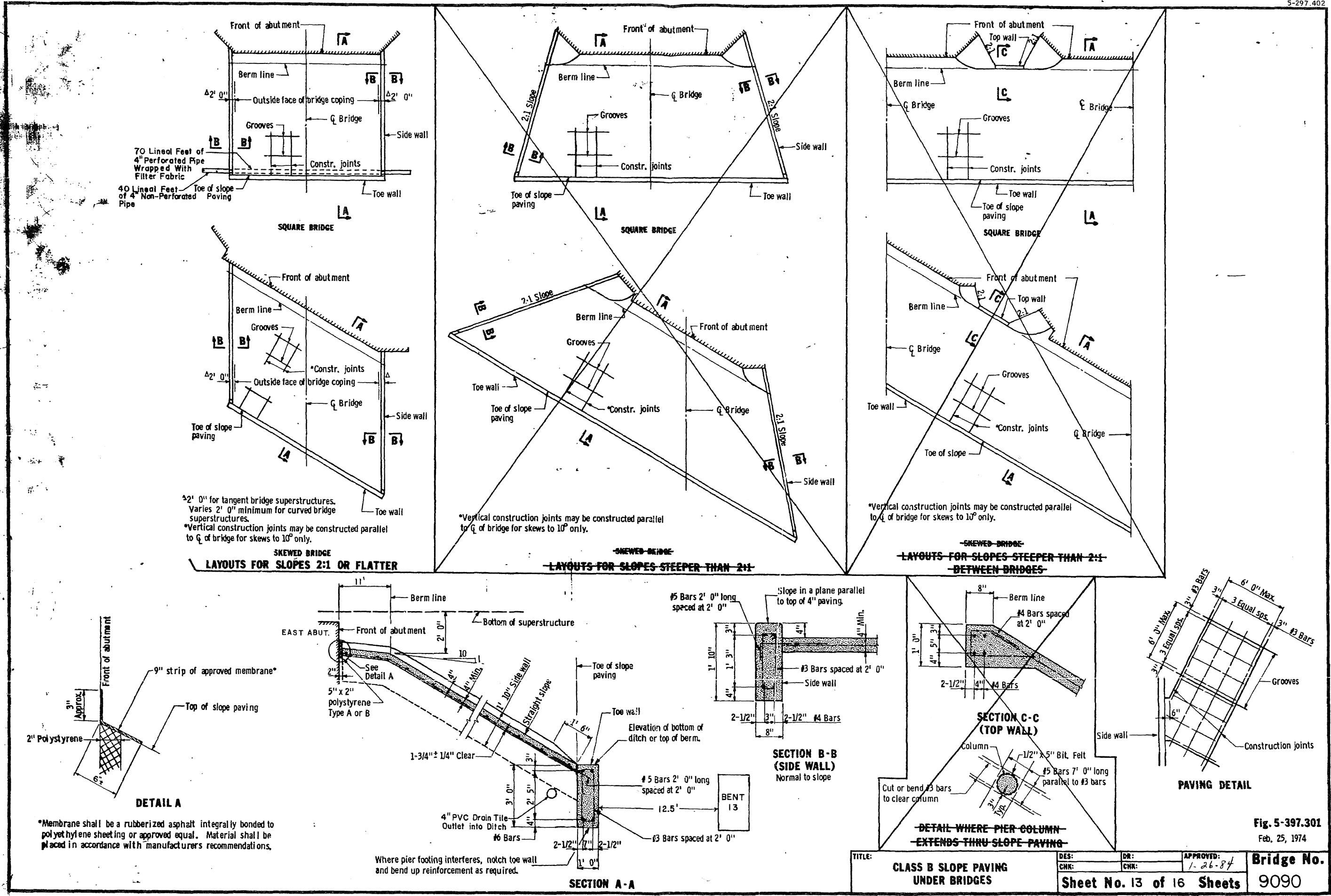
EAST APPROACH
DRAINAGE SYSTEM



TRANSVERSE SECTION OF EAST APPROACH
DRAINAGE SYSTEM



- ① PERFORATED PIPE SHALL BE WRAPPED WITH AN APPROVED WRAPPING. SEE SPECIAL PROVISIONS.
- ② ALL AGGREGATE BASE, CLASS 3, SHALL BE MODIFIED TO 0-5 % PASSING NO. 200 OR FINE FILTER AGGREGATE, SPEC. 3149.2J



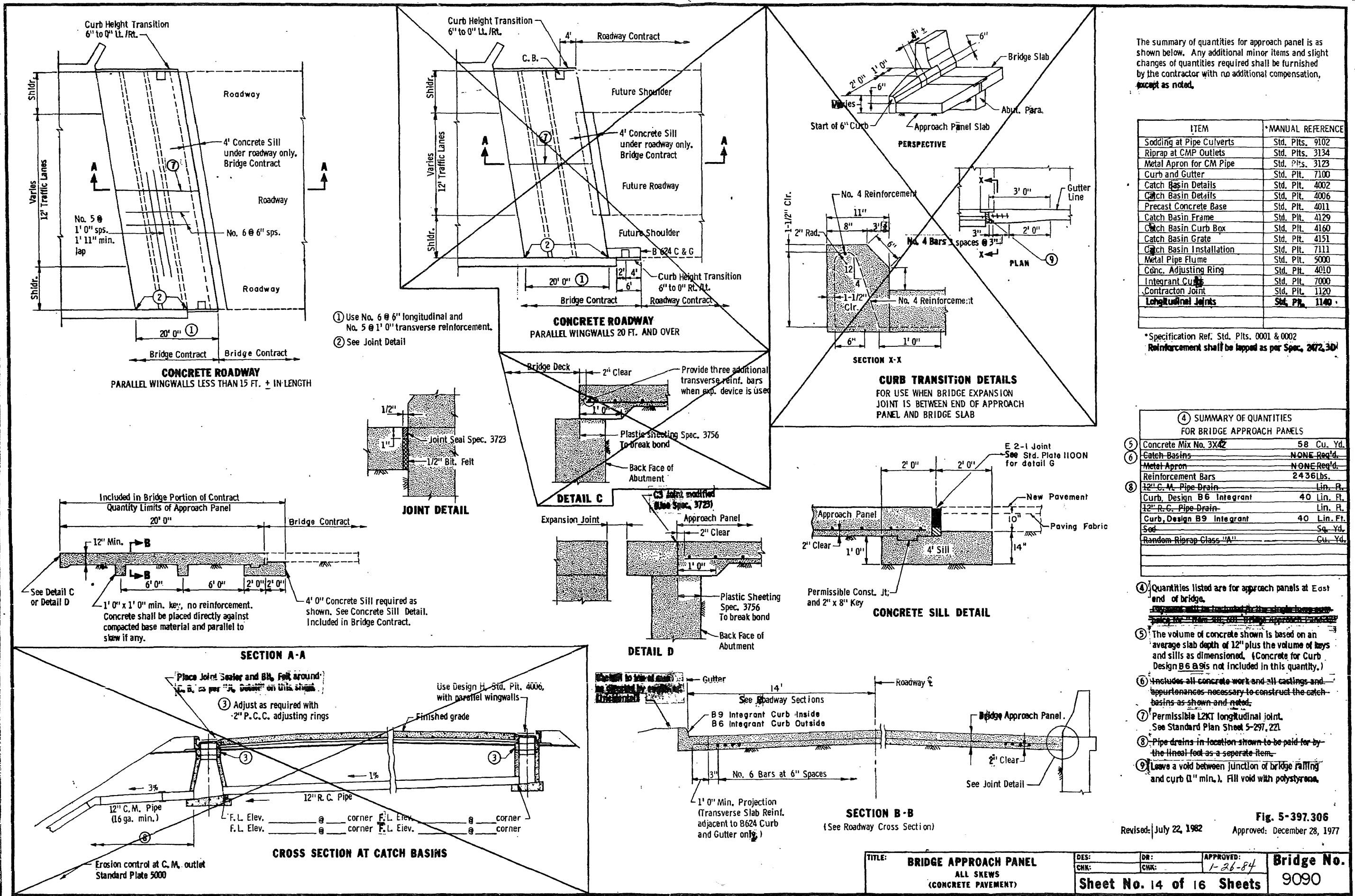
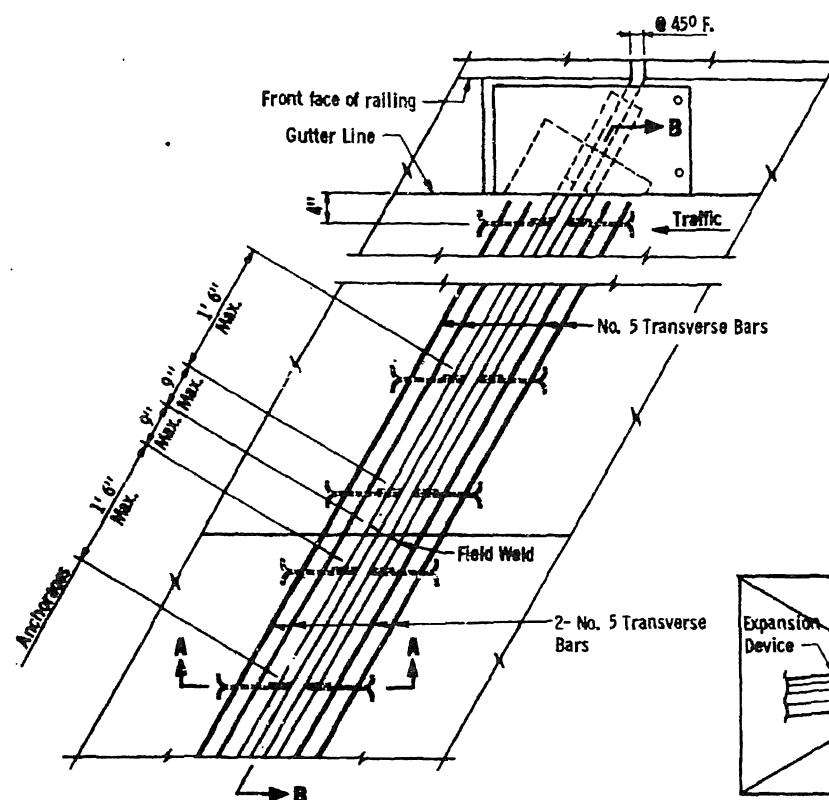


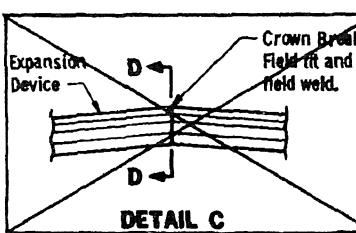
Fig. 5-397.306

Approved: December 28, 1977

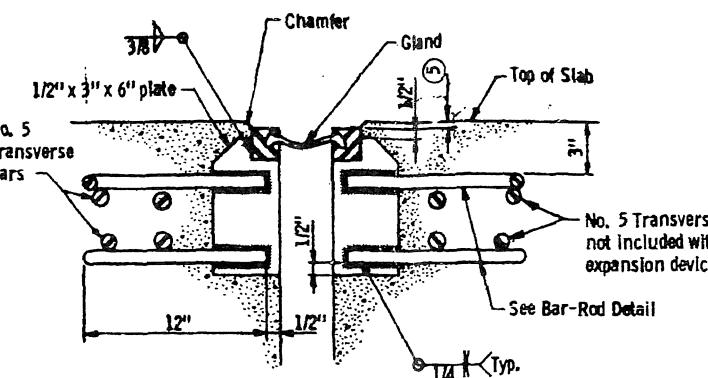
Revised: July 22, 1982



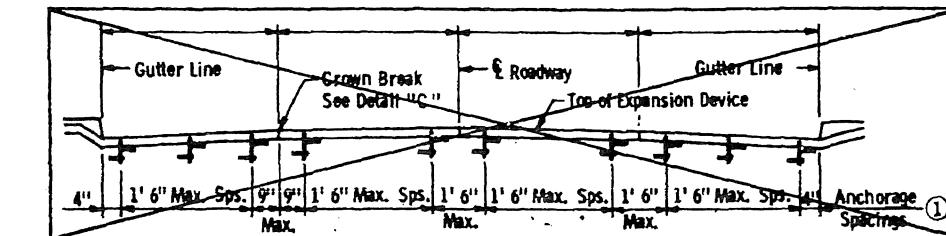
PLAN VIEW AT EXPANSION DEVICE
STRAIGHT EXPANSION DEVICE SHOWN



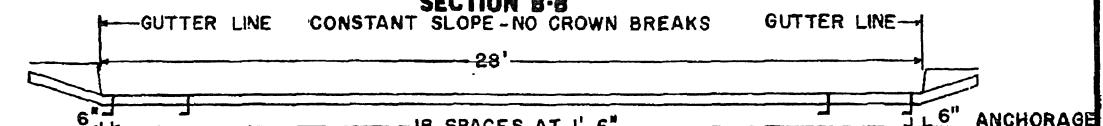
SECTION A-A
ANCHORAGE WITH ROD OPTION SHOW



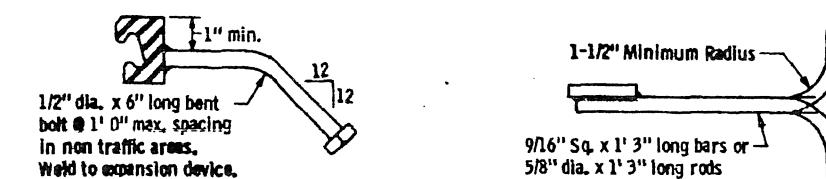
SECTION A-A



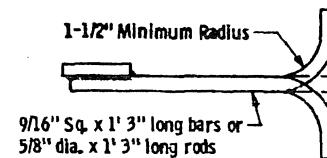
SECTION B-B



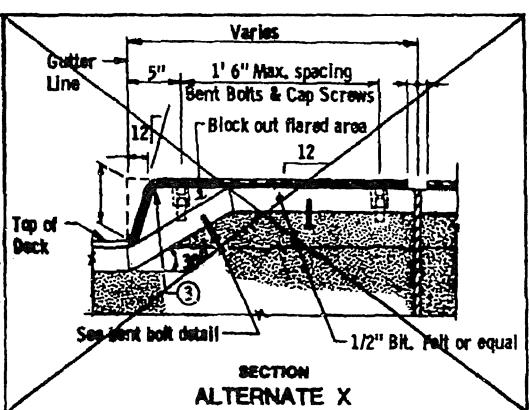
SECTION B-B
CONSTANT SLOPE - NO CROWN BREAKS



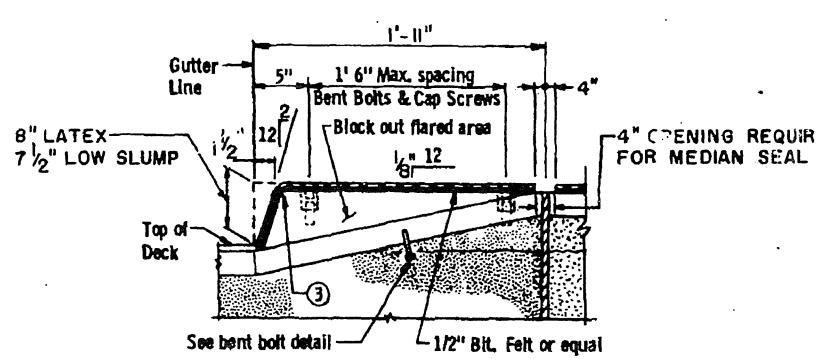
BENT BOLT DETAIL



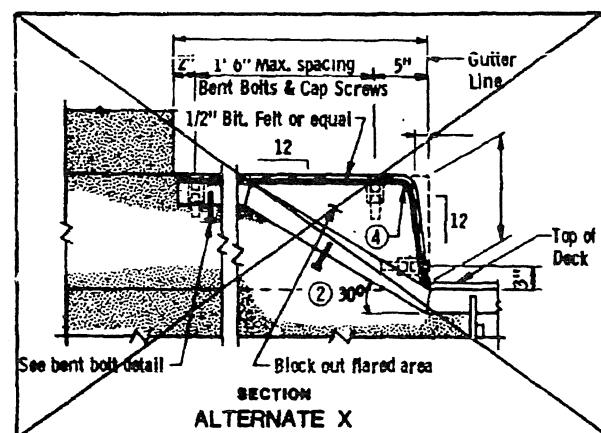
BAR-ROD DETAIL



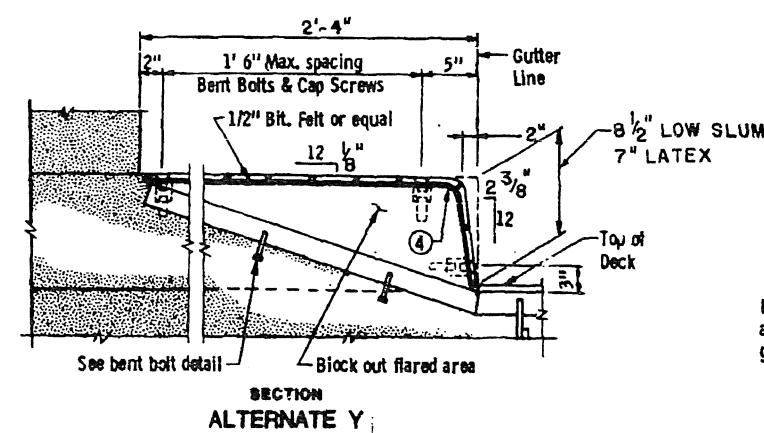
SECTION
ALTERNATE X



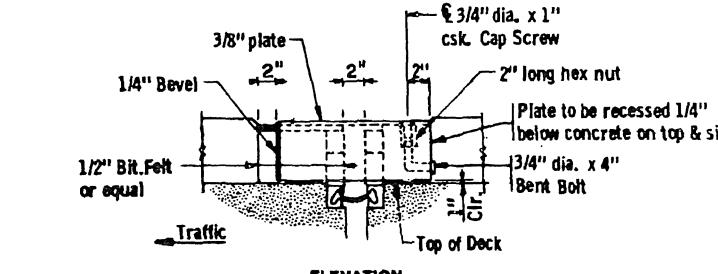
USED MEDIUM DETAN S



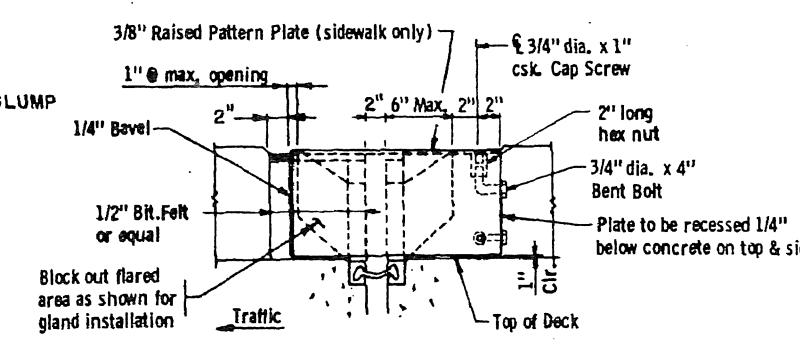
**SECTION
ALTERNATE X**



SIDEWALK DETAIL



ELEVATION



INSIDE ELEVATION

- ① Dimension along centerline of joint.
 - ② For roadway skewes over 25° use 45° .
 - ③ 1" outside radius of steel plate
 - ④ 1" outside radius of steel plate
 - ⑤ 1/2" (5/8" max.) when Snowplow Fingers are used.
1/8" (1/4" max.) when Snowplow Fingers are
not used.

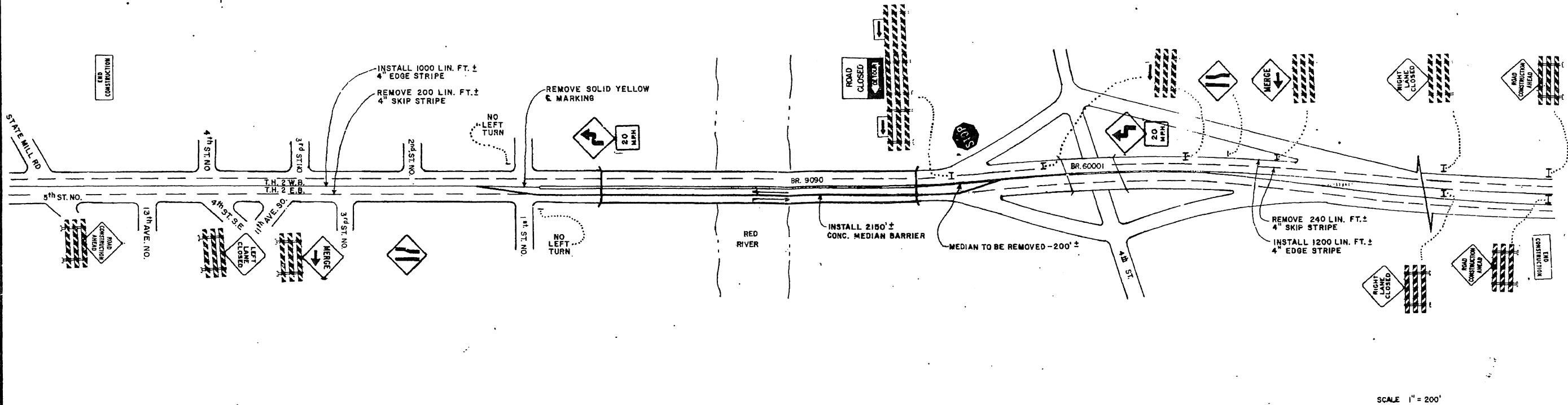
FIG. 5-397 631

Revised: January 20, 1983 Approved: July 16, 1982

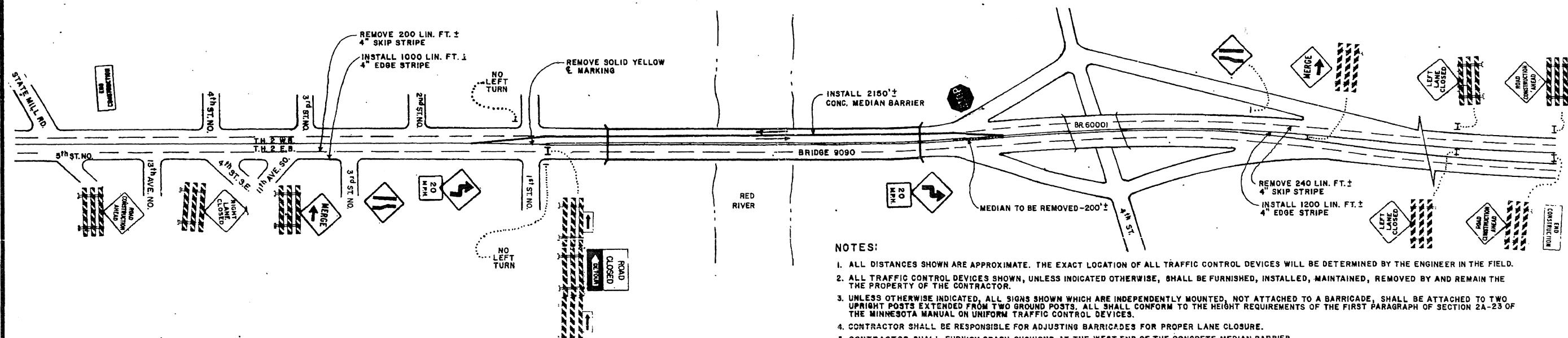
**WATERPROOF EXPANSION DEVICE
FOR REPAIR WORK
WITH SIDEWALK OR RAISED MEDIAN**

Revised: January 20, 1983		Approved: July 10, 1988
DES:	DR:	APPROVED:
CHK:	CHK:	1-26-87
Sheet No. 15 of 16 Sheets		Bridge No. 9090

STAGE CONSTRUCTION
WESTBOUND ROADWAY CLOSED



STAGE CONSTRUCTION
EASTBOUND ROADWAY CLOSED



NOTES:

1. ALL DISTANCES SHOWN ARE APPROXIMATE. THE EXACT LOCATION OF ALL TRAFFIC CONTROL DEVICES WILL BE DETERMINED BY THE ENGINEER IN THE FIELD.
2. ALL TRAFFIC CONTROL DEVICES SHOWN, UNLESS INDICATED OTHERWISE, SHALL BE FURNISHED, INSTALLED, MAINTAINED, REMOVED BY AND REMAIN THE PROPERTY OF THE CONTRACTOR.
3. UNLESS OTHERWISE INDICATED, ALL SIGNS SHOWN WHICH ARE INDEPENDENTLY MOUNTED, NOT ATTACHED TO A BARRICADE, SHALL BE ATTACHED TO TWO UPRIGHT POSTS EXTENDED FROM TWO GROUND POSTS. ALL SHALL CONFORM TO THE HEIGHT REQUIREMENTS OF THE FIRST PARAGRAPH OF SECTION 2A-23 OF THE MINNESOTA MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES.
4. CONTRACTOR SHALL BE RESPONSIBLE FOR ADJUSTING BARRICADES FOR PROPER LANE CLOSURE.
5. CONTRACTOR SHALL FURNISH CRASH CUSHIONS AT THE WEST END OF THE CONCRETE MEDIAN BARRIER.
6. INSTALL TYPE "B" HIGH INTENSITY FLASHING WARNING LIGHTS ON "ROAD CONSTRUCTION AHEAD" BARRICADES. (2 ON EACH)
7. INSTALL TYPE "A" LOW INTENSITY FLASHING WARNING LIGHTS ON ALL OTHER BARRICADES. (2 ON EACH)
8. INSTALL TYPE "A" LOW INTENSITY FLASHING WARNING LIGHTS ON ALL POST MOUNTED SIGNS. (1 ON EACH)
9. INSTALL TYPE "C" STEADY BURN LIGHTS AT 100' INTERVALS ON THE CONCRETE MEDIAN BARRIER.

TITLE:
TRAFFIC CONTROL LAYOUT

DES:	DR:	APPROVED:
CHK:	CHK:	1-26-84

Bridge No. 9090

Sheet No. 16 of 16 Sheets

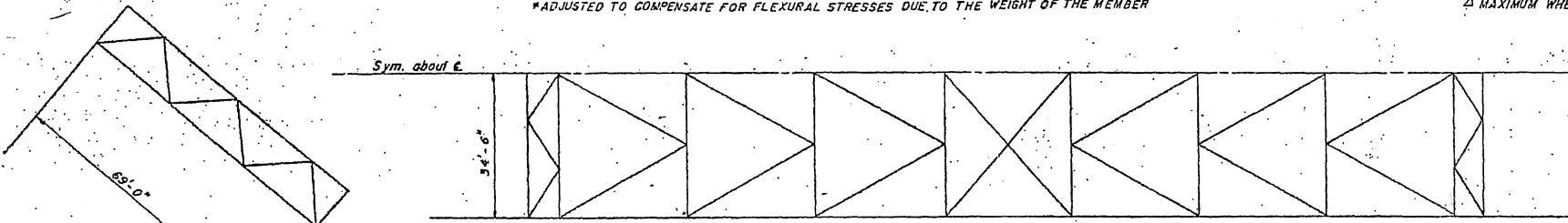
ROAD LIV. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
15	N.D.	F-708(1)		25	43

STRESSES AND SECTIONS

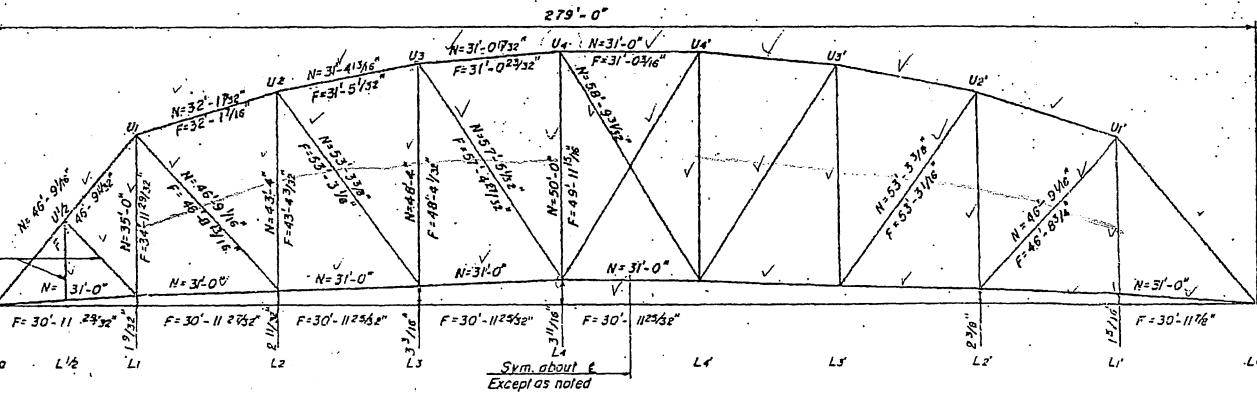
ADJUSTED TO COMPENSATE FOR FLEXURAL STRESSES DUE TO THE WEIGHT OF THE MEMBER

A MAXIMUM WHEN END BEARING MOVED TO $L/2$

⊕ ALLOWING 10% OVERSTRESS



Sym. about ϵ



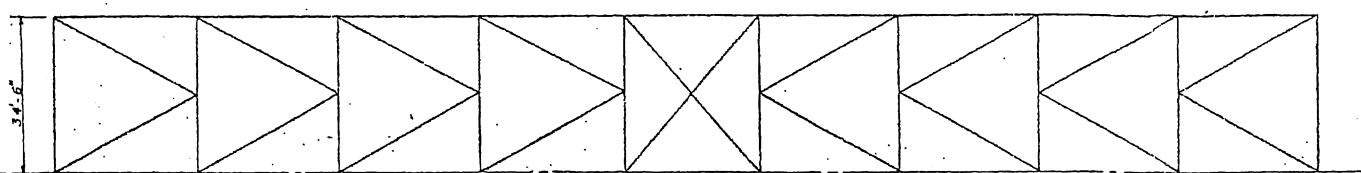
NOTE.

*Loc end of each truss shall be located on Pier No. 7.
The top figure on each truss member is its normal.*

length, with no stress and bottom chord horizontal.

The bottom figure is the adjusted length to which the member shall be fabricated, to account for dead load deflection, except that a deduction of $\frac{1}{16}$ " for draw shall be made in the center diagonals.

THESE TWO MEMBERS,
ONE END OF TRUSS ONLY



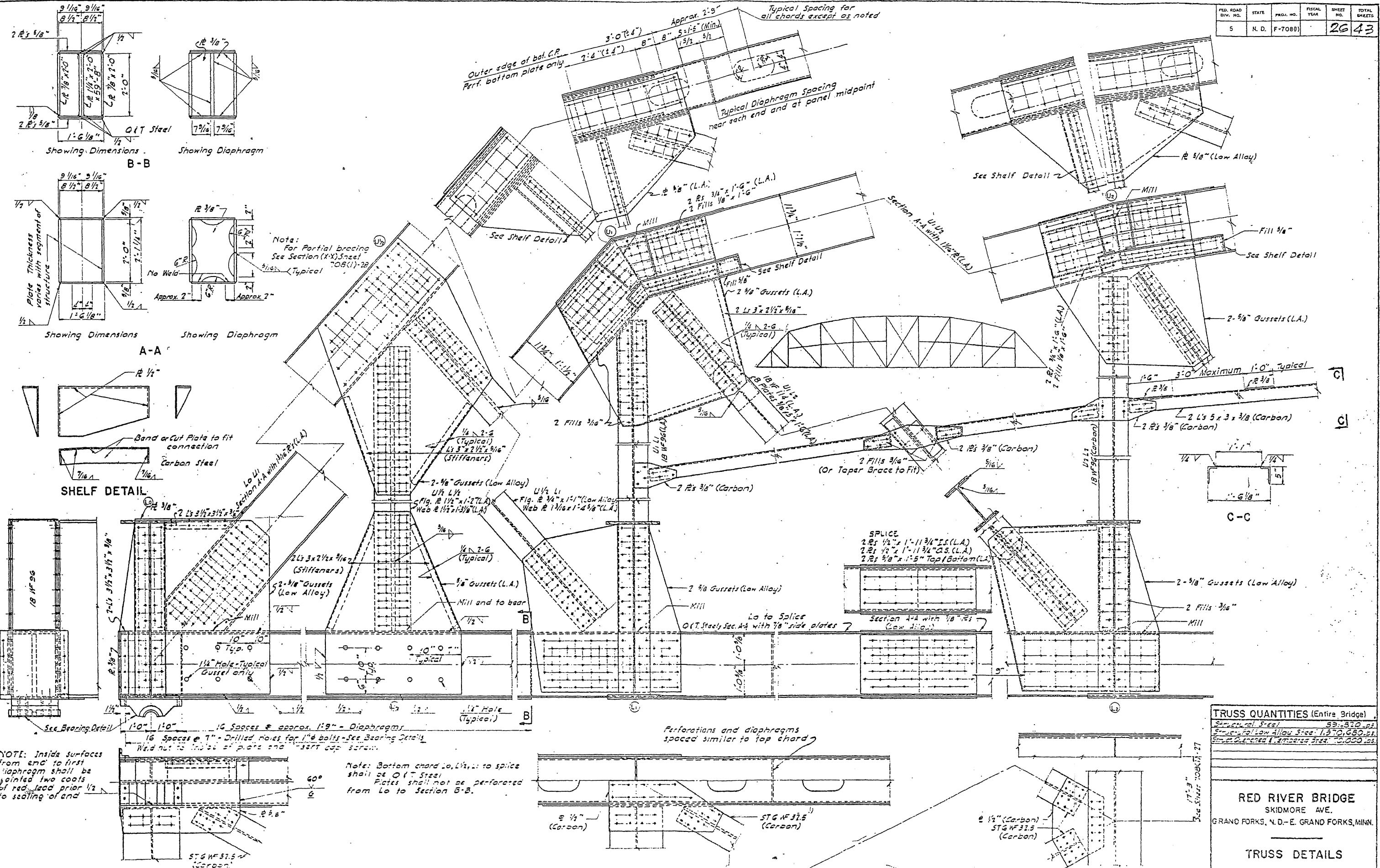
Sym. about

RED RIVER BRIDGE
SKIDMORE AVE.
GRAND FORKS, N.D.-E.GRAND FORKS, MINN.

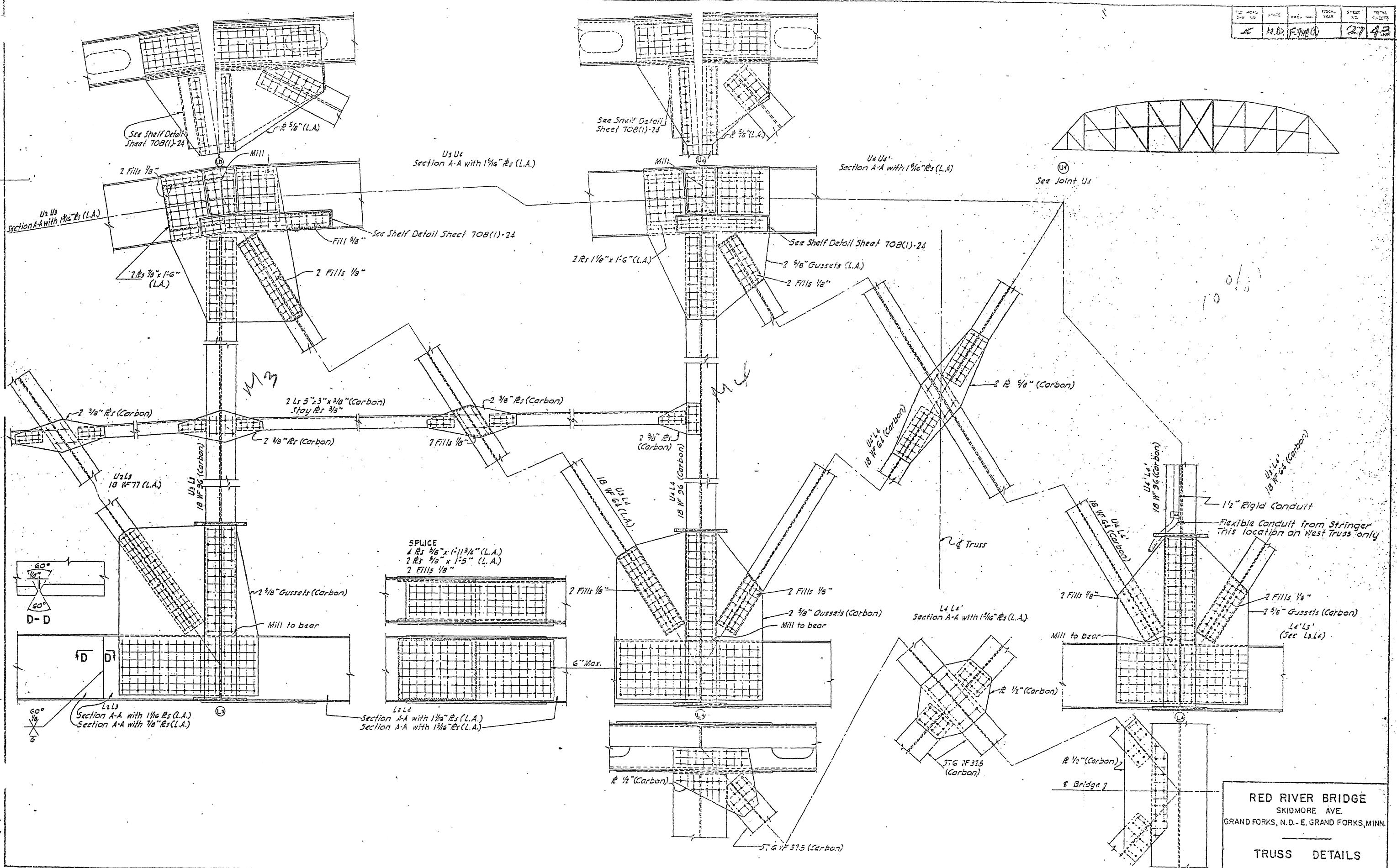
279 FT. TRUSSES

STRESSES AND CAMBER

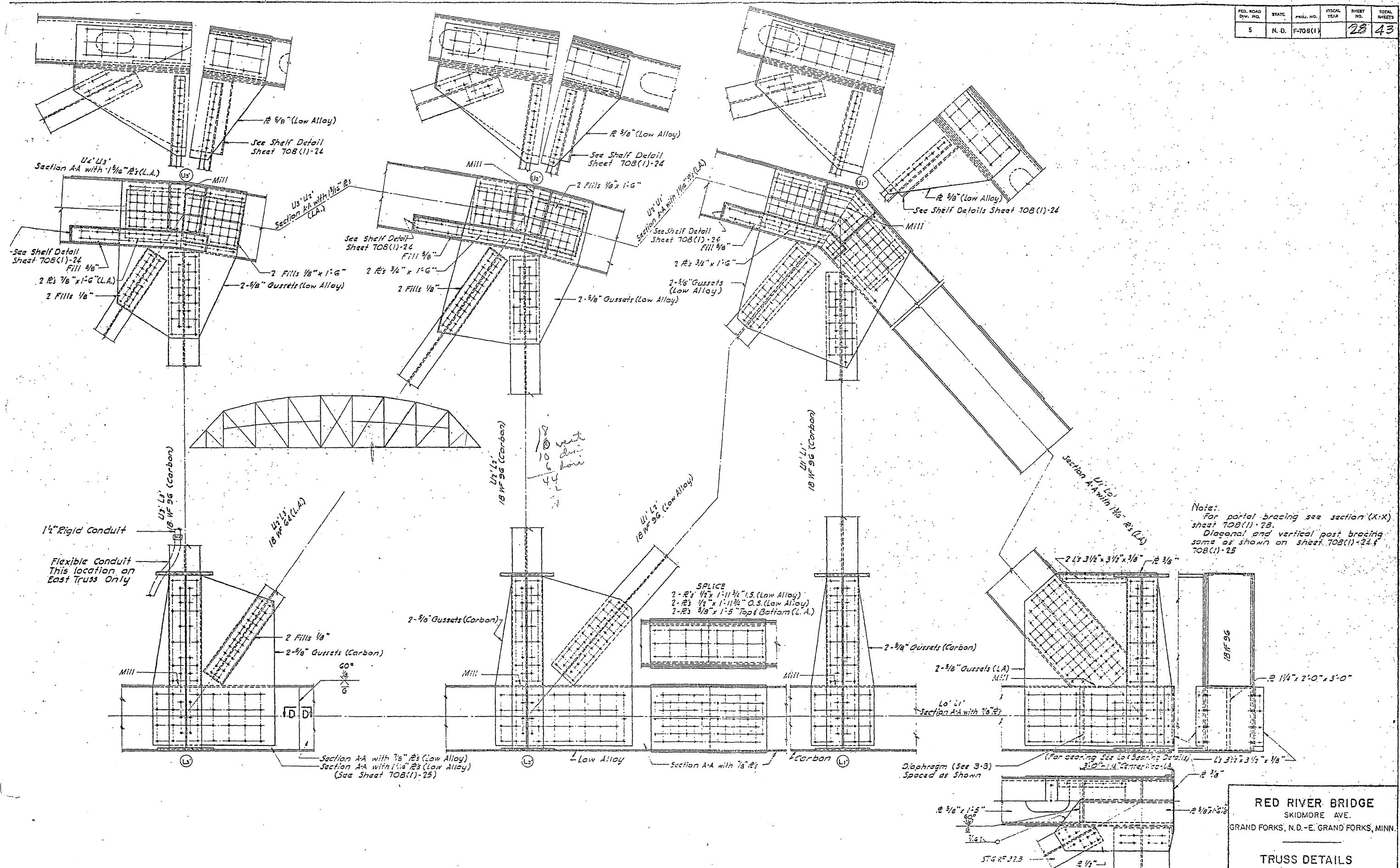
ROAD NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N. D.	F-7080)		26	43



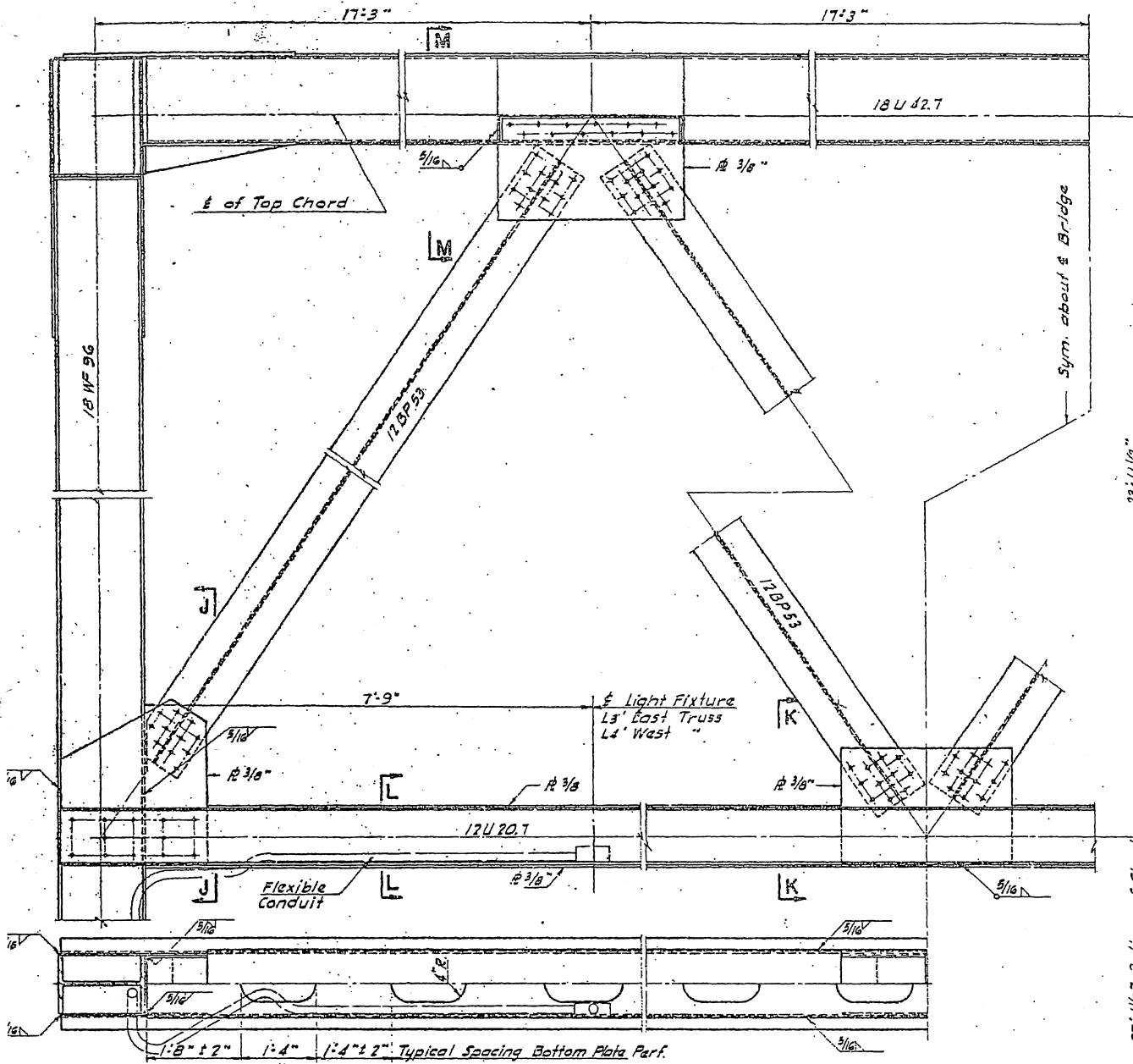
FILE NO.	SHEET NO.	STATE	WEEK NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	H.D.F-TAB				27	43



FED. ROAD DIV. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N. D.	F-708(1)		28	43

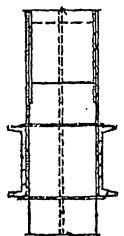


ED. ROAD CH. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N. D.	F-708(1)		29	43

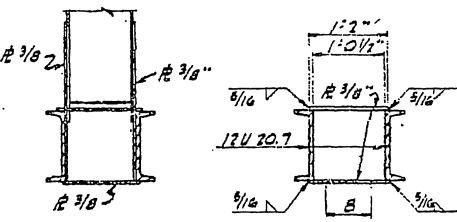


SWAY BRACING

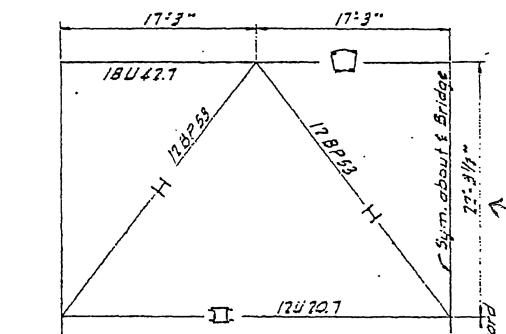
(Section @ 44-14 Shows - Connections Typical)



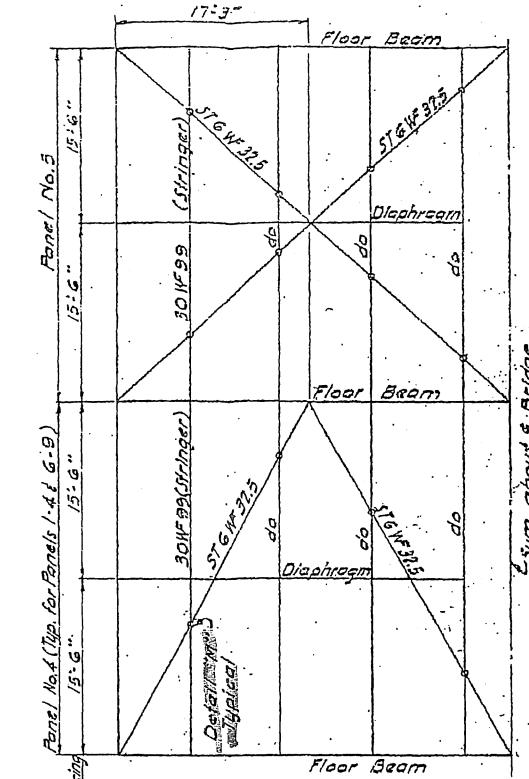
J-9



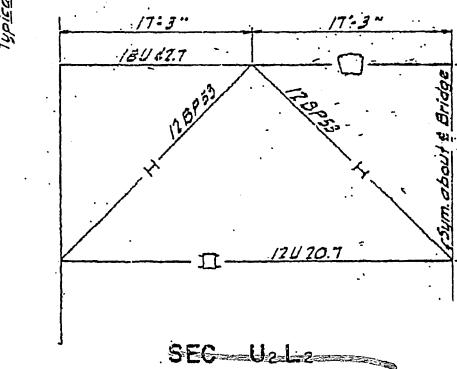
K - K



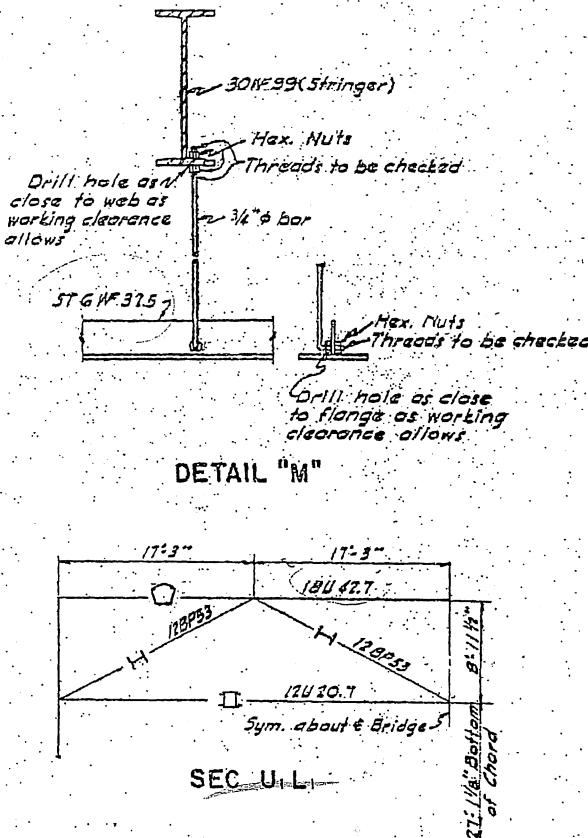
SEC. U₃L



PLAN VIEW
Showing Location of Ham
for Bottom Laterals



SEC-U₂L₂



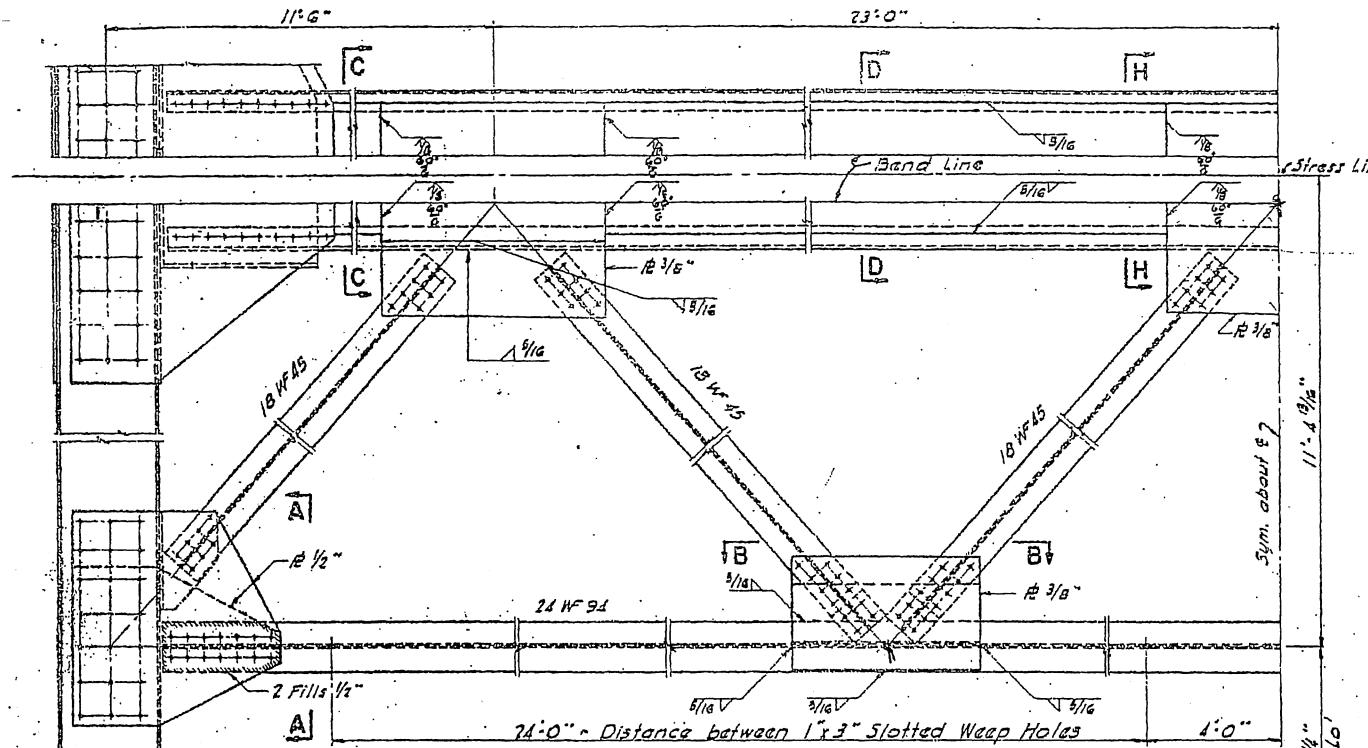
DETAIL "M"

SEC-U-L

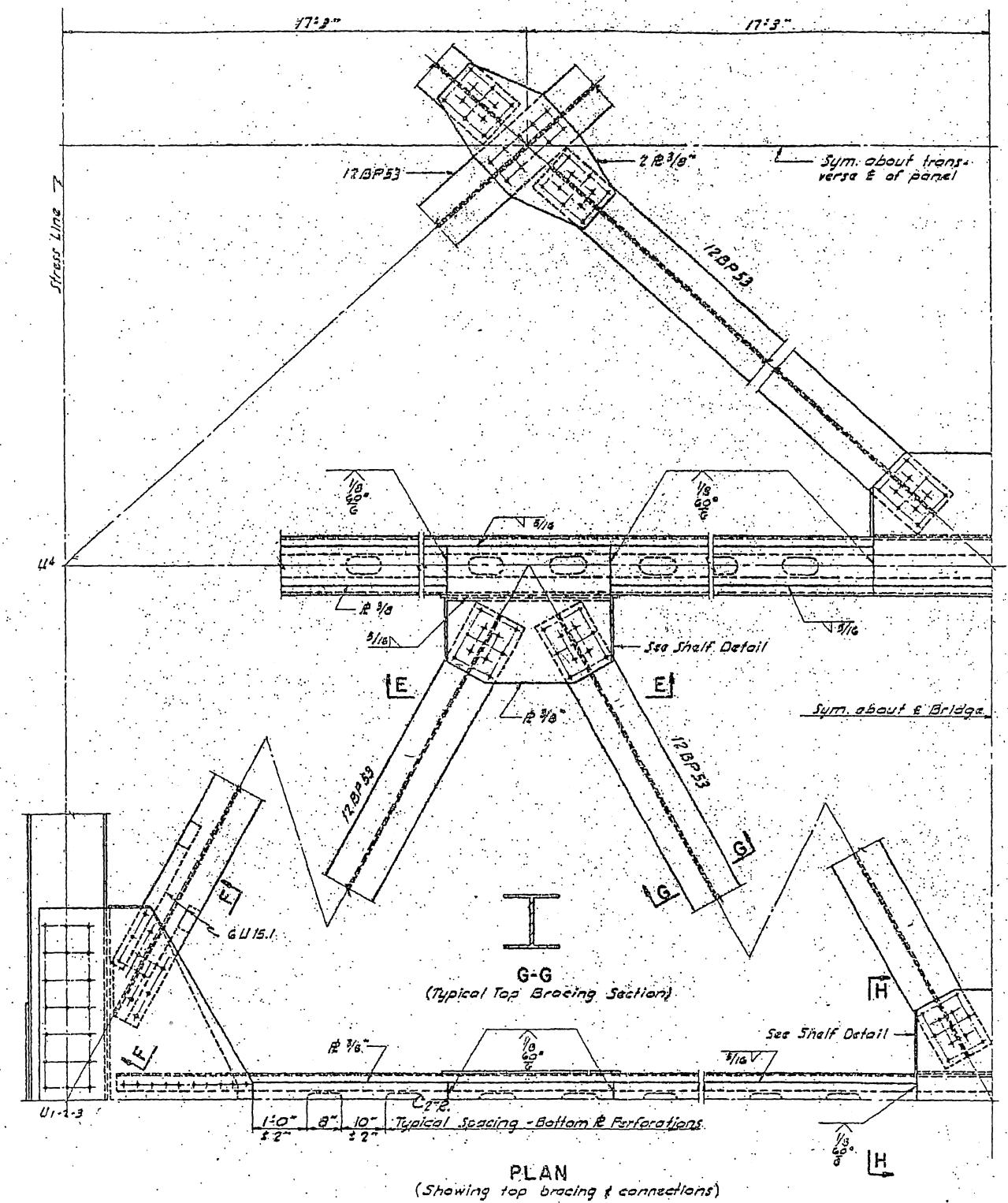
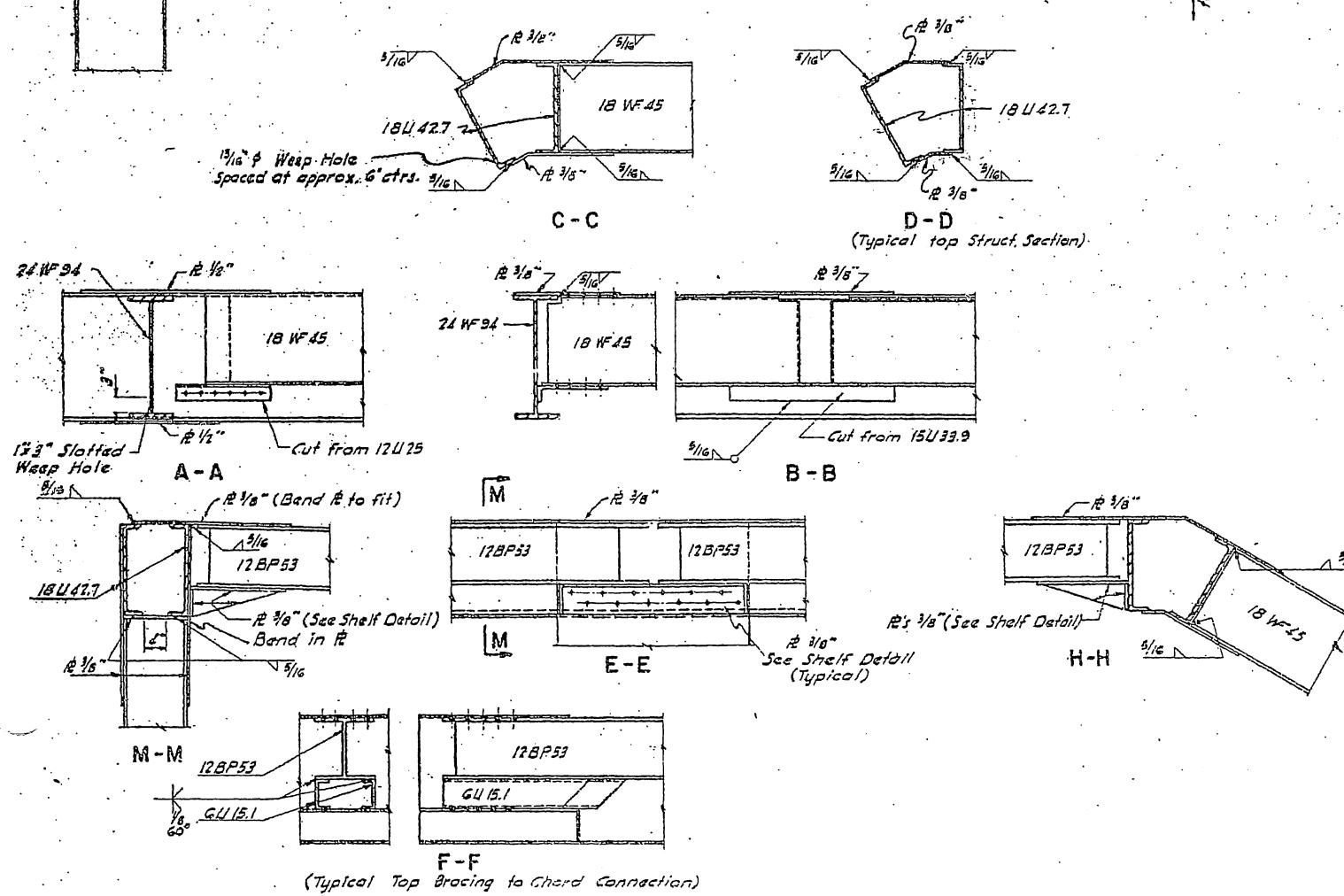
RED RIVER BRIDGE
SKIDMORE AVE.

SWAY BRACING

ROAD NO.	STATE	PHONE NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N. D.	F-708(1)		30	43



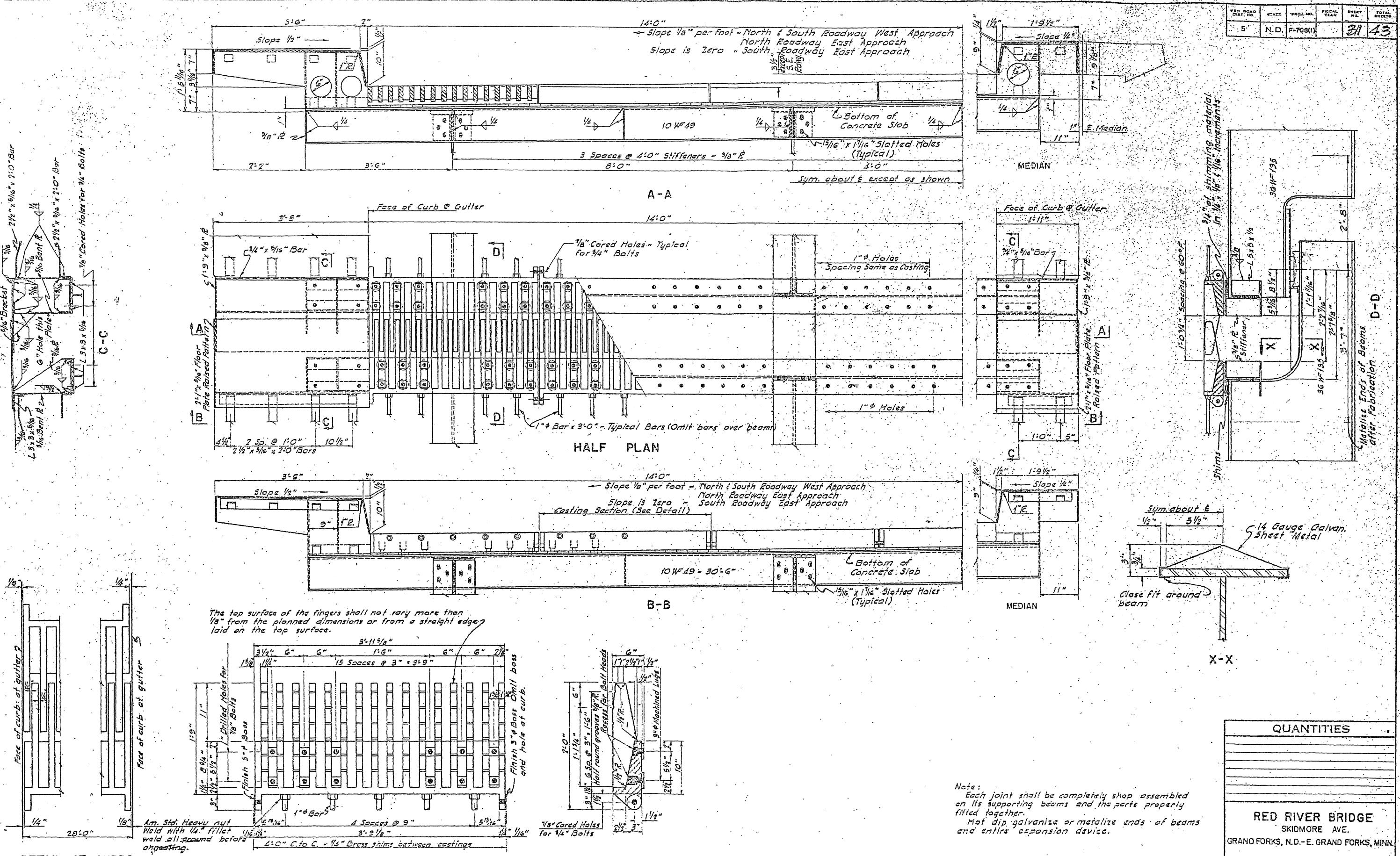
PORTAL (SEC. X-X)



PLAN
(Showing top bracing & connections)

RED RIVER BRIDGE
SKIDMORE AVE.
GRAND FORKS, N.D.-E. GRAND FORKS, MINN.

PORTAL 8
TOP LATERAL TRUSS



DETAIL AT CURBS

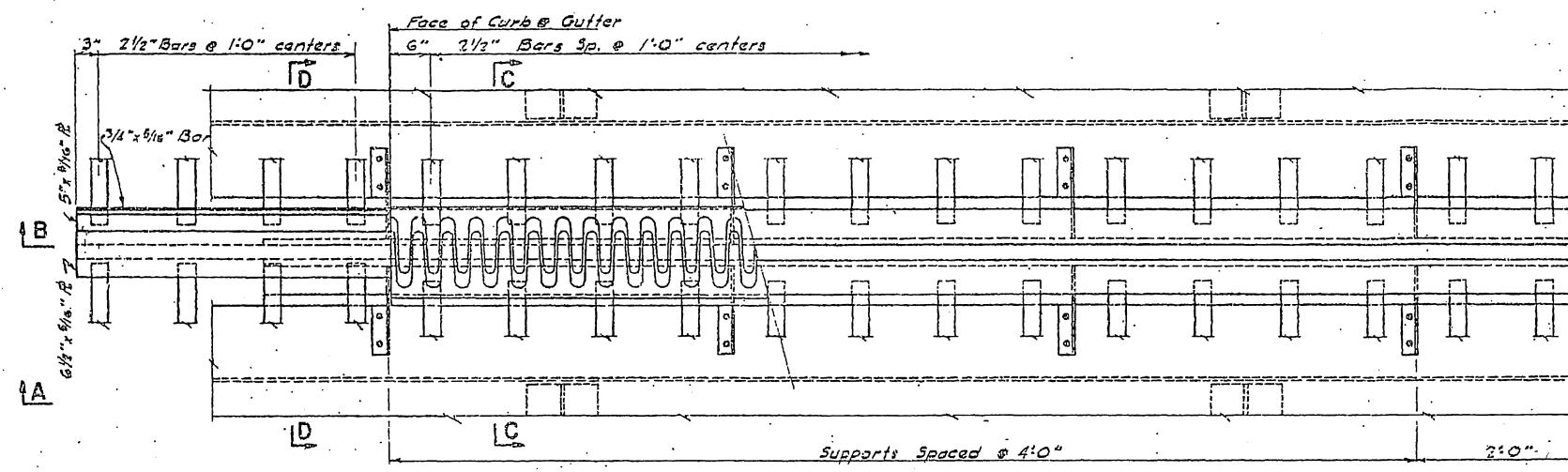
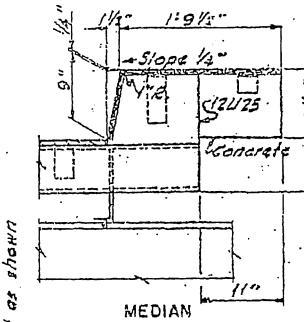
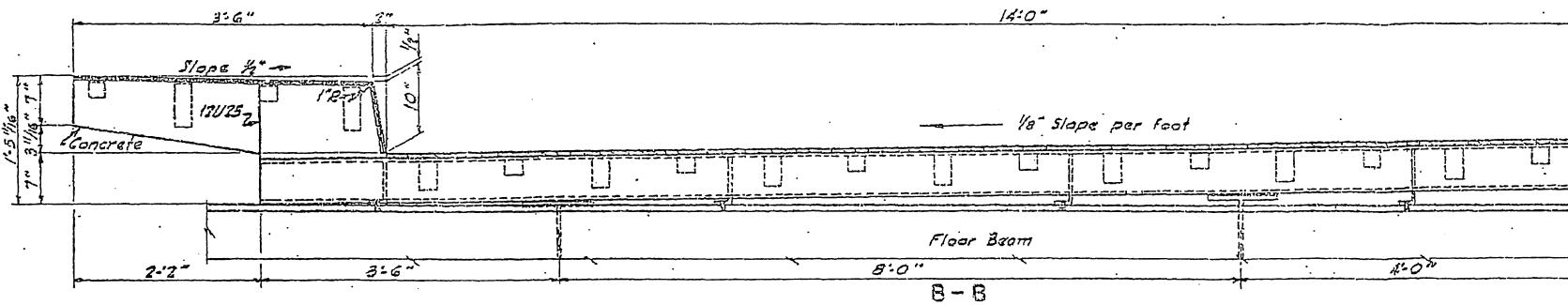
DETAIL OF STEEL CASTING

Note:
Each joint shall be completely shop assembled
on its supporting beams and the parts properly
fitted together.
Hot dip galvanize or metalize ends of beams
and entire expansion device.

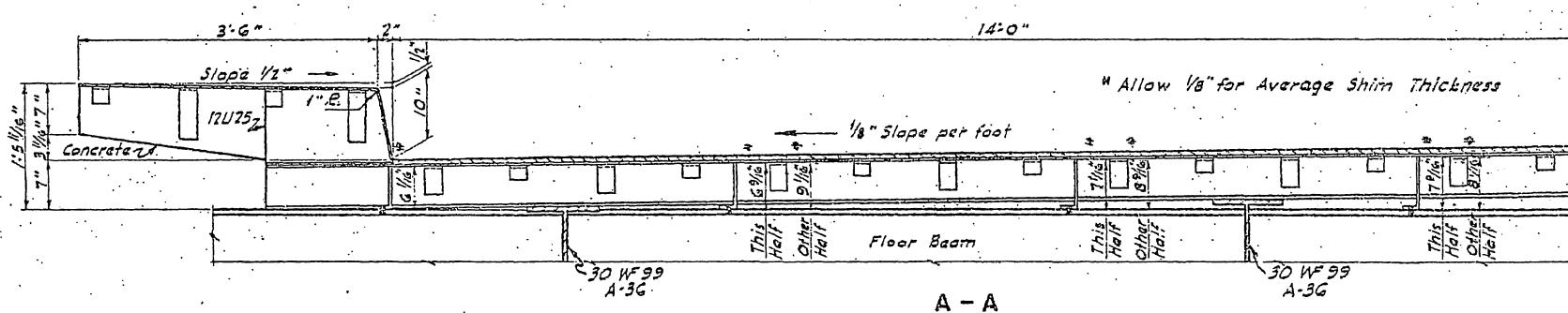
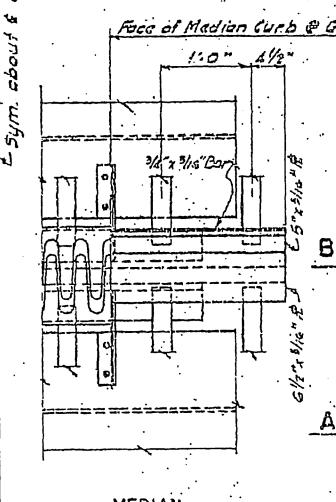
RED RIVER BRIDGE
SKIDMORE AVE.
GRAND FORKS, N.D.-E. GRAND FORKS, MINN.

EXPANSION DEVICE

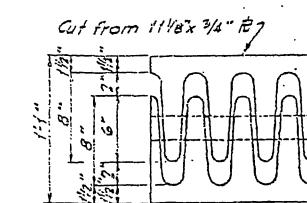
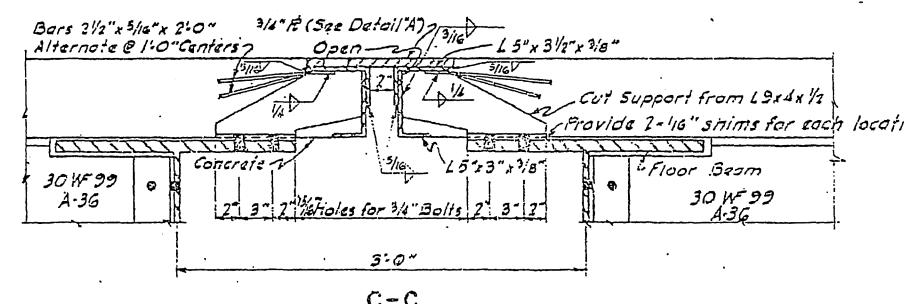
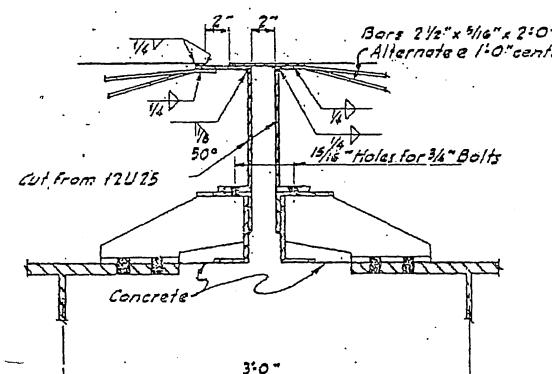
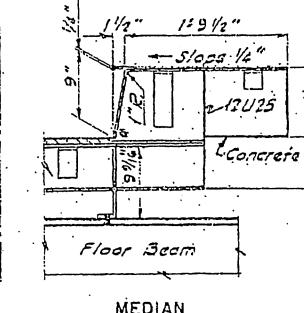
ROAD ST. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N.D.	P-708(U)		32	43



HALF PLAN



A - A



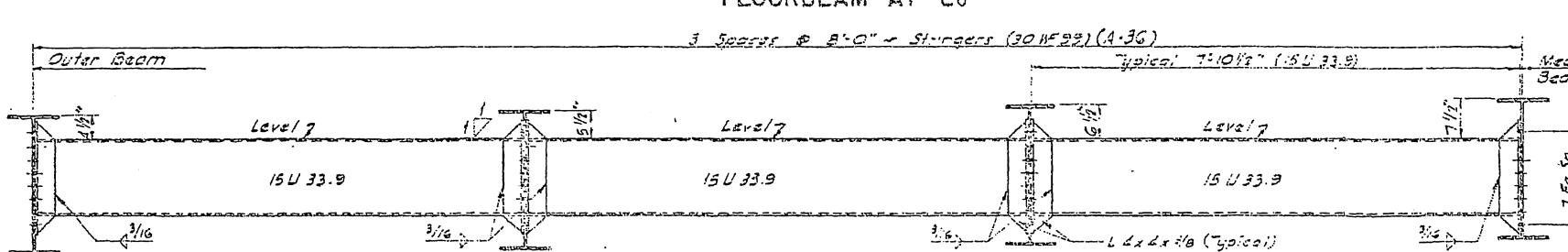
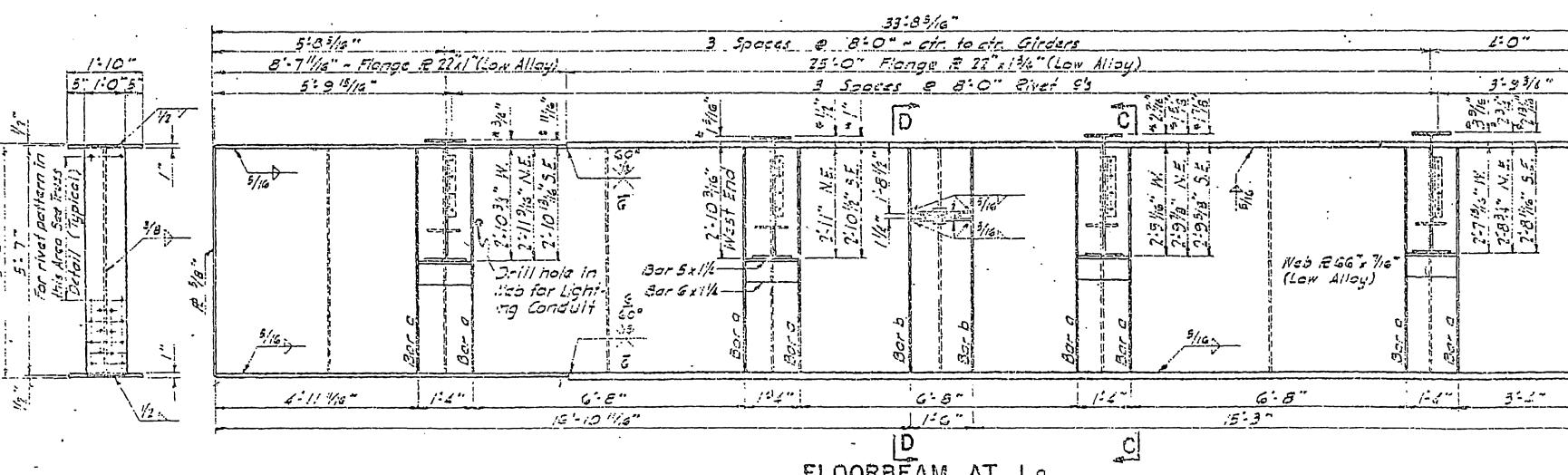
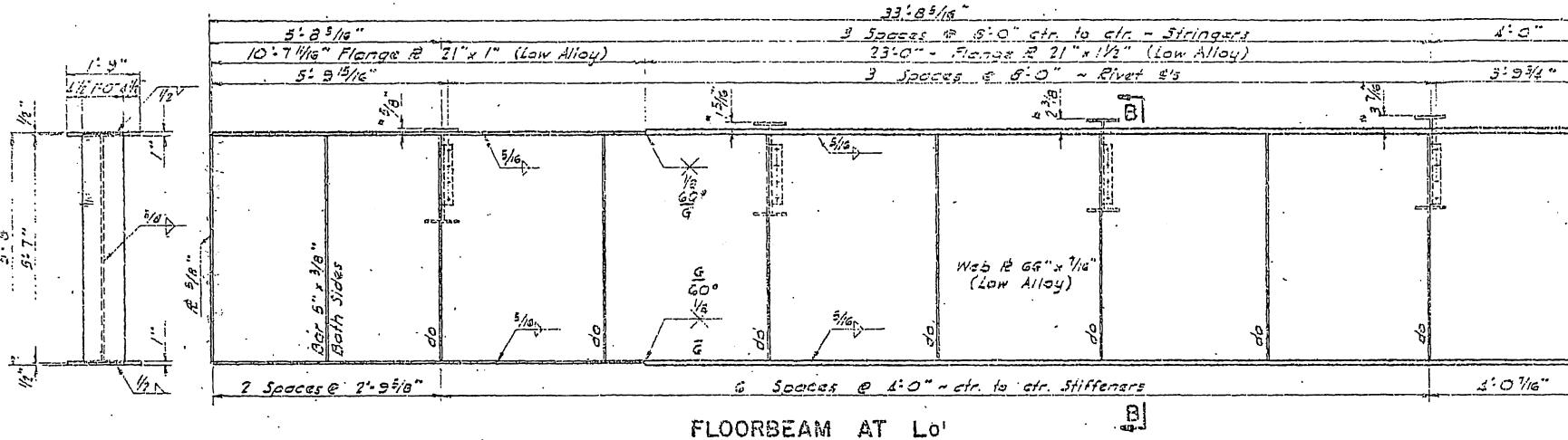
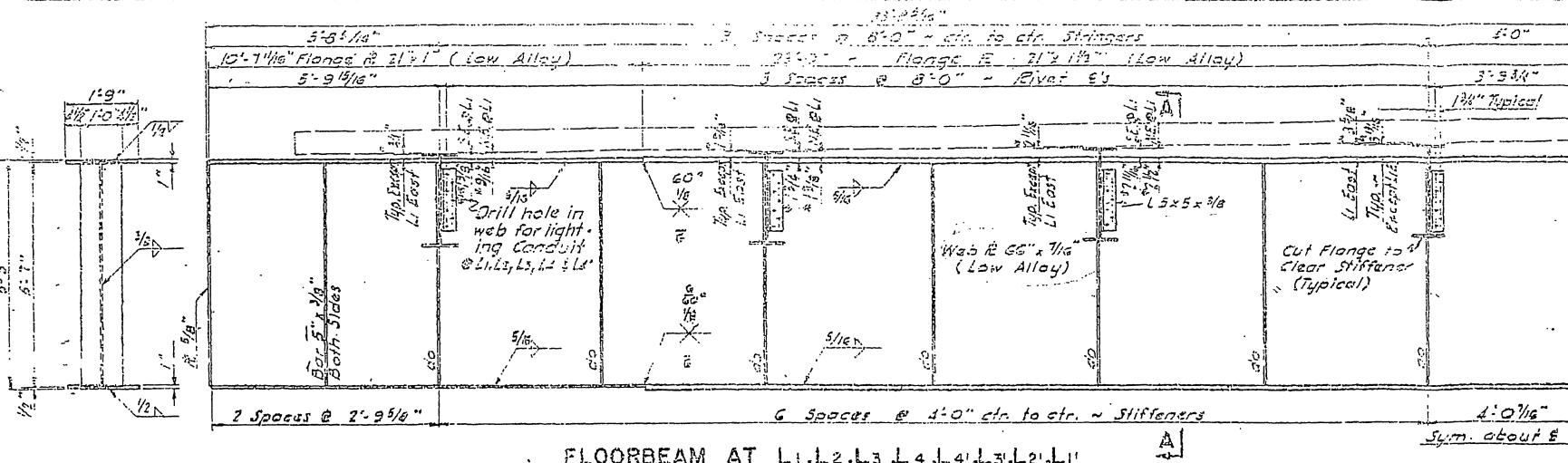
DETAIL "A"

•
QUANTITIES
•

RED RIVER BRIDGE
SKIDMORE AVE.
GRAND FORKS, N.D.-E GRAND FORKS, MINN.

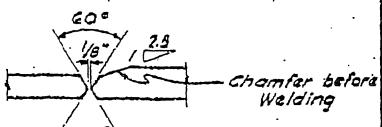
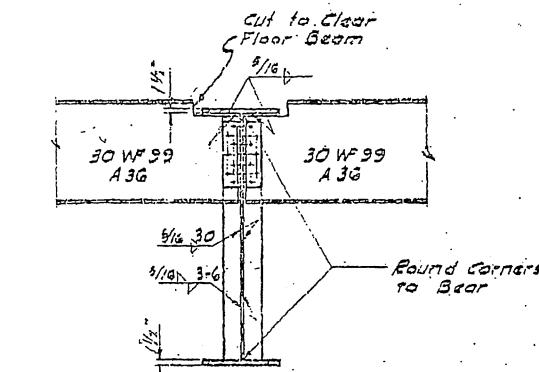
SLAB JOINT AT
PIER #7

PROJ. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
5	N. D.	F-708(1)		32	43

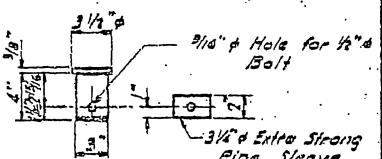


TRUSS FLOOR SYSTEM
Section Showing Diaphragms Spaced @ Mid Panel - See Plan View Sheet 7030-1

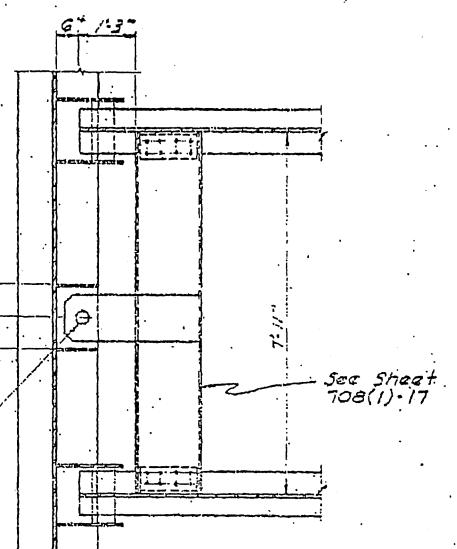
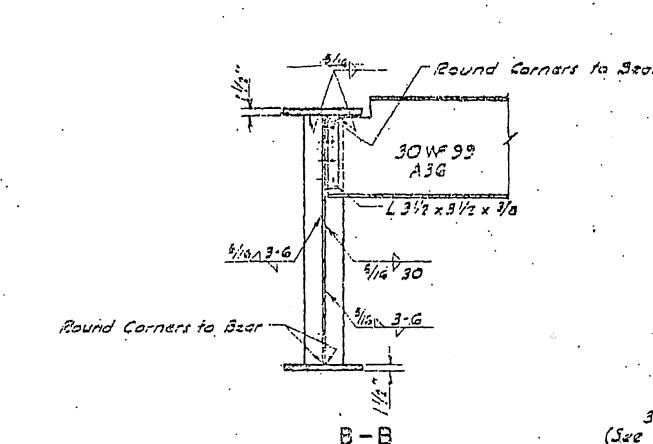
⁴ Includes Dead Load Deflections



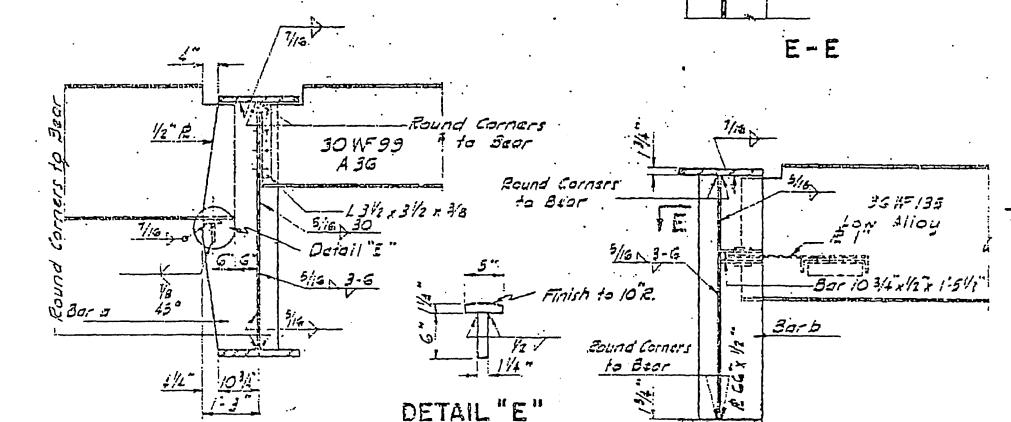
WELDING DETAIL



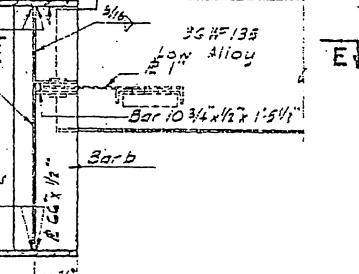
- PIN DETAIL



^{3" P₁}
(See Det)



DETAIL "E"

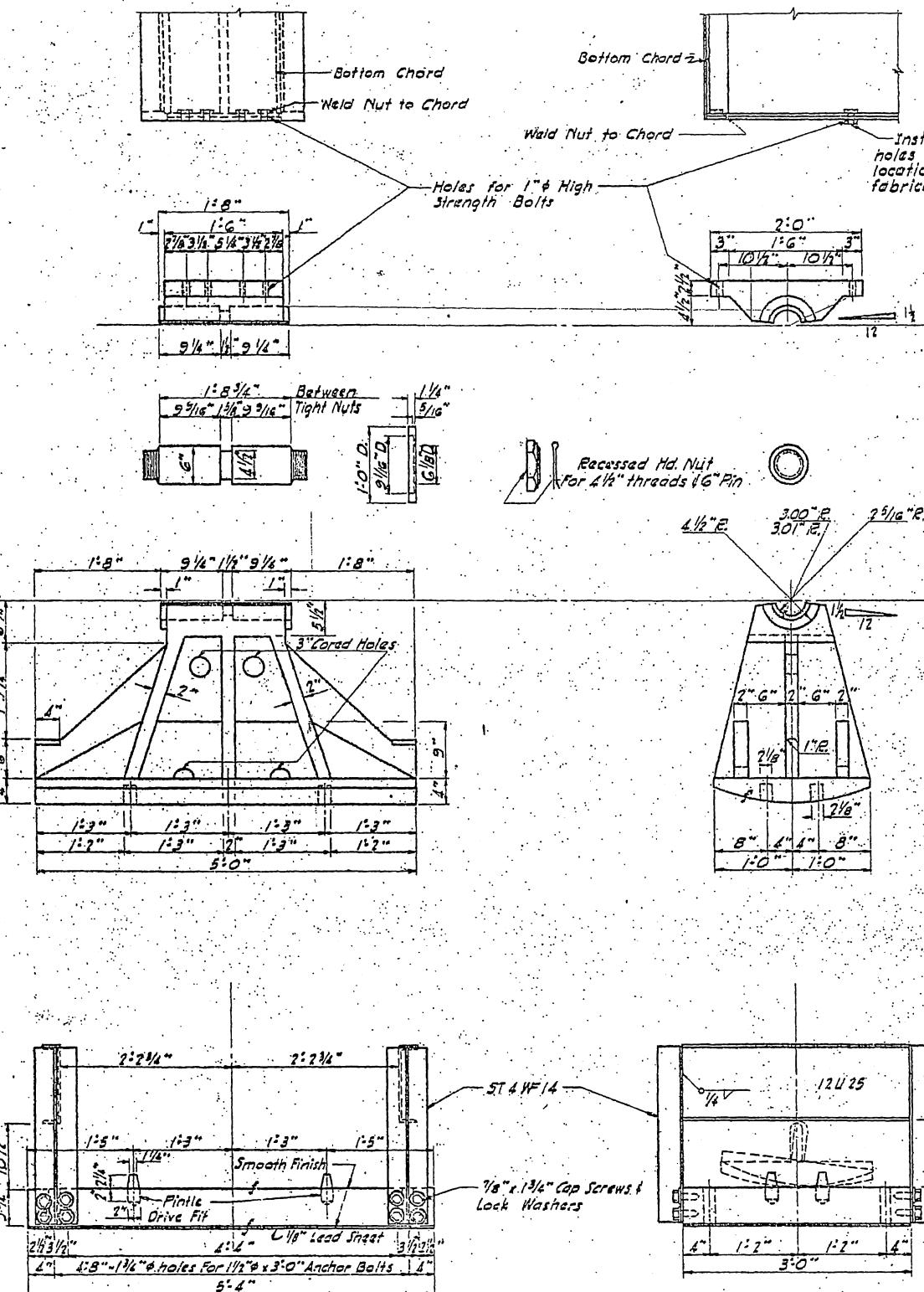


10

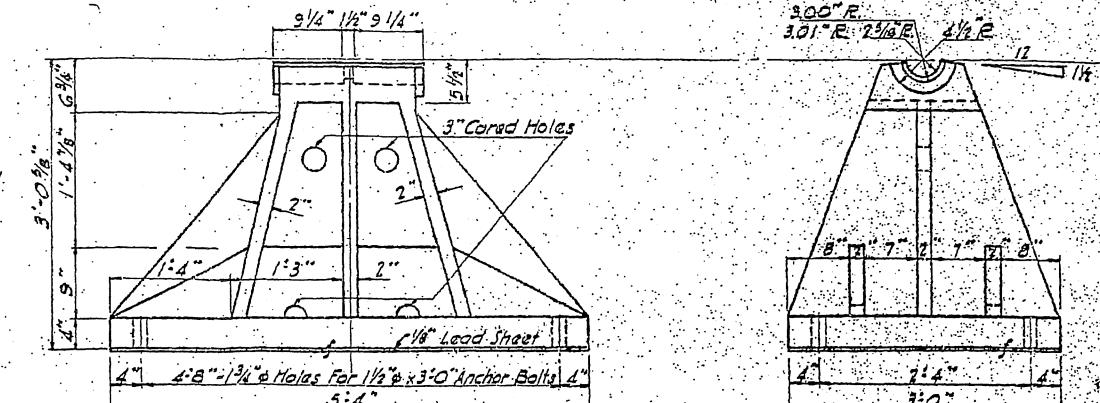
RED RIVER BRIDGE
SKIDMORE AVE.
RAND FORKS, N.D.-E GRAND FORKS, MINN.

FLOORBEAMS AND LOOR SYSTEM DETAILS

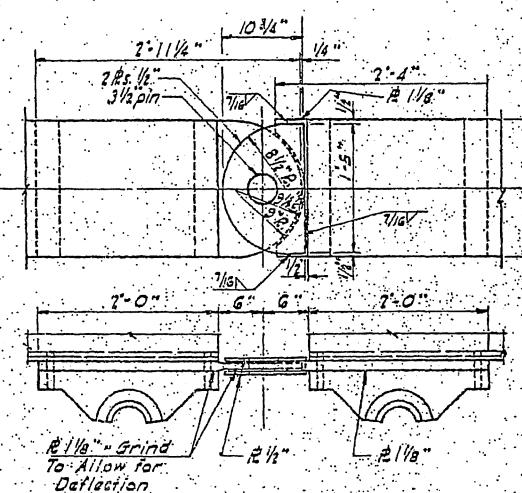
FED. ROAD DIV. NO.	STATE	PROJ. NO.	FEAS. YEAR	PICTURE NO.	TOTAL AMOUNT
5	N.D.	F-703(1)		34	43



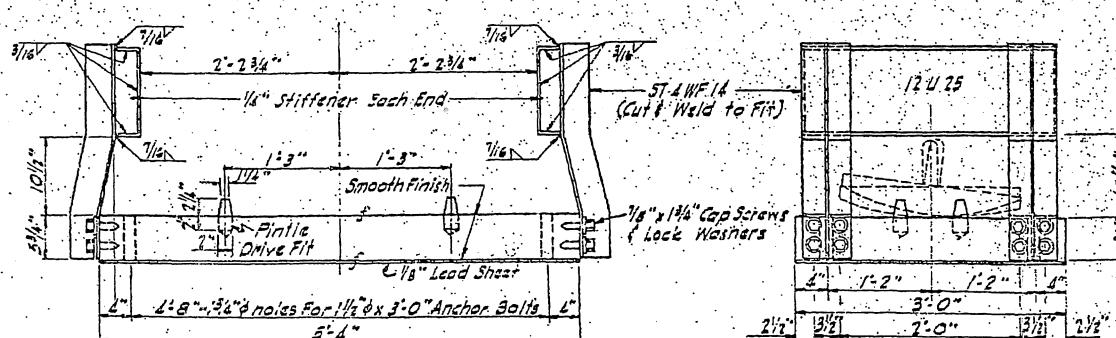
BEARING DETAILS PIER #6 & #8



BEARING DETAILS RIVER PIER #7
(North Side Only)



SWIVEL DETAILS RIVER PIER #7
(North Side Only)



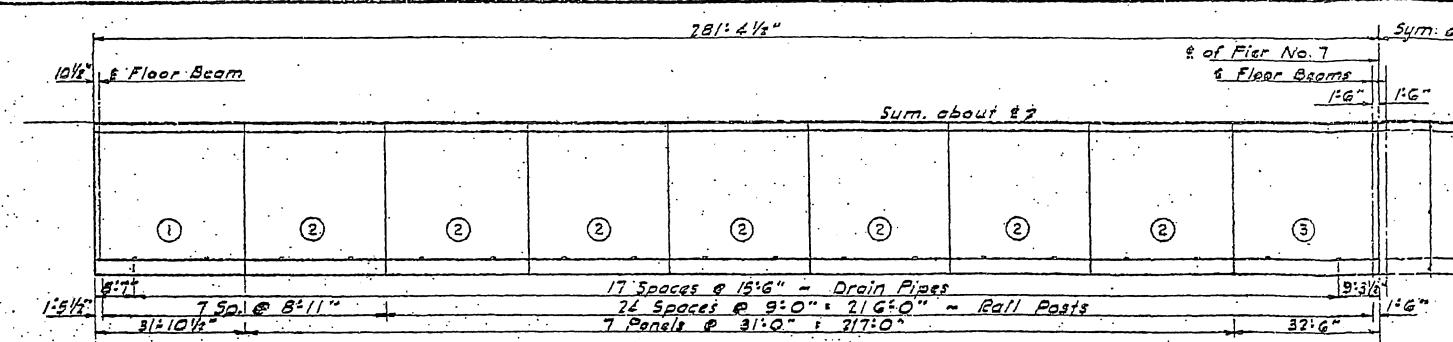
BEARING DETAILS PIER #7
(South Side Only)

MATERIALS:
Masonry plates for expansion bearing shall be rolled steel plates.
Expansion rockers and fixed shoes shall be cast steel.
Top bolsters may be cast steel or cut from rolled steel plates. In either case the pay weight will be computed as castings.
Lead sheets shall be paid for by the pound as structural steel.
Cast steel shall conform to A.A.S.H.O. M-192, Class 70-3G.

QUANTITIES

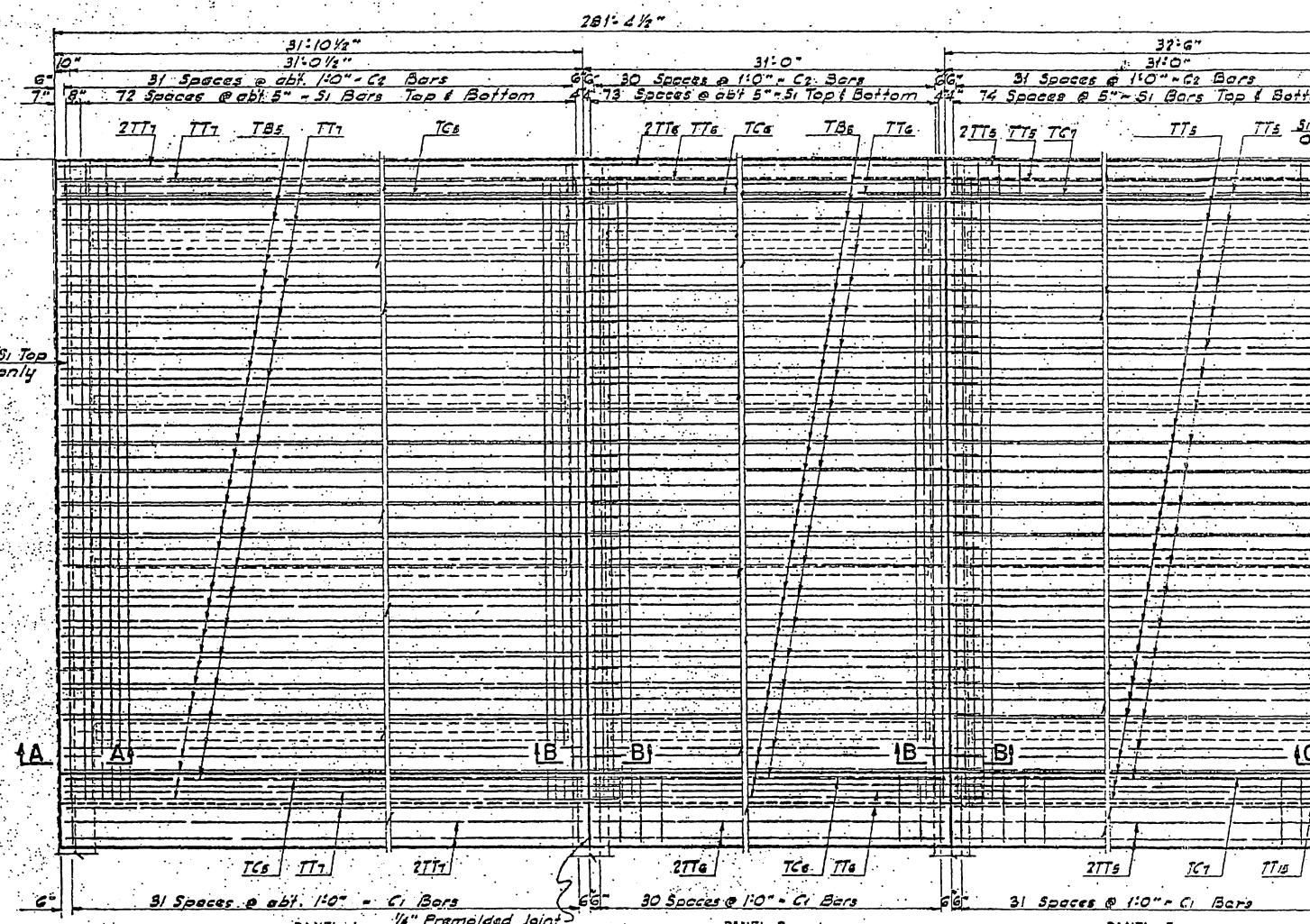
RED RIVER BRIDGE
SKIDMORE AVE.
GRAND FORKS, N.D.-E GRAND FORKS, MINN.

TRUSS BEARINGS



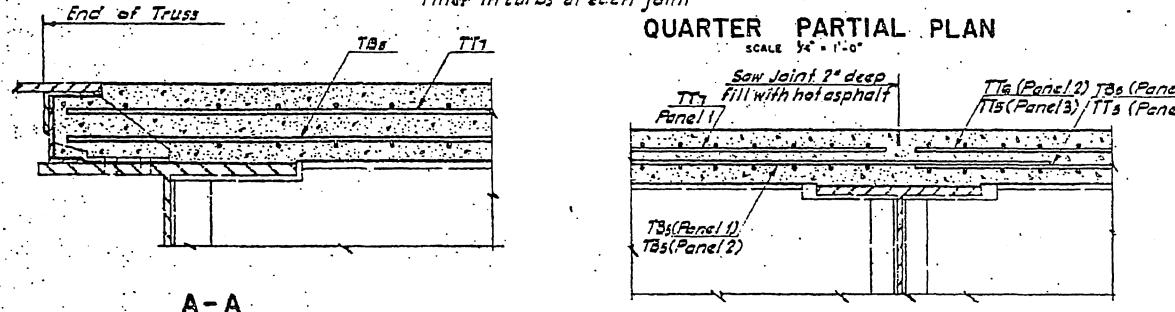
QUARTER DECK PLAN

SCALE 1" = 2'



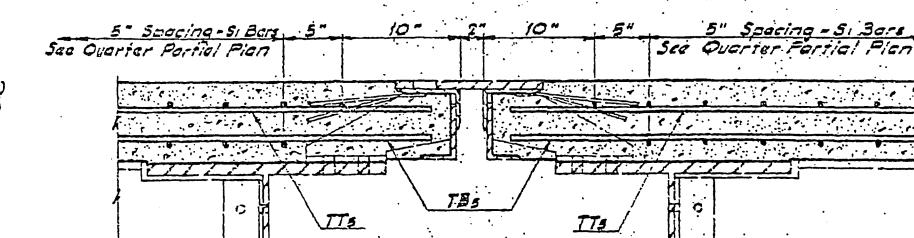
QUARTER PARTIAL PLA

SCALE $\frac{1}{2}'' = 1'-0''$



A-A

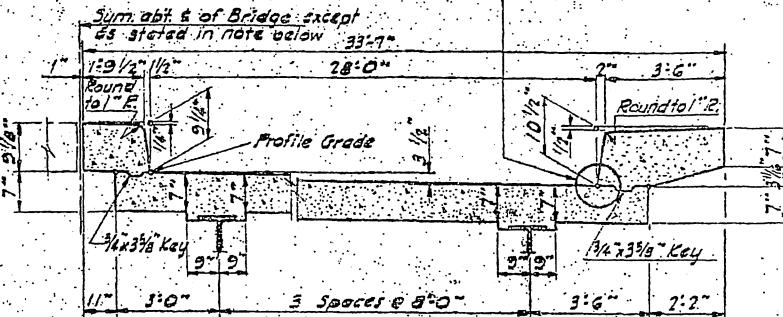
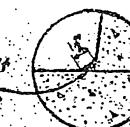
8-1



C -

BENT BAR DETAILS

Seal corner with asphalt
flashing compound.
(Knife Grade). — S



SLAB SECTION
Showing Dimensions

Slab section showing reinforcing steel in truss is the same as the approach spans shown on sheet 708(1)-22.

The square roadway from Sta. 1136+93.5 to Sta. 1157+55.5 shall be warped according to the profile grade and south gutter grades as shown on sheet 708(1)-22.

A camber of 1/16" shall be added to the profile girder at the mid-point of all stringers to account for dead load deflection. The truss floor slab, 12' width (30'-6") shall be poured continuously from end to end of truss.

Contraction joints, located at each floor beam, shall be sawed, preferably, within 8 hours of the time the concrete is poured, but not before the concrete has hardened to the extent that tearing and roavelling is prevented.

Note: For deck drains and quantities see sheet 708(1)-22

Yihong Gao - BR 9090 Update and final summary/ documentation

From: Joe Litman <Joe.Litman@lhbcorp.com>
To: "Yihong Gao" <Yihong.Gao@dot.state.mn.us>
Date: Wednesday, September 09, 2009 5:41 PM
Subject: BR 9090 Update and final summary/ documentation
CC: "Lisa Marynik" <Lisa.Marynik@lhbcorp.com>

Yihong,

Attached for your records is our final summary and checked documentation for the BR 9090 analysis work associated with the bearing location at L0. Though the result has not changed (a move of 7" more for total from original move of 14" for the bearing is still verified acceptable) the numbers herein vary from what you were emailed previously due to a couple more items we found and investigated while final checking and assembling. The primary change is an increase in the floor beam dead load contribution at joint L0. This increase is due to two items, the first being the need to include the dead load from the first truss panel which is shared 50/50 between joint L1 floorbeam and joint L0 floor beam but was not included in our earlier run and the second being an increase in the back (approach) span dead load for the span leading to the truss as our initial calculation utilized a 7" deck and we believe the approach span was also overlayed to a 9" slab just as the truss was so have adjusted that dead load accordingly. Note that truck load loading cases have also been removed as they do not govern for any instance. In the end as I mentioned previously though the rating factors etc do change the result as to what adjustment in the bearing location can be made remains the same. In any case it is important the records reflect our best interpretation/ analysis of the conditions which is what these now reflect.

I have also put a hard copy of all this in the mail to you so you will not have to print out and assemble this. Also, I'll give you a call to make sure you have no further questions and that the revisions are understood.

Thanks, Joe



21 West Superior Street, Suite 500
Duluth, Minnesota 55802
218 727-8446
Fax 218 727-8456
www.LHBcorp.com

September 9, 2009

Yihong Gao
Minnesota Department of Transportation
Office of Bridges and Structures, MS 610
3485 Hadley Avenue North
Oakdale, MN 55128-3307

Bridge 9090
Bearing Location/ L0 Gusset Check

Yihong,

Enclosed please find a copy of our hand and electronic file calculations for the review of the joint L0 gusset of Bridge 9090. As requested our review was performed to assess the impacts of the currently located support bearing, which is 7" from original location and to assess if the bearing could be moved an additional 7" or further. The results of our analysis work are detailed in the enclosed calculations consisting of:

- 10 pages of hand calculations and joint geometry/ loading diagrams
- 15 pages of hand calculations and program output summarizing loads used
- 12 pages of excel Gusset Check file output

In summary the findings indicate the controlling ratings for the joint L0 gusset are relatively unchanged for bearing position at the original location, the current 7" moved location and for an additional move of up to 7" (resulting in a total move from original construction of 14"). The analysis does however indicate that a total move from original beyond 14" (7" from existing) cannot be accommodated and would result in very unsatisfactory ratings for the gusset. As an example for a capacity reduction of 5% to account for age/ deterioration the Critical Operating Rating Factors are as follows:

Bearing Location	Joint L0 Critical Operating RF (CRF = .95)
Original Const. Loc.	1.38
7" from original Loc.	1.41
14" from original Loc.	1.41
21" from original Loc.	0.42

As you review these items please do not hesitate to call if you have any questions.

Sincerely
LHB, Inc.

A handwritten signature in black ink, appearing to read "Joseph D. Litman".

Joseph D. Litman P.E.

Enclosures
c: LHB Project No. 070745.3



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250 3rd Avenue North, Suite 450
Minneapolis, Minnesota 55401
612 338-2029
Fax 612 338-2088

PROJECT BR 9090 - JOINT LD GUSSET - ORIGINAL POSITION

PROJECT # 070745 / 090173 DATE 08/31/09 BY LMM SHEET NO. 01 OF 10
✓ 9/3/09 JDL

① BRIDGE INFORMATION:

- BUILT IN 1963
- GUSSET PLATE = LDW ALLOY STEEL ($\sigma_{fy} = 50 \text{ ksi}$, $F_u = 75 \text{ ksi}$)
- CHORD MEMBERS: $\phi F_y = 36 \text{ ksi}$ (Bottom chord @ L0 is Q & T steel, higher yield insig. though)
- HIGH STRENGTH BOLTS ($\phi F_s = 25 \text{ ksi}$)
- NO BOLT INFO FOUND - ASSUME DIA = $\frac{7}{8}''$, HOLE DIA = 1" JDL
- SEE SHEETS 4 AND 5 FOR GEOMETRY AND LOADING.
- LANE LOAD CREATES THE MAXIMUM LIVE LOAD IN THE TRUSS MEMBERS

CASE LN1: - WHEN THE CONCENTRATED LOAD IS PLACED AT L0, MAXIMUM BEARING RYN IS ACHIEVED

CASE LN2 - WHEN THE CONCENTRATED LOAD IS PLACED AT L1, MAXIMUM LIVE LOAD IN TRUSS MEMBERS IS ACHIEVED.

- RATINGS RECORDED BASED ON 5% SECTION LOSS

② TENSION - NO CHECK

- THE BOTTOM CHORD IS THE ONLY TENSION MEMBER.
IT IS FULLY WELDED TO THE GUSSET PLATE AND NOT SPLICED AT THE CENTER OF THE JOINT.

③ FLEXURE:

$$\begin{aligned} \text{A-A} - \text{LOAD CASE LN1} \text{ CREATES LOWEST RATING ON A-A} \\ A_g = 2 \times (0.625") \times (59.75") = 74.7 \text{ in}^2 & \quad y = \frac{1}{2}(59.75") \\ I_g = 2 \left(\frac{1}{2} \right) (0.625") (59.75")^3 = 22220 \text{ in}^4 & \quad = 29.9" \end{aligned}$$

USING THE LOADS ABOVE THE CUT: (T-LN1)

$$P_{BL} = 255.5^k + 830.2^k = 1085.7^k$$

$$P_{LL} = 118.0^k + 149.6^k = 267.6^k$$

$$M_{BL} = 255.5^k(29.9" - 12") + 830.2^k(29.9" - 25") = 8014.3 \text{ k-in}$$

$$M_{LL} = 118.0^k(29.9" - 12") + 149.6^k(29.9" - 25") = 2838.6 \text{ k-in}$$

$$RF_{INN} = 0.84 \quad RF_{OP} = 1.41$$



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PROJECT BR 9090 - JOINT LD GUSSET - ORIGINAL POSITION

PROJECT # 070745/090173 DATE 08/31/09 BY LMAN SHEET NO. 02 OF 10
19/3/09 JDL

SECTION A-A (CONTINUED)

USING THE LOADS BELOW THE CUT: (B-LN1)

$$P_{DL} = 1085.7 \text{ k}$$

$$P_{LL} = 267.6 \text{ k}$$

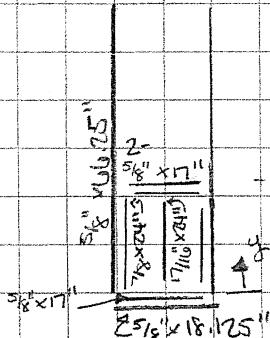
$$MDL = (1085.7 \text{ k})(29.9" - 12") - 735.9 \text{ k}(14.5") = 8736.3 \text{ k-in}$$

$$MLL = (267.6 \text{ k})(29.9" - 12") - 133.0 \text{ k}(14.5") = 2854.9 \text{ k-in}$$

$$RF_{INV} = 0.83 \quad RF_{OP} = 1.38 \quad \checkmark$$

SECTION B-B • USING LOAD CASE LN1, AND THE LOADS TO THE RIGHT OF THE CUT

- SECTION IS COMPOSED OF GUSSETS AND BOT. CHORD BUT NOT WF ABOVE CHORD



SECTION PROPERTIES CALCULATED IN EXCEL WKSHT

$$y = 21.1" \text{ (FROM BOTTOM)} \quad A = 193.98 \text{ in}^2$$

$$I = 626098 \text{ in}^4$$

$$P_{DL} = 736.6 \text{ k} - 735.9 \text{ k} = 0.7 \text{ k}$$

$$MDL = 0.7(21.1" - 12") = 6.4 \text{ k-in}$$

$$P_{LL} = 132.7 - 133.0 \text{ k} = 0.3 \text{ k}$$

$$MLL = 0.3(21.1" - 12") = 2.7 \text{ k-in}$$

$$RF_{INV} = 0.390 \quad RF_{OP} = 10.067 \quad \checkmark$$

(using conserv. Chord Fy of 36 kpsi)

SECTION C-C • USE LN2 LOADS

$$y = \frac{1}{2}(35.75" + 29") = \frac{1}{2}(64.75") = 32.4 \text{ in}$$

$$A = 2(0.1625") (64.75") = 80.9 \text{ in}^2 \quad I = \frac{1}{3}(0.1625") (64.75")^3 = 28278 \text{ in}^4$$

$$P_{DL} = \left(\frac{45}{78}\right) 1109.9 \text{ k} = 640.3 \text{ k}$$

$$MDL = 640.3 \text{ k}(32.4" - 29") = 21.61 \text{ k-in}$$

$$P_{LL} = \left(\frac{45}{78}\right) 257.8 \text{ k} = 148.7 \text{ k}$$

$$MLL = 148.7 \text{ k}(32.4" - 29") = 502 \text{ k-in}$$

$$RF_{INV} = 0.49 \quad RF_{OP} = 10.84 \quad \checkmark$$



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PROJECT BR 9090 - SOWT LD GUSSET - ORIGINAL POSITION

PROJECT # 070745 / 090173 DATE 08/31/09 BY LMM SHEET NO. 03 OF 10
✓ 9-3-09 JOL

(4) SHEAR: ~~(+) CONSERVATIVE CALCULATION~~

- END ANGLE AND PLATE ARE IGNORED AS
WELL AS WELDING OF GUSSET TO MEMBER
- LOADS ARE TAKEN BELOW THE CUT

(Load Case LN2)

$$P_{DL} = 735.9 \text{ k} \quad t_g = 5/8" \quad N_r = 1 \text{ (angle)} \\ P_{LL} = 159.1 \text{ k} \quad w_g = 60"$$

$$RF_{INV} = 1.44 \quad RF_{OP} = 2.40 \checkmark$$

E-E: DO NOT CHECK

- NO SPLICE IN BOTTOM CHORD THRUROUGH SECTION

(5) BLOCK SHEAR: NO CHECK - TENSION MEMBER WELDED

(6) EDGE BUCKLING:

RIGHT EDGE: $b = 23"$, NO STIFFENING REQUIRED

(7) BUCKLING: NO CHECK

- VERT. & DIAG. MEMB'S MILLED TO BEAR ON LD-LI

(8) RIVETS (0% SECTION LOSS)

$$LD-U1: P_{DL} = 1109.9 \text{ k} \quad N_{SS} = 78 \quad L_c = 3\frac{3}{8}" - 1" = 2\frac{3}{8}" \\ P_{LL} = 257.8 \text{ k} \quad N_{RS} = 0$$

$$RF_{INV} = 1.61 \quad RF_{OP} = 2.69$$

SUMMARY:

FLEXURE SECTION A-A CONTROLS

(LOAD CASE LN1)

$$RF_{INV} = 0.83 \quad RF_{OP} = 1.38$$

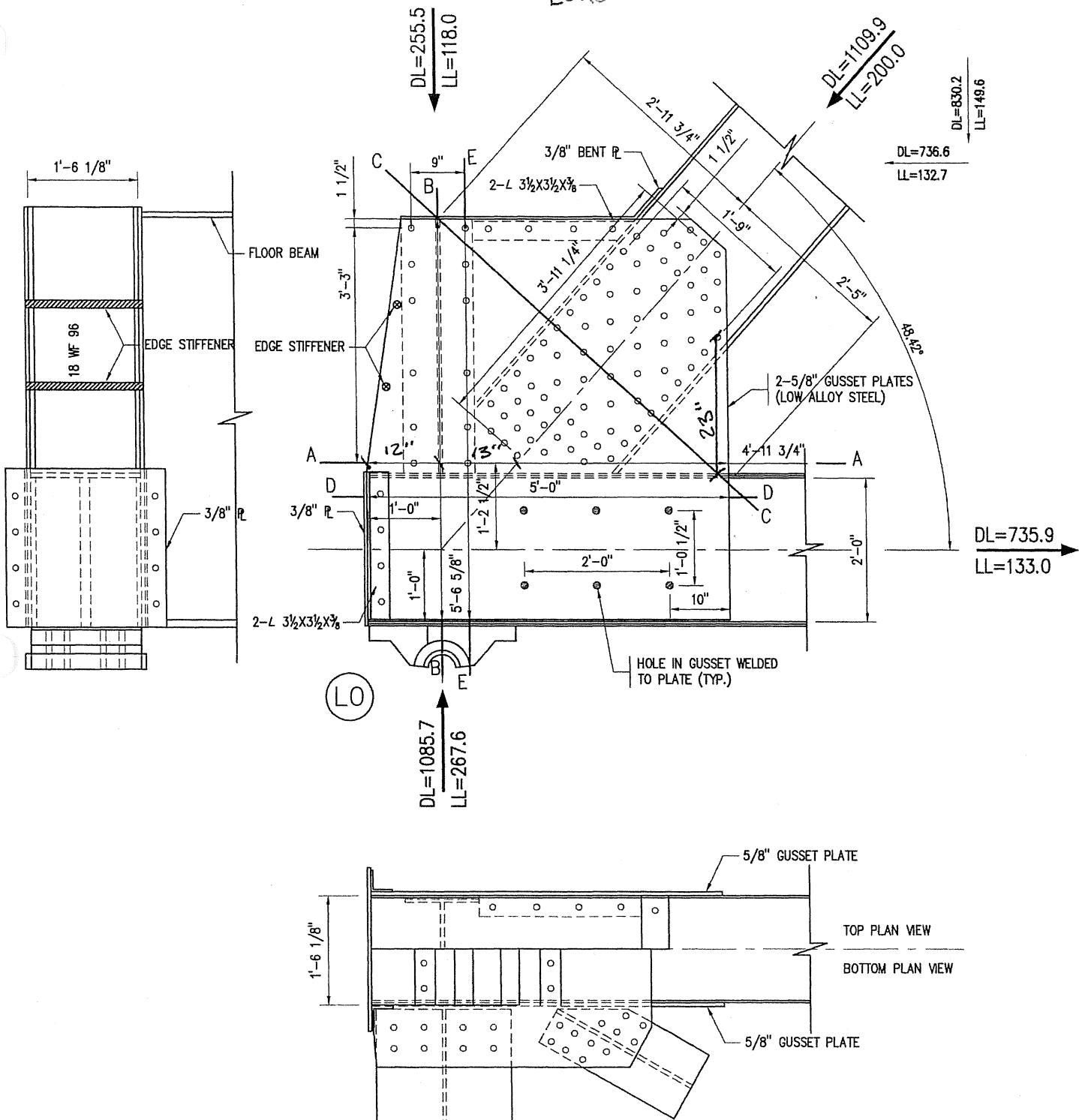


FLEXURE SECTION (A-A)

FLEXURE SECTION (B-B)

LOAD CASE LN1

4/10

Lane Load Conc.
Load Placed at L0

JOINT LO

SCALE: 0

2'

JOL 9/3/09

DATE: 08/31/09



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TITLE:

JOINT LO

(ORIGINAL POSITION - LANE LOAD W/ CONC. LOAD @ LO)

DR: LMM

CHK: JOL

APPROVED:

Bridge No.

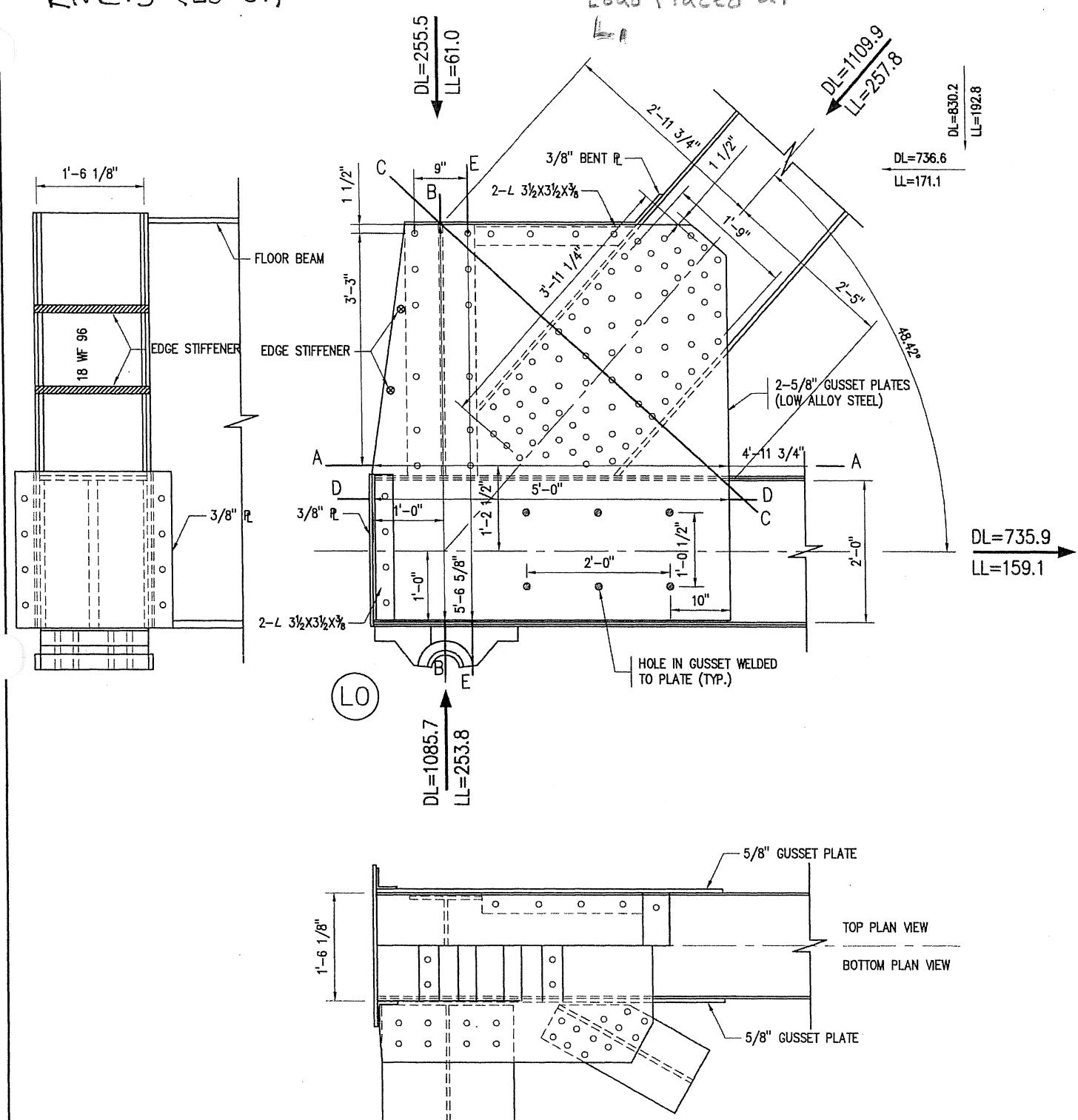
Sheet No. 04 of 10 Sheets

9090

FLEXURE SECTION C-C
SHEAR SECTION D-D
RIVETS (LO-U1)

LOAD CASE LN2

5/10



JOINT LO

SCALE: 0' 2'

✓ JDL 9/3/09

DATE: 08/31/09



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TITLE: JOINT LO (ORIGINAL POSITION - LANE LOAD W/ CONC. LOAD @ L1)	DR: LMM CHK: <u>JDL</u>	APPROVED:	Bridge No. 9090
		Sheet No. 05 of 10 Sheets	



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PROJECT BR 9090 - JOINT LD GUSSET - MOVED BEARING
PROJECT # 070745/090173 DATE 08/31/09 BY LMM SHEET NO. 06 OF 10
✓ 9/3/09 JDL

- BEARING WAS MOVED 7" FROM ITS ORIGINAL POSITION
- MN/DOT DESIRES TO MOVE IT 7" MORE, AND POTENTIALLY 7" AFTER THAT ✓
- THE FLEXURE SECTIONS A-A (B-LN1) AND B-B (LN1) ARE THE ONLY RATINGS THAT WILL BE AFFECTED
 - REFER TO SHEET 02 FOR ORIGINAL CALCULATION.

SECTION A-A (ONLY MOMENTS CHANGE FROM ORIG.)

$$7'' \text{ MOVE: } M_{DL} = (1085.7^k)(29.9'' - 19'') - 735.9^k(14.5'') = 1136.4 \text{ k-in}$$

$$M_{LL} = (267.6^k)(29.9'' - 19'') - 133.0^k(14.5'') = 981.7 \text{ k-in}$$

$$RF_{INV} = 2.50 \quad RF_{OP} = 4.18$$

$$14'' \text{ MOVE: } M_{DL} = -(1085.7^k)(29.9'' - 26'') + 735.9^k(14.5'') = 4163.5 \text{ k-in}$$

$$M_{LL} = -(267.6^k)(29.9'' - 26'') + 133.0^k(14.5'') = 891.6 \text{ k-in}$$

$$RF_{INV} = 1.81 \quad RF_{OP} = 3.01 \quad \checkmark$$

$$21'' \text{ MOVE: } M_{DL} = -(1085.7^k)(29.9'' - 33'') + 735.9^k(14.5'') = 14063 \text{ k-in}$$

$$(-267.6^k)(29.9'' - 33'') + 133.0^k(14.5'') = 27105 \text{ k-in}$$

$$RF_{INV} = 0.25 \quad RF_{OP} = 0.42 \quad \checkmark$$

SECTION B-B (ASSUME PDL = PLU = 0, LOADS SHOULD CANCEL)

$$7'' \text{ MOVE: } M_{DL} = 1085.7^k(7'') = 7600 \text{ k-in}$$

$$M_{LL} = 267.6^k(7'') = 1873 \text{ k-in} \quad RF_{INV} = 22.57 \quad RF_{OP} = 51.07$$

$$14'' \text{ MOVE: } M_{DL} = 1085.7^k(14'') = 15200 \text{ k-in}$$

$$M_{LL} = 267.6^k(14'') = 3744 \text{ k-in} \quad RF_{INV} = 10.07 \quad RF_{OP} = 11.81$$

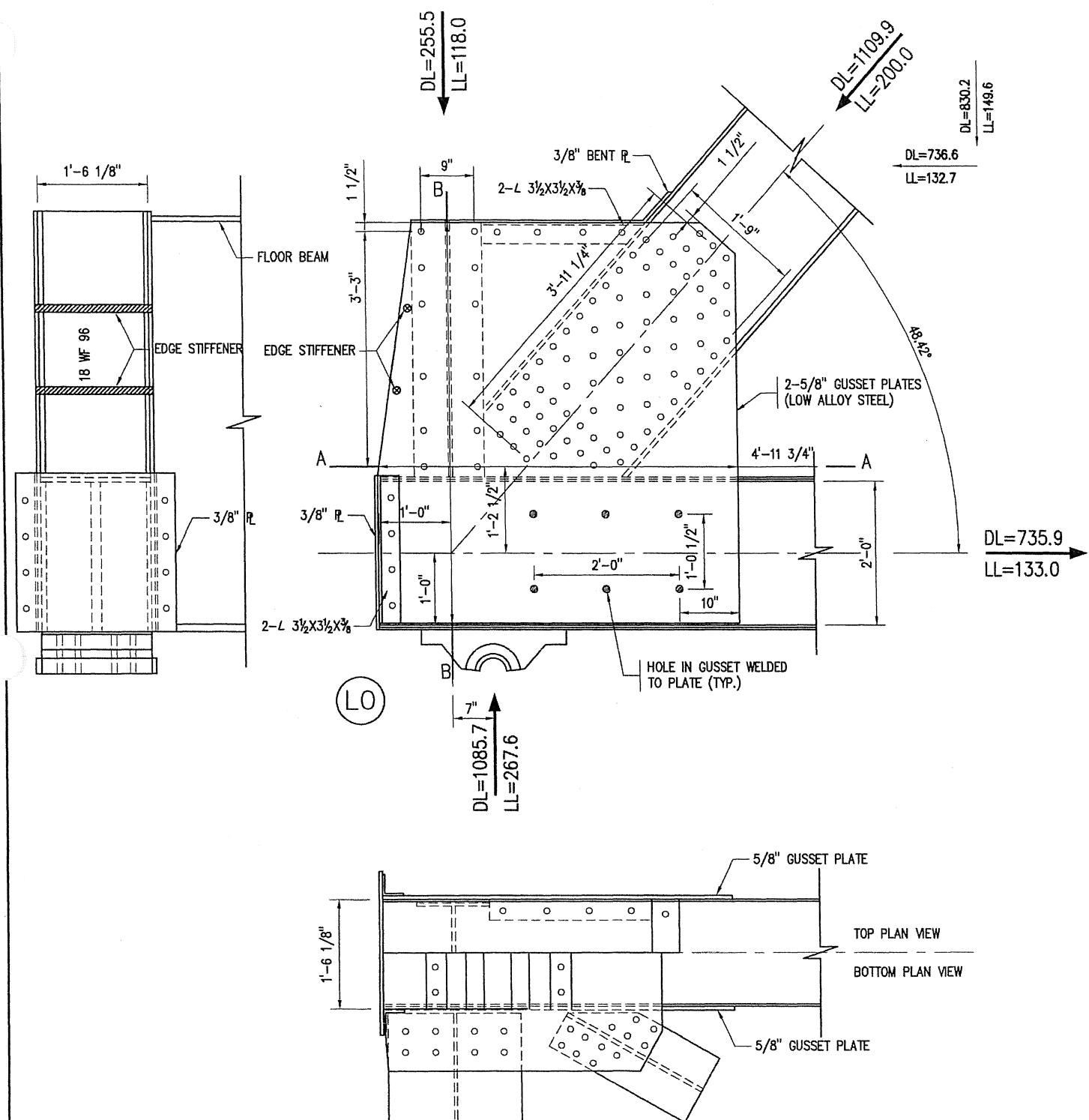
$$21'' \text{ MOVE: } M_{DL} = 1085.7^k(21'') = 22800 \text{ k-in}$$

$$M_{LL} = 267.6^k(21'') = 5620 \text{ k-in} \quad RF_{INV} = 5.90 \quad RF_{OP} = 9.85$$

FLEXURE A-A
B-B

LOAD CASE LN1

7/10



JOINT LO

SCALE: 0' 2'



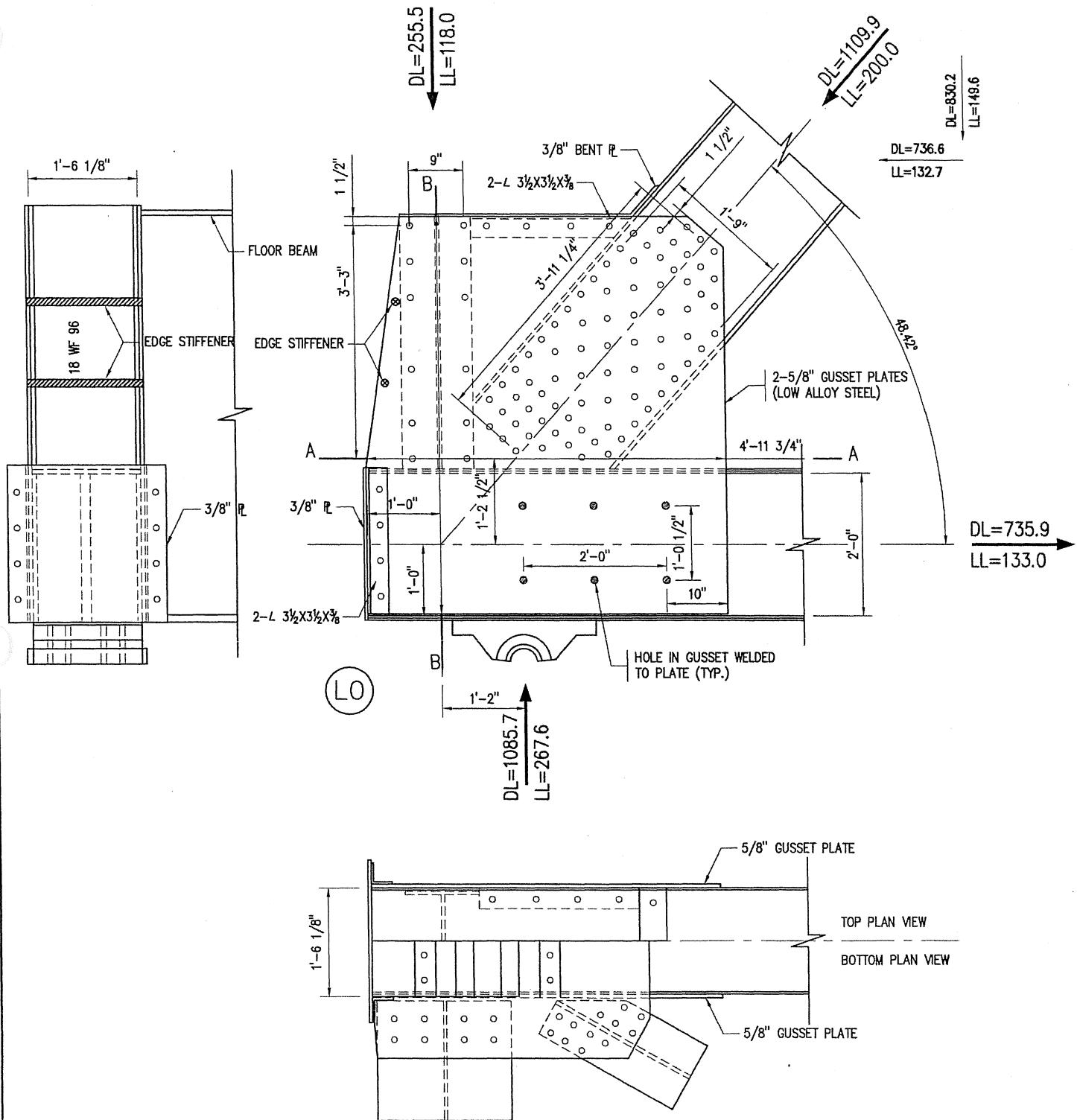
DATE: 08/31/09

TITLE: JOINT LO (BEARING MOVED 7" - LANE LOAD W/ CONC. LOAD @ LO)	DR: LMM CHK: TDL	APPROVED:	Bridge No. 9090
		Sheet No. 07 of 10 Sheets	

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FLEXURE A-A
B-B

LOAD CASE LN1
8/10



SCALE: 0 2'

✓ JOU 9/3/09

DATE: 08/31/09



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TITLE:

JOINT LO

(BEARING MOVED 14" - LANE LOAD W/ CONC. LOAD @ LO)

DR: LHM
CHK: JDL

APPROVED:

Bridge No.

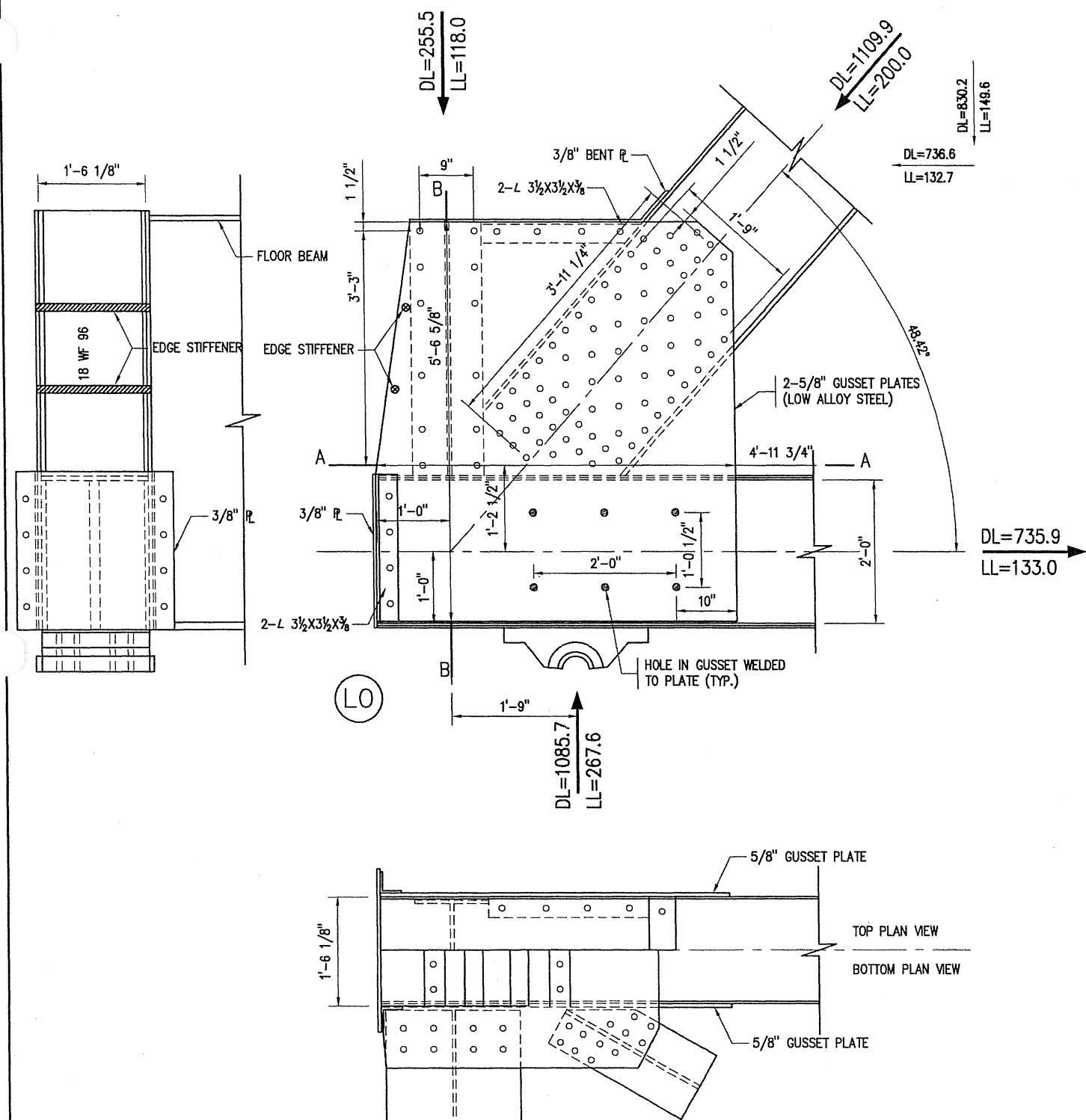
Sheet No. 08 of 10 Sheets

9090

FLEXURE A-A
B-B

LOAD CASE LN1

9/10



JOINT LO

SCALE: 0 2'

JOL 9/3/09

DATE: 08/31/09



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TITLE:
JOINT LO
(BEARING MOVED 21" - LANE LOAD w/ CONC. LOAD @ LO)

DR: LMM	APPROVED:
CHK: JOL	

Sheet No. 09 of 10 Sheets

Bridge No.
9090



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PROJECT BR 9090 - GUSSET LO

PROJECT # 070745/070173 DATE 08/31/09 BY LMM SHEET NO. 10 OF 10
9/3/09 JDL

SUMMARY:

- FLEXURE SECTION A-A CONTROLS THE PLATE
- IT IS NOT RECOMMENDED TO MOVE THE BEARING MORE THAN AN ADDITIONAL 7" (14" FROM ORIG. POSITION)
- THE RATING FOR THE PLATE AFTER THIS MOVE WILL BE AS FOLLOWS:

5% SECTION LOSS

$$RF_{INV} = 0.84$$

$$RF_{OP} = 1.141$$

10% SECTION LOSS

$$RF_{INV} = 0.53$$

$$RF_{OP} = 0.89$$

✓

✓

✓

- NOTE THAT THESE RATING FACTORS ARE CALCULATED USING THE LOADS ABOVE THE SECTION CUT AND NOT THE LOADS FROM THE BEARING ZEN



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PROJECT BR.9090 - JOINT LO

LOAD SUMMARY

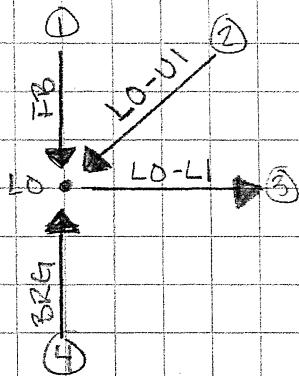
PROJECT # 070745

DATE 08/31/09

BY LMM

SHEET NO. 01 OF 09

✓ 9/3/09 JOL



DEAD AND LIVE LOAD REACTIONS HAVE BEEN CALCULATED FOR JOINT LO.

THERE ARE 4 REACTIONS AT THIS JOINT

1) FB = FLOORBEAM REACTION, WHICH INCLUDES LOADS FROM THE FIRST BAY OF THE TRUSS AS WELL AS THE BALKSPAN

2) LO-U1 = LOAD IN TRUSS MEMBER

3) LO-L1 = " " " "

4) BRG = BEARING REACTION

DEAD LOAD

- TWO SETS OF CALCULATIONS WERE PERFORMED FOR FLOOR BEAM
 - REFER TO SHEETS 02 TO 04 FOR CALC'S
- MEMBER LOADS WERE OBTAINED FROM TRR MODEL
 - REFER TO OUTPUT ON SHEETS 05 AND 06 AND 09
- REACTION FORCES WERE DETERMINED BY SUMMATION OF FORCES

$$1) FB = 93.7^k + 161.8^k = 255.5^k$$

$$2) LO-U1 = 1109.9^k, \angle = 48.42^\circ \quad (x = 736.6^k, y = 830.2^k)$$

$$3) LO-L1 = 735.9^k$$

$$4) BRG = 255.5^k + 830.2^k = 1085.7^k$$



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LOAD SUMMARY

02 OF 09

PROJECT BRIDGE 9090

PROJECT # 070745 DATE 8/24/09 BY JW S SHEET NO. 02 OF 09
✓ 9/3/09 JOL

COMPUTE DEAD LOAD APPLIED @ L₀

⇒ FROM 1/2 BAY OF TRUSS SYSTEM (31' BAYS)

- REFERENCE RAM CALCULATIONS (1/11/08)

STRINGERS	12276	#	-
FLOOR BEAM	23570		-
DIAPH'S / STIFF	912		-
GUSSET'S / Bracing	5500		-
	42,258	#	STEEL

CONE DECK	128,624	#	-
RAILS	7750		-

136,374 # CONC. Detail/Misc. wt. factors

$$\text{TOTAL @ } L_0 = [23570(1.02) + 18688(1.05) + 136,374]/2 + 3.665 \frac{\text{K}}{\text{ft}^2}$$

FROM TRUSS = 93,684 # ✓ truss wt.

⇒ From BACKSPAN ~56.5' SPAN

- REF. RAM CALC (8/14/09) (EXCEPT AS NOTED)

BEAMS = 61,290

STIFF = 3154

CHANN = 2658

DIAPH = 6394

73496 # STEEL ✓

ASSUMES 9" DECK AS
IN TRUSS 7" IN
THIS ANALYSIS.
WAS ASSUMED RAM USED
ON 8/14. THIS

$$\text{CONC DECK} = 2(27.66)(56.5)(150)(1/2) = 234,420$$

$$\text{RAILS } 250 \text{ PLF } (56.5)(2)(1/2) = 14,125$$

248,545 # CONC

$$\text{TOTAL @ } L_0 = [73496(1.02) + 248,545]/2 = 161,755 \#$$



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LOAD SUMMARY
03 0F 09

PROJECT BRIDGE NO. 9090

PROJECT # 070745.3 DATE 1/11/08 BY RAM SHEET NO. 1 OF 6
✓ CJM 2/13/08

FLOOR SYSTEM DEAD LOADS (AT FLOORBEAM LI)

STRINGERS

$$= (49 \text{ LB/FT})(3)(31'-0")^{1/2} = 12,276 \text{ LB}$$

NODE NUMBERS MATCH
ORIGINAL PLAN USED
RAM DEAD LOADS IN
TENSIS ANALYSIS.

FLOORBEAM

$$\text{WEB} = (.6"')(7\frac{1}{16"})(67'-4\frac{5}{8"}) (490 \text{ PCF}) = 6621 \text{ LB}$$

$$\text{FLANGES} = 2(1'-10") (1") (17'-3\frac{3}{8"}) (490 \text{ PCF}) = 2537.4 \text{ LB}$$

$$\text{FLANGES} = 2(1'-10") (1\frac{3}{4"}) (50-0") (490 \text{ PCF}) = 13,100.7 \text{ LB}$$

$$\text{STIFFENERS} = (.6") (5") (\frac{5}{8"}) (490 \text{ PCF}) (17) = 596.5 \text{ LB}$$

$$\text{END STIFFENER} = 2(.6"')(1-0") (\frac{5}{8"}) (490 \text{ PCF}) = 280.7 \text{ LB}$$

$$\text{CONNECTION ANGLE} = (8.5 \text{ LB/FT})(1-8") (8) = 113.3 \text{ LB}$$

235.6^a

DIAPHRAGMS

$$= (33.9 \text{ LB/FT})(8'-0") (6)^{1/2} = 813.6 \text{ LB}$$

$$\text{STIFFENERS} = (9.8 \text{ LB/FT})(1-8") (12) \frac{1}{2} = 98 \text{ LB}$$

NECK (FROM AUTOCAD DRAWING)

$$= 2(27.661 \text{ FT}^2)(31'-0") (150 \text{ PCF})^{1/2} = 103,623.7 \text{ LB}$$

RAILING (ASSUMED)

$$= (1-6") (1'-0") (150 \text{ PCF}) + 25 \text{ PLF} = (250 \text{ LB/FT})(31'-0") 2 (1/2) = 7,750 \text{ LB}$$



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LOAD SUMMARY

04 OF 09

PROJECT BRIDGE NO. 9090

PROJECT # DATE 8/14/09 BY RAM SHEET NO. 1 OF 1
✓ LMM

APPROACH SPAN LOADS

$$BEAMS = (135 \text{ LB/FT}) (56'-9") (8) = 61,290 \text{ LB}$$

$$\text{STIFFENERS} = (6\frac{1}{2}'' \times \frac{1}{2}'' \times 33.92'') (490 \text{ PCF}) 8 (8) = 2000.7 \text{ LB}$$

$$= (5'' \times \frac{1}{2}'' \times 33.92'') (490 \text{ PCF}) 6 (3) = 1154.2 \text{ LB}$$

$$CHANNELS = (7.25 \text{ LB/FT}) (10') (53) (8) = 2658.3 \text{ LB}$$

$$DIAPHRAGMS = (42.7 \text{ LB/FT}) (8'-0") (16) = 5465.6 \text{ LB}$$

$$= (58 \text{ LB/FT}) (8'-0") 2 = 928 \text{ LB}$$

$$72,906.2 \quad 80,296.3 \quad \Delta = 1/2\% \text{ OK}$$

$$\text{TOTAL STEEL} = 73,400.2 \text{ LB} + 10\% = 80,740.2 \text{ LB}$$

$$DECK = (2'') (56'-9") (150 \text{ LB/FT}) (31'-0" \times 2) = 207,360.6 \text{ LB } \cancel{1/2 (\text{sum})} \\ = 231,256.3$$

$$OVERHANG = (8.5") (3'-6") (56'-9") (150 \text{ LB/FT}) 2 = 42,307.3 \text{ LB}$$

$$MEDIAN = (9") (1'-11") (56'-9") (150 \text{ LB/FT}) 2 = 34,473.4 \text{ LB}$$

$$RAIL = (1'-6") (1'-0") (56'-9") (150 \text{ LB/FT}) 2 = 25,537.5 \text{ LB}$$

$$METAL = (30 \text{ LB/FT}) (56'-9") 2 = 3405 \text{ LB}$$

$$572,195.2 \quad 286,097.10 \quad 143,048.8 \\ \text{TOTAL} = 484,232.5 \text{ LB } \div 2 = 242,116.3 \text{ LB } \div 2 = 121,053.1 \text{ LB / GUS. PL}$$

$$143,048 + (1/2)(1/2)(80740.2) = 1675 \text{ COMPARE TO } 143,048 \text{ OK}$$

143,048.8

= 121 K

143 K

TABLE 3.13 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN DIAG. MEMBERS (UNFACTORED)

MEMBER	TOTAL STEEL		TOTAL DEAD LOAD	
	FORCE (K)	ADJ LENGTH (FT)	FORCE (K)	ADJ LENGTH (FT)
MnDOT LDU,	L 1 U 2	-1109.9	46.7303	-1109.9
	U 2 L 3	452.7	46.7725	452.7
	U 3 L 4	270.6	53.2994	270.6
	U 4 L 5	164.5	57.4350	164.5
	L 5 U 6	0.0	58.8303	0.0
	U 5 L 6	-1.5	58.8301	-1.5
	L 6 U 7	167.7	57.4353	167.7
	L 7 U 8	273.9	53.3042	273.9
	L 8 U 9	455.4	46.7807	455.4
	U 9 L 10	-1100.5	46.7305	-1100.5

TABLE 3.9 DEAD LOAD FORCES AND ADJUSTED LENGTHS IN LOWER CHORD (UNFACTORED)

MEMBER	TOTAL STEEL		TOTAL DEAD LOAD	
	FORCE (K)	ADJ LENGTH (FT)	FORCE (K)	ADJ LENGTH (FT)
(MnDOT L _o L _i)				
L 1 L 2	735.9	31.0069	735.9	31.0069
L 2 L 3	735.9	31.0135	735.9	31.0135
L 3 L 4	1036.0	31.0190	1036.0	31.0190
L 4 L 5	1193.5	31.0190	1193.5	31.0190
L 5 L 6	1282.3	31.0187	1282.3	31.0187
L 6 L 7	1190.9	31.0189	1190.9	31.0189
L 7 L 8	1031.6	31.0189	1031.6	31.0189
L 8 L 9	729.6	31.0134	729.6	31.0134
L 9 L 10	729.6	31.0134	729.6	31.0134



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PROJECT BR 9090 - JOINT LO -

LOAD SUMMARY

PROJECT # 070754 DATE 08/13/09 BY LNU SHEET NO. 07 OF 09

✓ 9-3-09 Job

LIVE LOADS

- REFER TO SHEET 01 FOR LOAD DIAGRAM / EXPLANATIONS
- MAXIMUM LIVE LOAD REACTIONS IN MEMBERS WERE ALL RESULTS OF LANE LOADING

LNU

- THE MAXIMUM REACTION AT THE FLOOR BEAM OCCURS WHEN THE CONCENTRATED LOAD IS APPLIED AT LD.
 - SEE SHEET 08 (LOAD CASE B)

$$1) FB = 118.0 \text{ k} \quad \checkmark$$

$$2) LO-U1 = 200.0 \text{ k} \quad (x = 132.7 \text{ k}, y = 149.6 \text{ k}) \quad \checkmark$$

$$3) LO-L1 = 133.0 \text{ k} \quad \checkmark$$

$$4) BRG = 118.0 \text{ k} + 149.6 \text{ k} = 267.6 \text{ k} \quad \checkmark$$

LN2

- THE MAXIMUM REACTION IN THE TRUSS MEMBER LO-U1 OCCURS WHEN THE CONCENTRATED LOAD IS APPLIED TO JOINT L1
- SEE SHEET 09 FOR COINCIDENT MEMBER LOADS

$$1) FB = [0.640 \text{ k/ft} (36.5 \text{ ft}) (\frac{1}{2}) + 0.640 \text{ k/ft} (31') (\frac{1}{2})] \times 1.676 \times 1.3 \\ = 61.0 \text{ k}$$

$$2) LO-U1 = 257.8 \text{ k} \quad (x = 171.0 \text{ k}, y = 192.8 \text{ k}) \quad \checkmark$$

$$3) LO-L1 = 159.1 \text{ k}$$

$$4) BRG = 61.0 \text{ k} + 192.8 \text{ k} = 253.8 \text{ k} \quad \checkmark$$

- GUSSET PLATE CALCULATIONS WILL REFER TO THE TWO ABOVE LOAD CASES AS LN1 AND LN2



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LOAD SUMMARY
08 OF 09

PROJECT BR. 9090

PROJECT # 070745

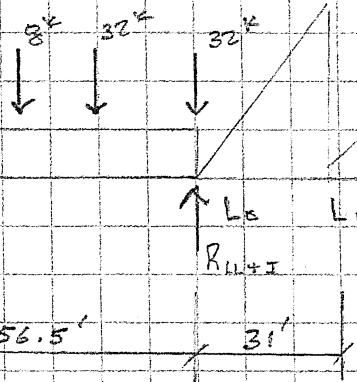
DATE 8/14/09

BY JWS

SHEET NO. 1 OF 1

CASE A - TRUCKS ON BACKSPAN

✓RAM 8/14/09
✓JDL 9/3/09



$$R_{L0+I} @ L_0 = \left[32 + 32 \left(\frac{42.5}{56.5} \right) + 3 \left(\frac{28.5}{56.5} \right) \right] \times 1.676 \text{ LANES} \times 1.28 \text{ Impact} = 129 \text{ k}$$

(NO LOAD IN TRUSS MEMBERS)

CASE B - LANE LOAD HINGE TO L₁

$$R_{L0+I} = \left[0.640(56.5)(1/2) + 0.640(31)(1/2) \right] \times 1.3 \times 1.676 + 26(1.3)(1.676) = 118 \text{ k}$$

$$\begin{cases} \text{LOAD IN } L_0-L_1 = 34 \text{ k} & (133 \text{ k if LANE LOAD TO END OF TRUSS}) \\ \text{LOAD IN } L_0-U_1 = -51 \text{ k} & (-200 \text{ k if LANE LOAD TO END OF TRUSS}) \end{cases}$$

See attached sheets 08a through 08f for lane load member force computations.

CASE C - TRUCK ON TRUSS @ L₀

$$R_{L0+I} = \left[32 + 32(17/31) + 3(3/31) \right] \times 1.676 \times 1.124 = 95 \text{ k}$$

$$\text{LOAD IN } L_0-L_1 = 32 \text{ k}$$

$$\text{LOAD IN } L_0-U_1 = -49 \text{ k}$$



Project: Mn/DOT - Truss Ratings
Project Number: 070745.30
Description: Truss Member Force Calculations

08a.

This template computes truss member live loads at a selected truss node.
Enter variables below shaded in grey. Regions or results in yellow self-compute.
Live Load is for HS-20 Lane Load with Concentrated Load for Flexure.

Note that this template reads external "excel" data files. These files must be properly linked to this worksheet for accurate function.

MN/DOT BRIDGE NO: 9090 - TH 2 over Red River in Grand Forks

IMPACT := 1.124

Input Impact Factor Based on Truss Length

DIST_FACTOR := 1.676

Input Distribution Factor for Truss,
Including any Applicable Reduction for
Multiple Lanes

MEMBER_TYPE := "D"

Input "D" for Diagonal, "V" for Vertical
or "C" for Chord.

PANEL_POINT := "L1"

Input Loaded Panel Point Under Consideration

MEMBER_NO := "L1L2"

Input Member Number Under Consideration

Member L0-L1 (MnDOT Numbering)

FOR VERTICAL MEMBERS, ENTER USING "L2U2T" AND "L2UTB" FOR FORCES

- Computation for Live Load Force in member
L₀-L₁, bot. chord for lane loading with
Conc. load placed at L₀ (MnDOT Numbering).

AT TOP AND BOTTOM OF MEMBER, WHICHEVER IS DESIRED

086

MEMBER_LOADLANE := AA·BB·IMPACT·DIST_FACTOR

MEMBER_LOADTRUCK := AA·CC·IMPACT·DIST_FACTOR

MEMBER_LOADLANE = 132.249

✓ Mn DOT
Member Lo-L₁

MEMBER_LOADTRUCK = 21.497

X := 0 , 1 .. 10

AA =

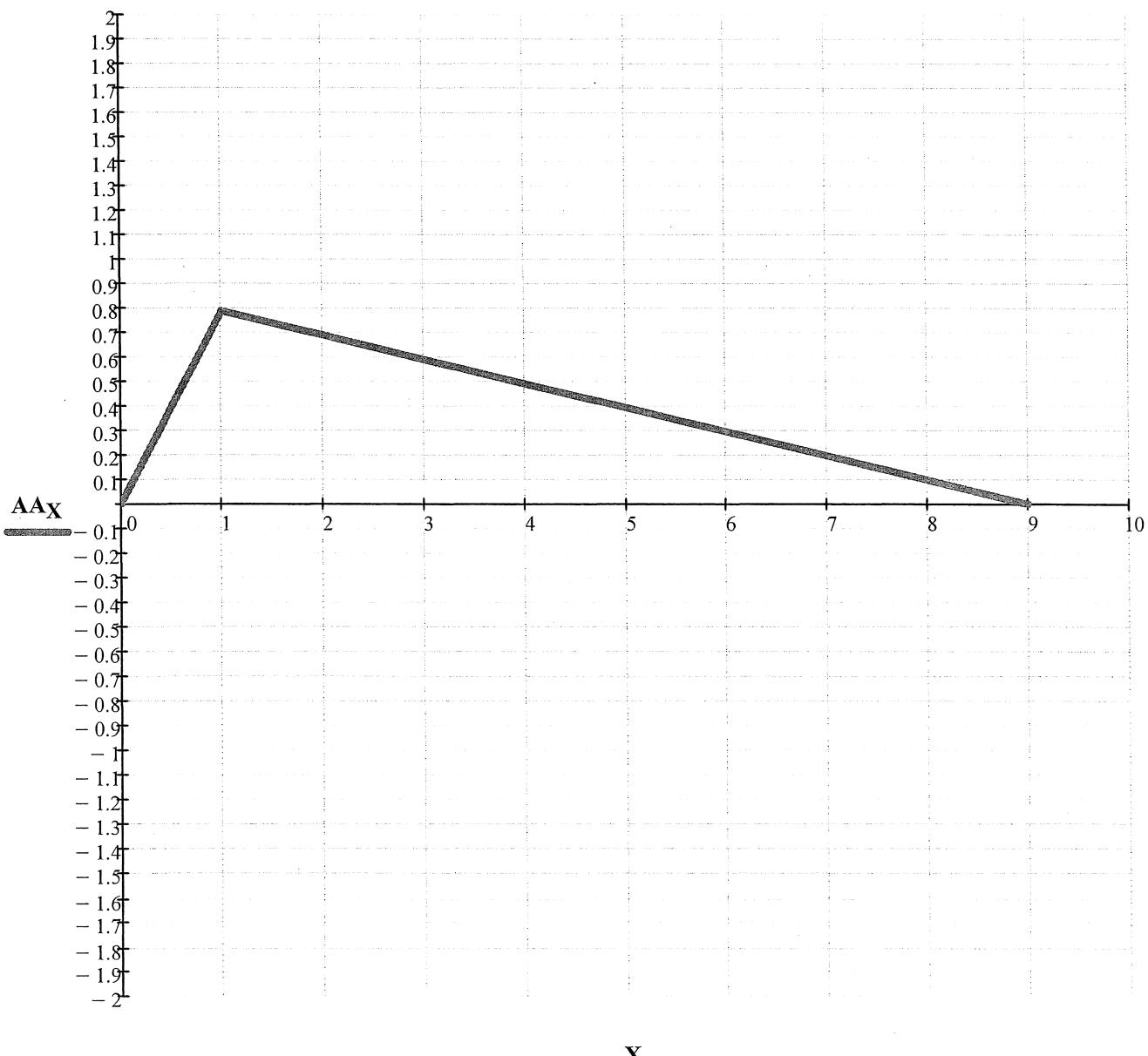
	0
0	0
1	0.787
2	0.689
3	0.59
4	0.492
5	0.394
6	0.295
7	0.197
8	0.098
9	0

This shows influence line ordinates
for the member selected above

08c.

INFLUENCE LINE

ORDNATE VALUE



X

08d.



Project: Mn/DOT - Truss Ratings
Project Number: 070745.30
Description: Truss Member Force Calculations

This template computes truss member live loads at a selected truss node.
Enter variables below shaded in grey. Regions or results in yellow self-compute.
Live Load is for HS-20 Lane Load with Concentrated Load for Flexure.

Note that this template reads external "excel" data files. These files must be properly linked to this worksheet for accurate function.

MN/DOT BRIDGE NO: 9090 - TH 2 over Red River in Grand Forks

IMPACT := 1.124

Input Impact Factor Based on Truss Length

DIST_FACTOR := 1.676

Input Distribution Factor for Truss,
Including any Applicable Reduction for
Multiple Lanes

MEMBER_TYPE := "D"

Input "D" for Diagonal, "V" for Vertical
or "C" for Chord.

PANEL_POINT := "L1"

Input Loaded Panel Point Under Consideration

MEMBER_NO := "L1U2"

Input Member Number Under Consideration

Member L0-U1 (MnDOT Numbering)

FOR VERTICAL MEMBERS, ENTER USING "L2U2T" AND "L2UTB" FOR FORCES

— Computation for Live Load Force in member
L0-U1, diagonal for Lane Loading w/ Conc. load
placed at L0 (MnDOT Numbering).

'AT TOP AND BOTTOM OF MEMBER, WHICHEVER IS DESIRED

08e.

MEMBER_LOADLANE := AA·BB·IMPACT·DIST_FACTOR

MEMBER_LOADTRUCK := AA·CC·IMPACT·DIST_FACTOR

MEMBER_LOADLANE = -199.494 ✓ (MnDOT Member
 $L_0 - U_1$) **AA =**

MEMBER_LOADTRUCK = -32.423

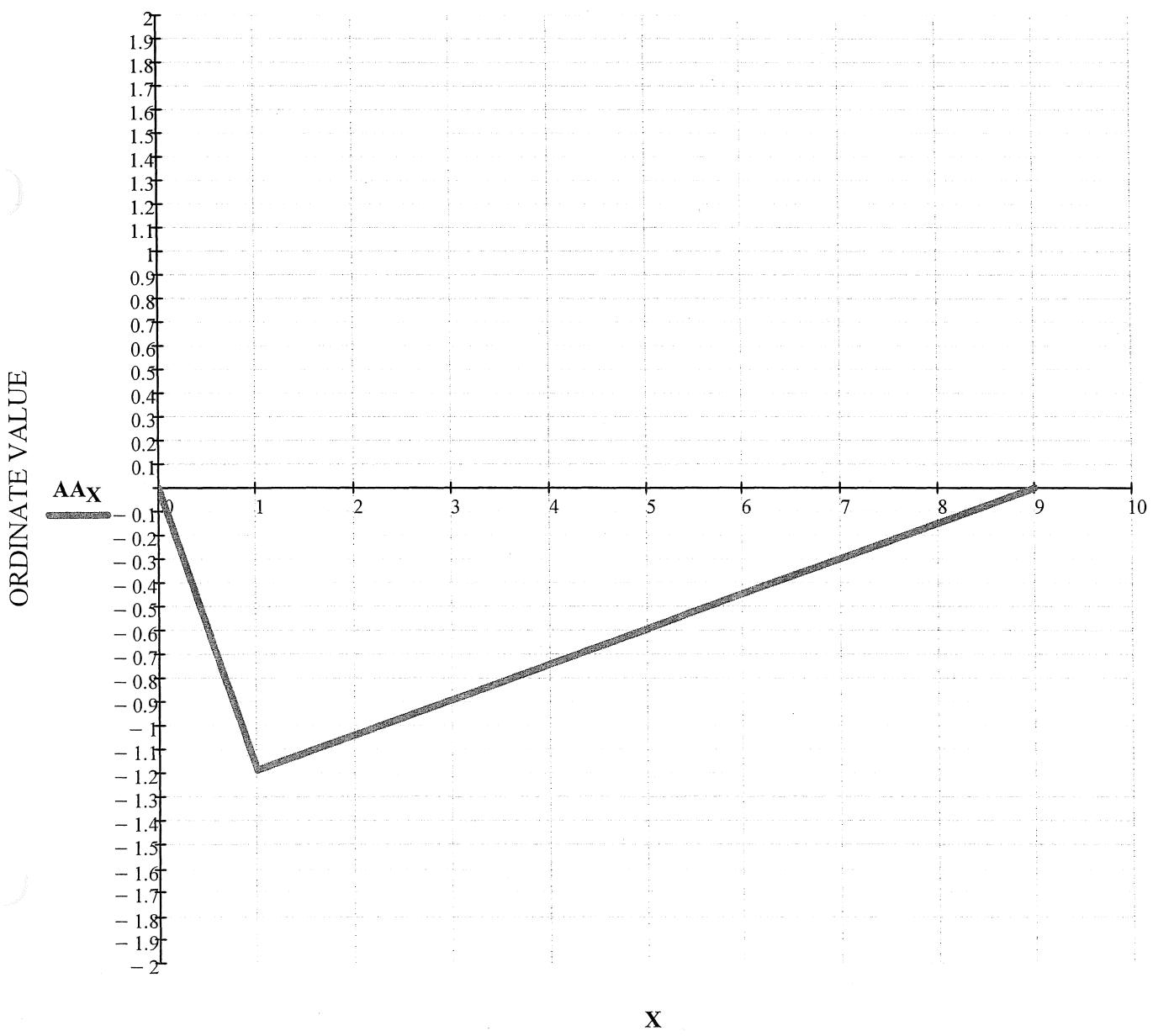
X := 0 ,1 .. 10

	0
0	0
1	-1.187
2	-1.039
3	-0.891
4	-0.742
5	-0.594
6	-0.445
7	-0.297
8	-0.148
9	0

This shows influence line ordinates
for the member selected above

08f.

INFLUENCE LINE



BRIDGE NO. 9090 - COINCIDENT MEMBER LOADS AT TRUSS JOINTS - HS20 LOADING																			COMPLETED BY: JWS			CHECKED BY: JDL																
JOINT NUMBER	NUMBER OF MEMBERS AT JOINT	COINCIDENT MEMBER LOADS - SERVICE LOAD WITH IMPACT INCLUDED (BOLD NUMBERS ARE MAXIMUM LOAD AT JOINT)																																				
		NOTE THAT NODE AND MEMBER LABELS DO NOT MATCH ORIGINAL PLAN - SOFTWARE USED REQUIRES FIRST NODE TO BE L1 INSTEAD OF L0. SEE ANALYSIS DATA FOR DRAWING SHOWING MEMBER/JOINT LABELS USED BELOW.																		MEMBER LOADS - BOTTOM CHORD (KIPS)																		
		L1-L2	L2-L3	L3-L4	L4-L5	L5-L6	L6-L7	L7-L8	L8-L9	L9-L10	U2-U3	U3-U4	U4-U5	U5-U6	U6-U7	U7-U8	U8-U9	L2-U2	L3-U3	L4-U4	L5-U5	L6-U6	L7-U7	L8-U8	L9-U9	L1-U2	L3-U2	L4-U3	L5-U4	L5-U6	L6-U5	L6-U7	L7-U8	L8-U9	L10-U9			
L1	2	159.1																								-239.9												
		159.1																								-257.8												
L2	3	159.1	159.1																71.3																			
		159.1	159.1																71.3																			
		90.1	90.1															114.6																				
L3	4		159.1	206.0															-15.6								70.8											
			155.7	224.9															-6.8								104.3											
			138.9	221.0															-10.0								124.3											
			86.3	60.9															-28.6								-38.2											
			108.4	142.6														66.5								51.6												
			98.9	159.9														-65.0								91.8												
L4	4			224.9	244.8														9.6								34.1											
				219.5	259.2														15.7								68.3											
				146.9	169.2														71.1								38.3											
				119.9	161.2													-53.9								71.0												
				177.3	234.9														2.9								99.5											
				142.5	109.5														46.1								-56.7											
L5	5				259.2	266.8													25.7								13.9	0 (A)										
					252.0	278.4													30.1								49.0	0 (A)										
					162.8	182.9												68.8								37.4	0 (A)											
					113.5	146.3												-51.2								60.7	0 (A)											
					180.0	229.1													8.5								90.8	0 (A)										
					169.3	136.4													51.3								-61.0	0 (A)										
L6	5					278.4	244.8												14.5								-17.7	45.1										
						259.8	259.2												14.4								13.3	13.9										
						264.6	264.1											15.0								13.5	14.2											
						167.4	198.0												11.1								73.6	15.2										
						206.2	129.9												9.0								-73.6	69.4										
						231.3	180.0												12.3								-4.5	90.8										
						109.1	169.3												7.4								51.7	-61.0	0 (A)									
L7	4						259.2	219.5											15.7										68.3									
							244.8	224.9											9.6										34.1									
							168.9	146.7										71.1										38.2										
							163.4	121.5										-53.9										72.0										
							234.4	176.6											2.9										99.5									
							109.6	142.5											46.1										-56.7									
L8	4							224.9	155.8										-6.8										104.3									
								206.0	159.1										-15.6										70.8									
								142.6	108.4									66.5										51.6										
								162.9	100.8									-65.0										93.6										
								221.0	138.9										-10.0										124.3									
								60.9	86.3										2																			

Truss Joint Review Summary - Lower Joints

Bridge Number 9090

DeadLoad =Original +1.5" Overlay in 1984

LiveLoad = HS20

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	Buckling K=1.0					Comments	
	Critical RF _{inv}	Critical RF _{op}	Critical RF _{inv}	Critical RF _{op}	^ CRF = 0.95	^ CRF = 0.85	
ORIGINAL POSITION							
L0	0.83	1.38	0.52	0.86			FLEXURE CONTROLS A-A (B-LN1)
BEARING MOVED 7" RIGHT							
L0	0.84	1.41	0.53	0.89			FLEXURE CONTROLS A-A (T-LN1)
BEARING MOVED 14" RIGHT							
L0	0.84	1.41	0.53	0.89			FLEXURE CONTROLS A-A (T-LN1)
BEARING MOVED 21" RIGHT							
L0	0.25	0.42	-0.06	-0.10			FLEXURE CONTROLS A-A (B-LN1)

¹ CRF= 1.00 for Rivet Check

² CRF= 0.95 for Rivet Check

B = Loads below the section cut are used

T = Loads above the section cut are used

LN1 = Live Lane Load Case 1 (Concentrated Load at L0)

LN2 = Live Lane Load Case 2 (Concentrated Load at L1)

Truss Joint Review Summary - Lower Joints

Bridge Number 9090

DeadLoad =Original +1.5" Overlay in 1984

LiveLoad = HS20

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	Buckling K=0.75					Comments
	Critical RF _{inv}	Critical RF _{op}	Critical RF _{inv}	Critical RF _{op}	¹ CRF = 0.95 ² CRF = 0.85	
ORIGINAL POSITION						
L0	0.83	1.38	0.52	0.86		FLEXURE CONTROLS A-A (B-LN1)
BEARING MOVED 7" RIGHT						
L0	0.84	1.41	0.53	0.89		FLEXURE CONTROLS A-A (T-LN1)
BEARING MOVED 14" RIGHT						
L0	0.84	1.41	0.53	0.89		FLEXURE CONTROLS A-A (T-LN1)
BEARING MOVED 21" RIGHT						
L0	0.25	0.42	-0.06	-0.10		FLEXURE CONTROLS A-A (B-LN1)

¹ CRF= 1.00 for Rivet Check

² CRF= 0.95 for Rivet Check

B = Loads below the section cut are used

T = Loads above the section cut are used

LN1 = Live Lane Load Case 1 (Concentrated Load at L0)

LN2 = Live Lane Load Case 2 (Concentrated Load at L1)

Tension in Gusset Plate (LRFD 6.13.5.2 and 6.8.2.1)

Bridge Number 9090

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

DL = dead load force in the member

LL+I = live load plus impact force in the member

Ped LL = pedestrian live load force in the member

F_y = minimum yield strength of gusset plate material

F_u = minimum tensile strength of gusset plate material

t_g = thickness of gusset plate before section loss

w1 = width between outside rivets/bolts in 1st row

d2 = distance from 1st row of rivets/bolts to last row of rivets

N_{sides} = number of sides of member with 30 degree distribution

$$W_{wh} = w1 + d2 \cdot (\tan 30) \cdot N_{sides}$$

(Whitmore effective width, see Figure 9-1 in AISC Steel Construction Manual 13th Edition)

N_{riv} = number of rivets/bolts crossed by whitmore effective width

Loss = percentage of section loss in plates

A_{gg} = gross area of gusset plates with section loss

A_{ng} = net area of gusset plates with section loss

A_{gspl} = gross area of splice plates with section loss

A_{nspl} = net area of splice plates with section loss

A_{gtb} = gross area of top and bottom plates with section loss

A_{ntb} = net area of top and bottom plates with section loss

A_g = gross area of all plates with section loss

A_n = net area of all plates with section loss

$$\phi_y P_{ny} = \phi_y F_y A_g$$

$$\phi_u P_{nu} = \phi_u F_u A_n$$

)—> ϕP_n is the smaller of $\phi_y P_{ny}$ and $\phi_u P_{nu}$

CRF = capacity reduction factor

$$RF_{inv} = (\phi P_n - 1.3 \cdot DL - 2.17 \cdot Ped LL) / (2.17 \cdot LL + I)$$

$$RF_{op} = (\phi P_n - 1.3 \cdot DL - 1.3 \cdot Ped LL) / (1.3 \cdot LL + I)$$

$$dia_{riv} = 0.875 \text{ in} \quad (\text{diameter of rivet/bolt})$$

designates input field

(No check required—Bot chord is
only tension member; there is no splice)

Location		Member Force			Gusset Plate Data										Splice Plates		Top/Bot Plates		Total Area		Tension Capacity		CRF = 0.95	CRF = 0.85			
Joint	Member	DL k	LL+I k	Ped LL k	F _y ksi	F _u ksi	t _g in	w1 in	d2 in	N _{sides}	W _{wh} in	N _{riv}	Loss %	A _{gg} in ²	A _{ng} in ²	A _{gspl} in ²	A _{nspl} in ²	A _{gtb} in ²	A _{ntb} in ²	A _g in ²	A _n in ²	ϕ _y P _{ny} k	ϕ _u P _{nu} k	RF _{inv}	RF _{op}	RF _{inv}	RF _{op}
L0	L0-L1				50.0	75.0	0.625				0.0			0.0	0.0					0.0	0.0	0	0	#####	#DIV/0!	#DIV/0!	#DIV/0!
											0.0			0.0	0.0					0.0	0.0	0	0	#####	#DIV/0!	#DIV/0!	#DIV/0!
											0.0			0.0	0.0					0.0	0.0	0	0	#####	#DIV/0!	#DIV/0!	#DIV/0!

Flexure in Gusset Plate (Truss Bridge Guide Specs. 1.11 and LRFD 6.14.2.8)

P_{DL} = axial force due to DL acting on the section

P_{LL+I} = axial force due to LL+I acting on the section

$P_{ped\ LL}$ = axial force due to pedestrian live load acting on the section

M_{DL} = moment due to DL acting on the section

M_{LL+I} = moment due to LL+I acting on the section

$M_{ped\ LL}$ = moment due to pedestrian live load acting on the section

Loss = percentage of section loss in plates

A_g = gross area of section cut through gusset plate with section loss

y = distance from c.g. of section to outside edge of gusset plate

I_g = moment of inertia of gross section cut through gusset plate with section loss

Bridge Number

9090

designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

f_{DL} = stress at edge of section due to DL

f_{LL+I} = stress at edge of section due to LL+I

$f_{ped\ LL}$ = stress at edge of section due to pedestrian live load

CRF = capacity reduction factor

$RF_{inv} = (\phi F_y - 1.3 \cdot f_{DL} - 2.17 \cdot f_{ped\ LL}) / (2.17 \cdot f_{LL+I})$

$RF_{op} = (\phi F_y - 1.3 \cdot f_{DL} - 1.3 \cdot f_{ped\ LL}) / (1.3 \cdot f_{LL+I})$

$\phi F_y = 50$ ksi

$\phi F_y = 36$ ksi, section B-B combined bot chord and gusset

Joint	Section	CRF = 0.95										CRF = 0.85						
		P_{DL} k	P_{LL+I} k	$P_{ped\ LL}$ k	M_{DL} k-in	M_{LL+I} k-in	$M_{ped\ LL}$ k-in	Loss %	A_g in^2	y in	I_g in^4	f_{DL} ksi	f_{LL+I} ksi	$f_{ped\ LL}$ ksi	RF_{inv}	RF_{op}	RF_{inv}	RF_{op}
L0	A-A(T-LN1)	1085.7	267.6		8614.3	2838.6			74.7	29.9	22220	26.1	7.4	0.0	0.84	1.41	0.53	0.89
L0	A-A(B-LN1)	1085.7	267.6		8736.3	2854.9			74.7	29.9	22220	26.3	7.4	0.0	0.83	1.38	0.52	0.86
L0	B-B (LN1)	0.7	0.3		6.4	2.7			194.0	21.1	62698	0.0	0.0	0.0	6390.47	10667.18	5717.64	9544.07
L0	C-C (LN2)	640.3	148.7		2161.1	502.0			80.9	32.4	28278	10.4	2.4	0.0	6.49	10.84	5.54	9.25
L0-7	A-A(T-LN1)	1085.7	267.6		8614.3	2838.6			74.7	29.9	22220	26.1	7.4	0.0	0.84	1.41	0.53	0.89
L0-7	A-A(B-LN1)	1085.7	267.6		1136.4	981.7			74.7	29.9	22220	16.1	4.9	0.0	2.50	4.18	2.03	3.39
L0-7	B-B (LN1)	0.0	0.0		7599.9	1873.2			194.0	21.1	62698	2.6	0.6	0.0	22.57	37.67	19.94	33.28
L0-7	C-C (LN2)	640.3	148.7		2161.1	502.0			80.9	32.4	28278	10.4	2.4	0.0	6.49	10.84	5.54	9.25
L0-14	A-A(T-LN1)	1085.7	267.6		8614.3	2838.6			74.7	29.9	22220	26.1	7.4	0.0	0.84	1.41	0.53	0.89
L0-14	A-A(B-LN1)	1085.7	267.6		6463.5	891.6			74.7	29.9	22220	23.2	4.8	0.0	1.67	2.78	1.19	1.98
L0-14	B-B (LN1)	0.0	0.0		15199.8	3746.4			194.0	21.1	62698	5.1	1.3	0.0	10.07	16.81	8.75	14.61
L0-14	C-C (LN2)	640.3	148.7		2161.1	502.0			80.9	32.4	28278	10.4	2.4	0.0	6.49	10.84	5.54	9.25
L0-21	A-A(T-LN1)	1085.7	267.6		8614.3	2838.6			74.7	29.9	22220	26.1	7.4	0.0	0.84	1.41	0.53	0.89
L0-21	A-A(B-LN1)	1085.7	267.6		14063.4	2764.8			74.7	29.9	22220	33.4	7.3	0.0	0.25	0.42	-0.06	-0.10
L0-21	B-B (LN1)	0.0	0.0		22799.7	5619.6			194.0	21.1	62698	7.7	1.9	0.0	5.90	9.85	5.02	8.39
L0-21	C-C (LN2)	640.3	148.7		2161.1	502.0			80.9	32.4	28278	10.4	2.4	0.0	6.49	10.84	5.54	9.25

Load Description on Section

B = Loads below the section cut are used

T = Loads above the section cut are used

LN1 = Live Lane Load Case 1 (Concentrated Load at L0)

LN2 = Live Lane Load Case 2 (Concentrated Load at L1)

* = Based on $\phi F_y = 36$ ksi using lesser strength of bottom chord

Θ = Not affected by movement of bearing

SECTION PROPERTIES AT L0, SECTION B-B

FLEXURAL SECTION CONSISTS OF 2 GUSSET PLATES AND BOTTOM CHORD

(0% section loss assumed in all plates)

	B	D	Y_{top}	A	$Y_{top} \cdot A$	$Y_{tot} - Y_{top}$	I_{part}	AD^2
GUSSET	0.625	66.625	33.31	41.64	1387.15	-12.21	15403	6207
GUSSET	0.625	66.625	33.31	41.64	1387.15	-12.21	15403	6207
SIDE PLATE	0.875	24.000	12.00	21.00	252.00	9.10	1008	1740
SIDE PLATE	0.875	24.000	12.00	21.00	252.00	9.10	1008	1740
diaph. plate	1.063	24.000	12.00	25.50	306.00	9.10	1224	2113
TOP PLATE	17.000	0.625	24.31	10.63	258.29	-3.21	0	109
TOP PLATE	17.000	0.625	24.94	10.63	264.99	-3.84	0	156
BOT. PLATE	17.000	0.625	-0.31	10.63	-3.32	21.42	0	4873
BOT. PLATE	18.125	<u>0.625</u>	-0.94	11.33	<u>-10.62</u>	22.04	<u>0</u>	5503

$$d = 66.625 \quad A_{tot} = 193.98 \quad 4093.65 \quad 34047.8 \quad 28649.85$$

$$Y_{tot} = 21.10 \text{ in} \quad I_{tot} = 62698$$

Note: If this section property spreadsheet is copied and edited for
use with other joints, you MUST revise $Y_{tot} - Y_{top}$ equation

Shear in Gusset Plate (Truss Bridge Guide Specs. 1.11 and AISC 13th Edition J4.2)

V_{DL} = shear force due to DL acting on the section

V_{LL+I} = shear force due to LL+I acting on the section

$V_{ped\ LL}$ = shear force due to pedestrian live load acting on the section

F_y = minimum yield strength of gusset plate material

F_u = minimum tensile strength of gusset plate material

t_g = thickness of gusset plate before section loss

w_g = width of the gusset plate at the cut section

Loss = percentage of section loss in gusset plates

A_g = gross area of 2 gusset plates including section loss

N_{rivets} = number of rivets/bolts crossed by whitmore effective width

A_{net} = net area of 2 gusset plates including section loss

ϕV_{ny} = shear yield capacity at cut section = $\phi_{ny} \cdot 0.74 \cdot (0.58 \cdot F_y) \cdot A_g$, where $\phi_{ny} = 0.95$ (per FHWA draft guidance)

ϕV_{nu} = shear rupture capacity at cut section = $\phi_{nu} \cdot (0.58 \cdot F_u) \cdot A_n$, where $\phi_{nu} = 0.80$ (per modified FHWA draft guidance)

ϕV_n = smaller of ϕV_{ny} and ϕV_{nu}

CRF = capacity reduction factor

$RF_{inv} = (\phi V_n - 1.3 \cdot V_{DL} - 2.17 \cdot V_{ped\ LL}) / (2.17 \cdot V_{LL+I})$

$RF_{op} = (\phi V_n - 1.3 \cdot V_{DL} - 1.3 \cdot V_{ped\ LL}) / (1.3 \cdot V_{LL+I})$

dia_{riv} = 0.875 in (diameter of rivet/bolt)

Bridge Number

9090

designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	Section	V_{DL} k	V_{LL+I} k	$V_{ped\ LL}$ k	F_y ksi	F_u ksi	t_g in	w_g in	Loss %	A_g in^2	N_{rivets}	A_{net} in^2	ϕV_{ny} k	ϕV_{nu} k	CRF =	0.95	CRF =	0.85
															RF_{inv}	RF_{op}	RF_{inv}	RF_{op}
L0	D-D (LN2)	735.9	159.1		50.0	75.0	0.625	60.0		75.0	1.0	73.8	1529	2567	1.44	2.40	0.99	1.66

Shear in Gusset Plate (Truss Bridge Guide Specs. 1.11 and AISC 13th Edition J4.2)

V_{DL} = shear force due to DL acting on the section

V_{LL+I} = shear force due to LL+I acting on the section

$V_{ped\ LL}$ = shear force due to pedestrian live load acting on the section

F_y = minimum yield strength of gusset plate material

F_u = minimum tensile strength of gusset plate material

t_g = thickness of gusset plate before section loss

w_g = width of the gusset plate at the cut section

Loss = percentage of section loss in gusset plates

A_g = gross area of 2 gusset plates including section loss

N_{rivets} = number of rivets/bolts crossed by whitmore effective width

A_{net} = net area of 2 gusset plates including section loss

ϕV_{ny} = shear yield capacity at cut section = $\phi_{vy} \cdot 0.74 \cdot (0.58 \cdot F_y) \cdot A_g$, where $\phi_{vy} = 0.95$ (per FHWA draft guidance)

ϕV_{nu} = shear rupture capacity at cut section = $\phi_{vu} \cdot 0.74 \cdot (0.58 \cdot F_u) \cdot A_n$, where $\phi_{vu} = 0.80$ (per FHWA draft guidance)

ϕV_n = smaller of ϕV_{ny} and ϕV_{nu}

CRF = capacity reduction factor

$$RF_{inv} = (\phi V_n - 1.3 \cdot V_{DL} - 2.17 \cdot V_{ped\ LL}) / (2.17 \cdot V_{LL+I})$$

$$RF_{op} = (\phi V_n - 1.3 \cdot V_{DL} - 1.3 \cdot V_{ped\ LL}) / (1.3 \cdot V_{LL+I})$$

dia_{riv} = 0.875 in (diameter of rivet/bolt)

Bridge Number

9090

designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	Section	V_{DL} k	V_{LL+I} k	$V_{ped\ LL}$ k	F_y ksi	F_u ksi	t_g in	w_g in	Loss %	A_g in^2	N_{rivets}	A_{net} in^2	ϕV_{ny} k	ϕV_{nu} k	CRF = 0.95		CRF = 0.85	
															RF_{inv}	RF_{op}	RF_{inv}	RF_{op}
L0	D-D	735.9	159.1		50.0	75.0	0.625	60.0		75.0	1.0	73.8	1529	1899	1.44	2.40	0.99	1.66

Block Shear in Gusset Plate (LRFD 6.13.4)

Bridge Number 9090

DL = dead load force in the member

LL+I = live load plus impact force in the member

Ped LL = pedestrian live load force in the member

F_y = minimum yield strength of gusset plate material

F_u = minimum tensile strength of gusset plate material

t_g = thickness of gusset plate before section loss

L_t = total length of all tension rupture lines in 1 gusset plate

N_{triv} = fractional number of rivets/bolts crossed by tension rupture lines in 1 gusset plate

Loss = percentage of section loss in plates

A_{tgadd} = gross area of section in any additional plates resisting tension with section loss

A_{tnadd} = net area of section in any additional plates resisting tension with section loss

A_{tg} = gross area of section in 2 gusset plates resisting tension with section loss

A_{tn} = net area of section in 2 gusset plates resisting tension with section loss

L_v = total length of all shear rupture lines in 1 gusset plate

N_{vriv} = fractional number of rivets/bolts crossed by shear rupture lines in 1 gusset plate

A_{vgadd} = gross area of section in any additional plates resisting shear with section loss

A_{vnadd} = net area of section in any additional plates resisting shear with section loss

A_{vg} = gross area of section in 2 gusset plates resisting shear with section loss

A_{vn} = net area of section in 2 gusset plates resisting shear with section loss

R_r = factored block shear rupture resistance for 2 gusset plates

CRF = capacity reduction factor

RF_{inv} = (R_r - 1.3·DL - 2.17·Ped LL) / (2.17·LL+I)

RF_{op} = (R_r - 1.3·DL - 1.3·Ped LL) / (1.3·LL+I)

dia_{riv} = 0.875 in (diameter of rivet/bolt)

(No check Req'd)

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	Member	DL k	LL+I k	Ped LL k	F _y ksi	F _u ksi	t _g in	L _t in	N _{triv}	Loss %	A _{tgadd} in ²	A _{tnadd} in ²	A _{tg} in ²	A _{tn} in ²	L _v in	N _{vriv}	A _{vgadd} in ²	A _{vnadd} in ²	A _{vg} in ²	A _{vn} in ²	A _{tn} /A _{vn} k	R _r k	RF _{inv}	RF _{op}	RF _{inv}	RF _{op}
L0	L0-L1				50.0	75.0	0.625				0.0	0.0							0.0	0.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Edge Buckling in Gusset Plate (Truss Bridge Guide Specs. 1.11)

Bridge Number 9090

b = length of unsupported gusset plate edge

t_g = thickness of gusset plate before section loss

Loss = percentage of section loss in plates

F_y = minimum yield strength of gusset plate material

 designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

Joint	b in	t_g in	Loss %	F_y psi	b/ t_g	$11000 / \sqrt{F_y}$	Stiffening Requirements
L0-R	23.00	0.625		50000	36.8	49.2	No stiffening required #DIV/0! #DIV/0!

Buckling in Gusset Plate (Std. Specs. 10.54.1.1)

Bridge Number 9090

DL = dead load force in the member

LL+I = live load plus impact force in the member

Ped LL = pedestrian live load force in the member

t_g = thickness of gusset plate before section loss

Loss = percentage of section loss in plates

w1 = width between outside rivets/bolts in 1st row

d2 = distance from 1st row of rivets/bolts to last row of rivets

N_{sides} = number of sides of member with 30 degree distribution

$$W_{wh} = w1 + d2 \cdot (\tan 30) \cdot N_{sides}$$

(Whitmore effective width, see Figure 9-1 in AISC Steel Construction Manual 13th Edition)

A_{column} = area of a single 1 inch wide "column" of unsupported gusset plates acting to resist buckling with section loss

L_c = unsupported length of gusset

r = radius of gyration for single 1 inch wide "column" of gusset plate

$$C_c = \sqrt{2\pi^2 E/F_y}$$

F_{cr} = buckling stress

P_u = maximum column strength

p_{DL} = DL acting on a single 1 inch wide "column"

p_{LL+I} = LL+I acting on a single 1 inch wide "column"

p_{ped LL} = pedestrian LL acting on 1 inch wide "column"

CRF = capacity reduction factor

$$RF_{inv} = (\phi P_u - 1.3 \cdot p_{DL} - 2.17 \cdot p_{ped LL}) / (2.17 \cdot p_{LL+I}) \text{ where } \phi = 1.0$$

$$RF_{op} = (\phi P_u - 1.3 \cdot p_{DL} - 1.3 \cdot p_{ped LL}) / (1.3 \cdot p_{LL+I}) \text{ where } \phi = 1.0$$

K = 1.00 (effective length factor)

E = 29000 ksi

designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

(No Check Req'd.)

Joint	Member	DL k	LL+I k	Ped LL k	F _y ksi	t _g in	Loss %	w1 in	d2 in	N _{sides}	W _{wh} in	A _{column} in ²	L _c in	r in	KL _c /r	C _c	F _{cr} ksi	P _u k	p _{DL} k/in	p _{LL+I} k/in	p _{ped LL} k/in	RF _{inv}	RF _{op}	RF _{inv}	RF _{op}	
L0	L0-U1				50.0	0.625					0.0	0.63		0.180	0.0	107.0	50.0	26.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Buckling in Gusset Plate (Std. Specs. 10.54.1.1)

Bridge Number 9090

DL = dead load force in the member

$LL + I$ = live load plus impact force in the member

Ped 11 = pedestrian live load force in the member

t_c = thickness of gusset plate before section loss

Loss = percentage of section loss in plates

w1 = width between outside rivets/bolts in 1st row

d_2 = distance from 1st row of rivets/bolts to last row of rivets

N_{side} = number of sides of member with 30 degree distribution

(Whitmore effective width, see Figure 9-1 in AISC Steel Construction Manual, 13th Edition)

A_{column} = area of a single 1 inch wide "column" of unsupported gusset plates acting to resist buckling with section loss

L = unsupported length of gusset

r = radius of curvature for single 4-inch-wide "backwall" of support plates

$$r = \text{Radius of gy}$$

E_c = buckling stress

P_c = maximum column strength

P_u = Maximum column strength

PDE = DE acting on a single 1-inch wide "column"

PLL+I = PLL Facing on a single 1-inch wide column

P_{ped} LL = pedestrian LL acting on

CRF = capacity reduction factor

RF_{inv} = (ψ_{u} - 1.3 μ_{DL} - 2.17 $\mu_{\text{ped}} \text{LD}$) / (2.17 $\mu_{\text{LL+I}}$) where $\psi = 1.0$

16 2.75 (55.0)

$$E = 29000 \text{ ksi}$$

 designates input field

Date: 08/31/09

Prepared By: LMM

Checked By: JDL (09-04-09)

(No check req'd.)

Bearing and Shear Check of Rivets/Bolts (Std. Specs. 10.56.1.3)

Bridge Number 9090

DL = dead load force in the member

LL+I = live load plus impact force in the member

Ped LL = pedestrian live load force in the member

F_u = minimum tensile strength of gusset plate material

SS N_{rv} = number of rivets/bolts in single shear in the member to gusset plate connection

DS N_{rv} = number of rivets/bolts in double shear in the member to gusset plate connection

SS p_{DL} = DL per rivet/bolt for rivets in single shear

SS p_{LL+I} = LL+I per rivet/bolt for rivets in single shear

SS p_{ped LL} = pedestrian live load per rivet/bolt for rivets in single shear

DS p_{DL} = DL per rivet/bolt for rivets in double shear

DS p_{LL+I} = LL+I per rivet/bolt for rivets in double shear

DS p_{ped LL} = pedestrian live load per rivet/bolt for rivets in double shear

SS t_g = thickness of gusset plate before loss

DS t_g = total thickness of plates before loss that rivets in double shear bear on

Loss = percentage of section loss in plates

L_c = smaller of clear distance between holes or clear distance between hole and edge of plate

d = rivet/bolt diameter

SS φR_b = factored bearing resistance for rivets in single shear

DS φR_b = factored bearing resistance for rivets in double shear

φR_s = factored total shear resistance for all rivets

CRF = capacity reduction factor

RF_{inv} = minimum of (φR - 1.3·p_{DL}) / (2.17·p_{LL+I}) for bearing and shear

RF_{op} = minimum of (φR - 1.3·p_{DL}) / (1.3·p_{LL+I}) for bearing and shear

dia_{rv} = 0.875 in (diameter of rivet/bolt)

φF_s = 25.000 ksi (shear capacity for rivet/bolt)

Date: 08/31/09

Prepared By: LMM

designates input field

Checked By: JDL (09-04-09)

Joint	Member	DL k	LL+I k	Ped LL k	F _u ksi	SS N _{rv}	DS N _{rv}	SS p _{DL} k/rivet	SS p _{LL+I} k/rivet	DS p _{DL} k/rivet	DS p _{LL+I} k/rivet	DS p _{ped LL} k/rivet	SS t _g in	DS t _g in	Loss %	L _c in	SS φR _b k	DS φR _b k	φR _s k	RF _{inv}	RF _{op}	RF _{inv}	RF _{op}
L0	L0-U1(LN2)	1109.9	257.8		75.0	78		7.1	1.7	0.0	0.0	0.0	0.625			2.38	73.8	0.0	2345	1.61	2.69	1.53	2.56



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*Received
3/24/08*

March 21, 2008

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**Rating Submittal
Bridge 9090- TH 2 over Red River
Updated Summary Sheets**

Enclosed please find copies of the updated truss member, floor beam and stringer rating sheets for Bridge No. 9090. As we have discussed these sheets have been updated to reflect the 0.95 and 0.85 Mn/DOT modifiers as well as to incorporate headings which indicate what formulas and factors have been utilized in creating the reports.

Sincerely
LHB, Inc.

A handwritten signature in black ink that reads "Joseph D. Litman".

Joseph D. Litman P.E.

Enclosures

c: LHB Project No. 070745.3



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February 13, 2008

Yihong Gao
Minnesota Department of Transportation
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3485 Hadley Avenue North
Oakdale, MN 55128-3307

**Rating Submittal
Bridge 9090- TH 2 over Red River**

Enclosed please find our submittal for the rating of Bridge No. 9090. As you review please let us know if you would like any additional detail or if you would like us to present any of this information in a different format. We also are available to meet at any time should you wish to go over in person.

We are proceeding with work on Bridge 9030 and will keep you informed as to our progress.

Sincerely
LHB, Inc.

A handwritten signature in black ink that reads "Joseph D. Litman".

Joseph D. Litman P.E.

Enclosures

c: LHB Project No. 070745.3

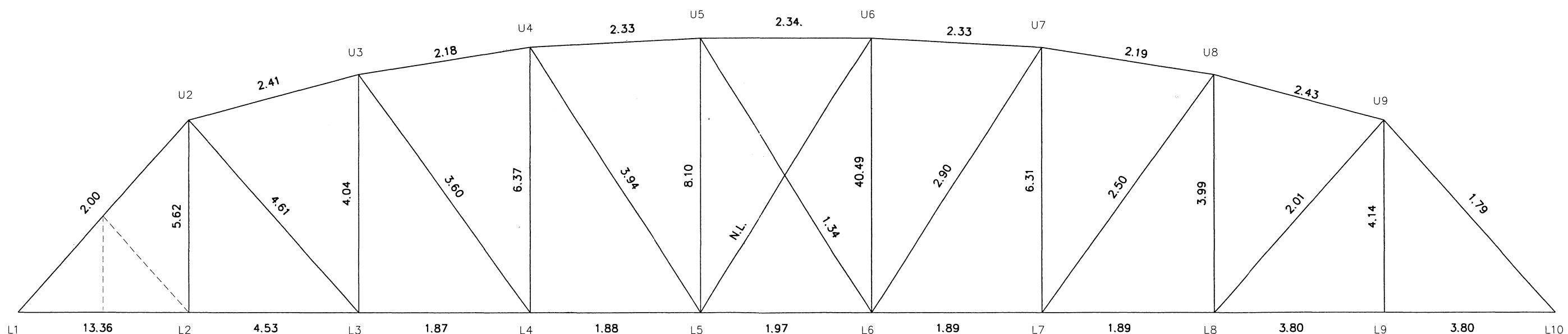
BRIDGE 9090 – ELECTRONIC FILES

There are 26 files contained on this CD. Below is a description of each file:

File Name	File Type	Description
2008-HS & Posting Trucks.dat	TRAP Data	Dead & Live load analysis input – four lanes HS 20 and Posting Trucks including dead load
2008-HS & Posting Trucks.res	TRAP Results	Dead & Live load analysis results – four lanes HS 20 and Posting Trucks including dead load
2008-P411 Truck.dat	TRAP Data	Live load analysis input – P411 Permit Truck
2008-P411 Truck.res	TRAP Results	Live load analysis results – P411 Permit Truck
2008-P413 Truck.dat	TRAP Data	Live load analysis input – P413 Permit Truck
2008-P413 Truck.res	TRAP Results	Live load analysis results – P413 Permit Truck
2008-Std A Truck.dat	TRAP Data	Live load analysis input – Standard A Permit Truck
2008-Std A Truck.res	TRAP Results	Live load analysis results – Standard A Permit Truck
2008-Std B Truck.dat	TRAP Data	Live load analysis input – Standard B Permit Truck
2008-Std B Truck.res	TRAP Results	Live load analysis results – Standard B Permit Truck
2008-Std C Truck.dat	TRAP Data	Live load analysis input – Standard C Permit Truck
2008-Std C Truck.res	TRAP Results	Live load analysis results – Standard C Permit Truck
COINCIDENTAL MEMBER LOADS – FINAL.xls	MS Excel	Tabulation of coincidental loads at truss node locations.
Dead Loads for Current Bridge.xls	MS Excel	Truss dead load calculations for current bridge.
Dead Loads for Original Bridge.xls	MS Excel	Truss dead load calculations for original bridge.
Final Summary Table AT 85%.xls	MS Excel	Final truss rating summary using Mn/DOT strength modifier of 85%.
Final Summary Table AT 95%.xls	MS Excel	Final truss rating summary using Mn/DOT strength modifier of 95%.
Final Tabulation at 85%.xls	MS Excel	Final truss member rating data using Mn/DOT strength modifier of 85%.
Final Tabulation at 95%.xls	MS Excel	Final truss member rating data using Mn/DOT strength modifier of 95%.
Influence Line Table.xls	MS Excel	Influence line tabulation for all members. This file is linked to the MathCad file listed below.
MEMBER FORCES - BRIDGE 9090.xmcd	MathCad	Program for computing coincidental member loads. Note that the program references the excel data file above (influence line table.xls) and will not function unless the file location is correctly specified in the matrix function named "AA" located to the far right inside the MathCad document. The file path will have to be changed manually in each line. Contact Jon Sitter, LHB at 218-727-8446 with questions.
Original Bridge – L1.dat	Trap Data	Dead load analysis input – original truss loads with support at node L1. Used as QA comparison to plan member loads.

Original Bridge – L1.res	Trap Results	Dead load analysis results – original truss loads with support at node L1. Used as QA comparison to plan member loads.
Original Bridge – L2.dat	Trap Data	Dead load analysis data – original truss loads with support at node L2. Used as QA comparison to plan member loads.
Original Bridge – L2.res	Trap Results	Dead load analysis results – original truss loads with support at node L2. Used as QA comparison to plan member loads.
READ ME.doc	MS Word	This document, describing files.

BRIDGE NO. 9090 - T.H. 2 OVER RED RIVER IN EAST GRAND FORKS
HS20 OPERATING RATING FACTORS
0.95 MnDOT STRENGTH MODIFIER



N.L. - NO LOAD IN MEMBER

TITLE:	DES:	DR:	APPROVED:	Bridge No.
HS20 OPERATING RF	CJM	CJM		9090
	CHK:	CHK:	JWS	
	Sheet No.	1 of 1	Sheet	